

## Appendix Q

### **Hydrology Data**



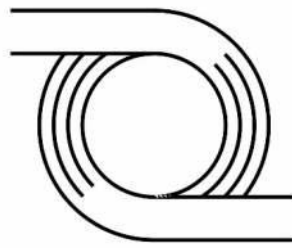


# Inglewood Basketball and Entertainment Center Low Impact Development (LID) Report

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**AECOM**

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D & D ENGINEERING, INC.

# INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER LOW IMPACT DEVELOPMENT (LID) REPORT

May 2, 2019

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## **I. Introduction**

The purpose of this report is to outline and describe the proposed Low Impact Development (LID) strategies and Best Management Practices (BMPs) necessary to adequately reduce the hydrological and environmental impact of developing the proposed Inglewood Basketball and Entertainment Center (IBEC) project, to comply with the requirements of LID Ordinance and LID Standard Manual<sup>1</sup>. Additionally, this report will determine the storm water quality design volume (SWQDV) calculated from the 85<sup>th</sup> percentile, 24-hour rain event that is required to be treated. Finally, this report will also discuss the methodology used to arrive at these conclusions, the infrastructure necessary to support it and the operations and maintenance procedures required to maintain the system effective over time.

## **II. Project Description**

The Inglewood Basketball and Entertainment Center (IBEC) Project is comprised of three sites located near the intersection of Century Boulevard and Prairie Avenue in the city of Inglewood. The first and main project site is located to the southeast of the intersection the second parcel is located to the southwest of the intersection, and the third piece is southeast of Century and Doty intersection. The first site of the proposed development includes a multi-purpose sport arena, a parking structure and other miscellaneous-use buildings. The site is located on an approximately 17-acre site bound by Century Blvd. on the North, Prairie Avenue on the West, Doty Avenue on the East and 103th Street on the South. The second site includes proposed parking structure over an approximately 5.5-acre parcel, not contiguous to the main project site, just west of Prairie Avenue. The third site includes a proposed parking structure and a hotel over an approximately 5-acre parcel, not contiguous to the main project site, just east of Doty Avenue. Refer to the project site map, *Figure 1 — Vicinity Map*, for project site locations.

The IBEC project is a mixed-use project that includes a multi-purpose sport arena with auxiliary structures including retail, office buildings, restaurants, hotel, parking structures and plaza areas. The project consists of 71,000 sq. ft. of office space, 48,000 sq. ft. of retail and food service space, 85,000 sq. ft. of practice facilities, 25,000 sq. ft. of Sports Medicine Clinic. 15,000 sq. ft. of Community Space, an 18,000-fixed seat arena with an additional 500 temporary seats, a parking structure and substantial surface parking.

### **a. Existing Conditions**

The existing site over the proposed main project site currently contains commercial buildings, a hotel, a fast-food restaurant and significant portions of vacant land. The existing site over the proposed parking structure, surface parking and a hotel consists of five parcels that are currently all vacant. The existing site over the proposed parking structure west of Prairie Avenue site consists of thirty parcels that are currently all vacant.

Preliminary geotechnical investigations indicate that infiltration is infeasible for the site. The native soil characteristics are generally draining poorly and mostly heavily clayey or silty with an infiltration rate less than the LA County minimum for infiltration of 0.3 in/hr. Refer to the geotechnical report and recommendations, *Appendix A — Excerpt from Geotechnical Report*, for a summary of geotechnical findings.

### **b. Proposed Conditions**

The proposed project seeks to develop the site into a mixed-use development composed of three general sites. The main site is considered the event area and includes a multi-purpose sports arena, retail/commercial buildings, a parking structure, and outdoor plaza. The east site proposes a hotel and parking structure, while the west site

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<sup>1</sup> (County of Los Angeles Department of Public Works, 2014)

proposes a parking structure. Due to these improvements, it is estimated that approximately 90% of the project site will be covered by impervious surfaces.

### **III. Low Impact Development (LID) Stormwater Quality Control Measures**

The Low Impact Development (LID) plan is intended to mitigate the hydrological and environmental stresses imposed on the site due to its proposed development. As the site's development typically increases impervious level, so does the stormwater runoff volume and the amount of environmental pollutant it produces. The goal of the LID plan is to mitigate these factors by both reducing the volume of stormwater and potential pollutants in stormwater runoff to the most reasonable extent possible. This strategy may be accomplished by implementing a variety of Best Management Practices (BMPs) stormwater quality control measures designed to handle the frequent, smaller storm event, or the initial volume of stormwater run-off from a larger storm event (referred as first flush). This study will focus on and follow the procedures for selecting and implementing stormwater quality measures, as recommended in the Los Angeles County Department of Public Works (LACDPW) Low Impact Development Standards Manual.

#### **a. Los Angeles County Design Guidelines**

The focus of the design criteria for stormwater control measures is the construction and implementation of stormwater quality control measures that meet stormwater runoff requirements in terms of on-site retention and pollutant removal. The project must design and implement stormwater quality control measures that can handle the SWQDv. Any surplus storm run-off must be diverted around the stormwater quality control measures to prevent overloading. The Los Angeles County Department of Public Works Low Impact Development Standards Manual categorized stormwater control quality measures into the following types listed in level of priority:

1. Retention based BMPs (bioretention, infiltration basin, drywells, capture and reuse cisterns, green roof)
2. Biofiltration BMPs (biofiltration)
3. Vegetation-based BMPs (stormwater planters, vegetated swales, tree-well filter, etc.)
4. Treatment-based BMPs (Extended detention basin, constructed wetlands, wet pond, sand filters, proprietary devices)

Systems in a lower priority level may only be used if higher priority measures are deemed to be technically infeasible as set forth in the county's standards manual. Due to the properties of the native soils and the tendency to percolate well, this study will focus on retention-based BMPs.

#### **b. Proposed Low Impact Development (LID) System**

The proposed Low Impact Development (LID) system will utilize a combination of county standard bio-filtration and/or stormwater planters to treat the SWQDv from the 85<sup>th</sup> percentile, 24-hour storm. This will be accomplished through directing runoff from drainage areas to onsite bio-filtration and stormwater planters currently proposed as part of the site hydrology study.

The proposed bio-filtration systems are designed to capture site runoff from roof drains and/or surface flow, treat the runoff through biological reactions within the planter soil media, and discharge at a rate intended to mimic pre-developed conditions. Refer to the specific system configurations, *Figure 3 – Site Specific Bio-Filtration Details*, for bio-filtration system configurations at their given locations. Sizing and capacity analysis of the proposed conventional bio-filtration systems will be calculated by following the design guidelines defined through the State of California Los Angeles Regional Water Quality Control Board. It is anticipated that the city of Inglewood will apply directly to the water board for approval. Once approval is granted to the city of Inglewood, only city approval is required for continuation.

### **IV. Hydromodification Analysis**

As outlined in Section 8.2 of the Los Angeles County Department of Public Works Low Impact Development Standards Manual, projects may be exempt from implementation of hydromodification control measures where assessments

of downstream channel conditions and proposed discharge hydrology indicate that adverse hydromodification effects to beneficial uses of natural drainage systems are unlikely. Since the proposed project site will discharge through a storm drain system into the concrete Dominguez Channel, the project is exempt from Hydromodification Control Measures.

## V. Site Design BMPs

### a. Site Design

Current water quality requirements are based on treating a specific volume of stormwater run-off from the project site (SWQDv). The design storm from which the SWQDv is calculated is defined as the greater of:

- The 0.75-inch, 24-hour rain event, or
- The 85<sup>th</sup> percentile, 24-hour rain event as determined by the Los Angeles County 85<sup>th</sup> percentile precipitation isohyetal map

The volume of stormwater run-off that must be retained at a project site is calculated using MODRAT. In this case, the SWQDv volume from the 85<sup>th</sup> percentile, 24-hour rain event will be utilized. LACDPW developed a hydrologic calculator (HydroCalc) that completes the full MODRAT calculation process and produce the SWQDv volumes and flow rates for single subareas. This report will utilize the results from HydroCalc as a means of determining the stormwater quality design volumes (SWQDv). The proposed site was divided into drainage sub-areas, based on the proposed site grading and proposed drainage patterns. Refer to the Conceptual Low Impact Development Exhibit, *Figure 2 – Conceptual Low Impact Development (LID) Exhibit*, for the definition of the drainage sub areas. The following table, Table 1 - Post-Development Conditions, summarizes the results of the study and required treating volumes SWQDv for each subarea.

**TABLE 1 - POST-DEVELOPMENT CONDITIONS AND BMP SUFFICIENCY SUMMARY**

*Inglewood Basketball and Entertainment Center*

Drainage Subarea				BMP Sufficiency Summary			
	Area (sf)	Q <sub>pm</sub> (cfs)	SWQDv x 1.5 (cf)	Bio-Filtration System	Required (sf)	Provided (sf)	Sufficient
A	55,094	0.3687	6,251	Biofiltration/ Stormwater Planter	2,500	2,600	Yes
B	168,409	0.8625	18,122	Biofiltration/ Stormwater Planter	7,249	7,300	Yes
CD	712,655	3.8106	81,434	Biofiltration/ Stormwater Planter	32,573	33,000	Yes
E	136,207	1.0662	15,122	Biofiltration/ Stormwater Planter	6,049	6,100	Yes
F	105,106	0.8028	10,950	Biofiltration/ Stormwater Planter	4,380	4,500	Yes
<b>Totals</b>	<b>1,101,446</b>	<b>7.8659</b>	<b>120,855</b>				

Refer to *Appendix B – Site Design Calculations* for each subarea HydroCalc worksheets.

Refer to *Appendix C – Sizing Calculations* for each Bio-Filtration System calculation.

## **b. BMP Selection**

All drainage areas, as listed in the table above, discharge via roof drains or surface flow to bio-filtration/stormwater planters located on the surface. Refer to the conceptual low Impact Development (LID) Exhibit, *Figure 2 – Conceptual Low Impact Development (LID) Exhibit*, for stormwater distribution.

Refer to the calculation sheets in *Appendix C – Bio-Filtration Sizing Calculations*, for detailed calculations demonstrating the capacity of each proposed bio-filtration system.

## **VI. Summary and Conclusion**

To summarize, the proposed low impact development (LID) system stormwater quality control measures and structural source measures are adequately designed and sized to accomplish the following:

- Capture and mitigate the SQWDv volume from the 85<sup>th</sup> percentile, 24-hour storm;
- Bio-filtration of captured volume by bio-filtration through a combination of standard bio-filtration and stormwater planters
- Prevent pollutants from contacting stormwater run-off and/or prevent discharge of contaminated stormwater run-off to stormdrain system

Based on the calculations and conclusions presented in this report, the proposed LID stormwater quality control measures will retain on-site through bio-filtration and will mitigate the required SWQDv volumes as defined by the Los Angeles County Department of Public Works Low Impact Development Standards Manual.

## **VII. References**

County of Los Angeles Department of Public Works. (2014). *Low Impact Development Standards Manual*. Los Angeles.

## **FIGURES**



***Figure 1 — Vicinity Map***

***Figure 2 — Conceptual Low Impact Development (LID)***

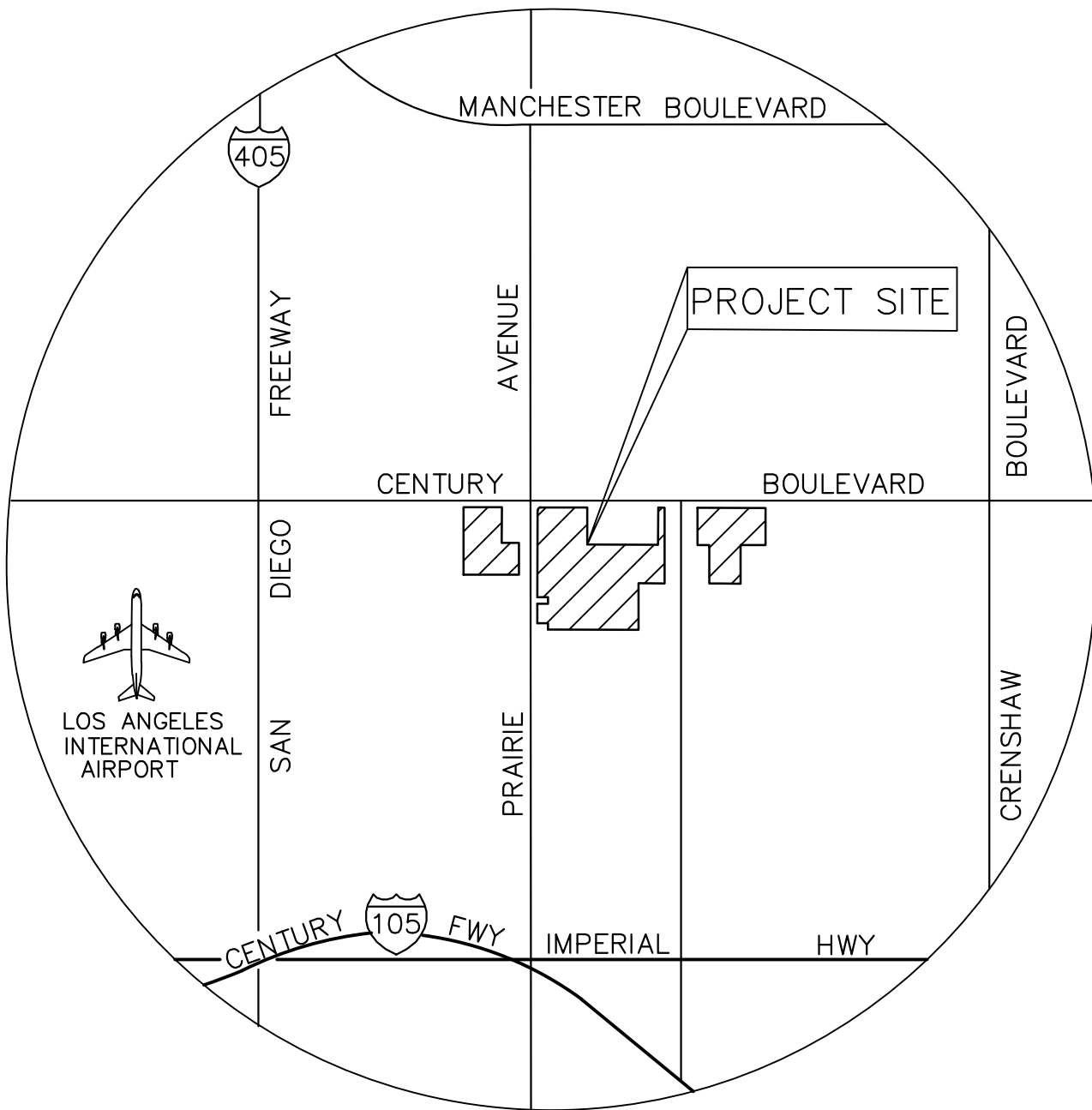
***Figure 3 — Site Specific Bio-Filtration Details***



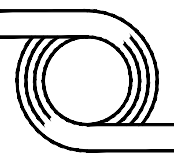
## **Figure 1**



## ***Vicinity Map***



**FIGURE 1**

	<b>D &amp; D ENGINEERING, INC.</b> 8901 S. LA CIENEGA BLVD, SUITE 106 INGLEWOOD, CA 90301 Phone: 424-351-6800	<b>INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER</b>		SCALE: AS SHOWN
		<b>VICINITY MAP</b>		DATE: 05/01/19
				SHT NO.: 01 OF 01

## **Figure 2**



### ***Conceptual Low Impact Development (LID)***



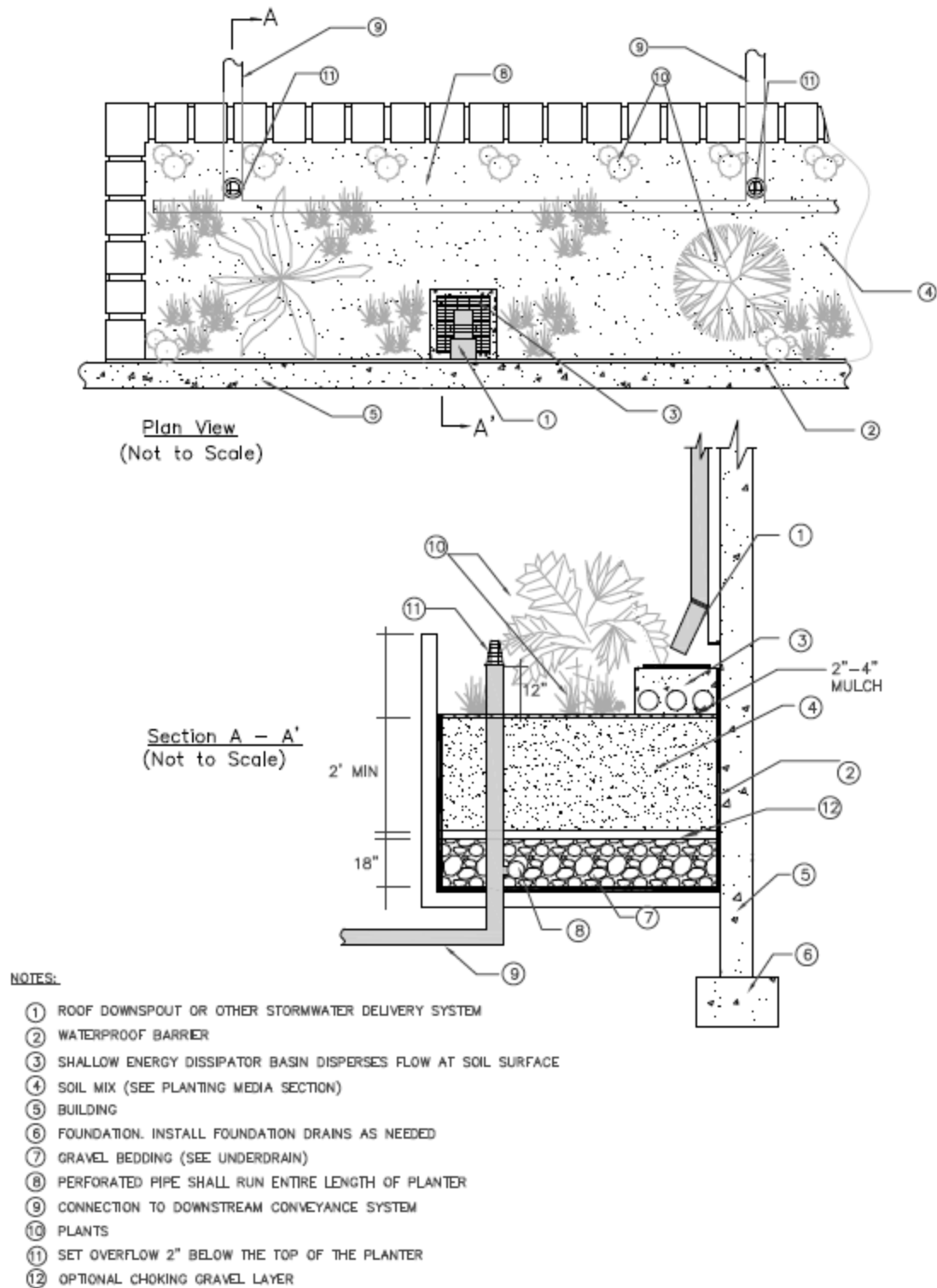




## **Figure 3**

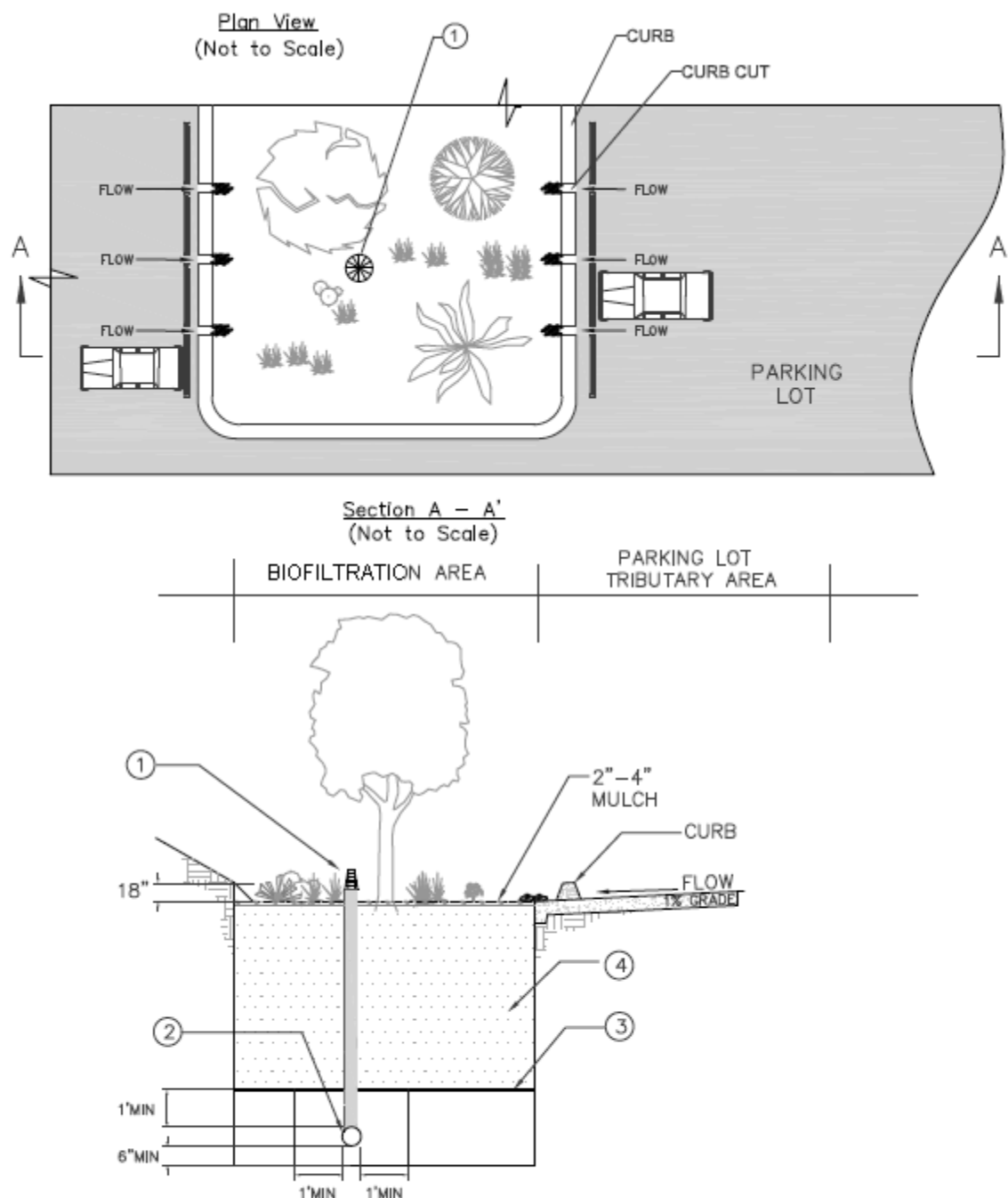


### ***Site Specific Bio-Filtration Details***



**Figure E-9. Stormwater Planter Schematic**





## NOTES

- ① OVERFLOW DEVICE: VERTICAL RISER OR EQUIVALENT.
- ② PERFORATED 6" MIN PVC PIPE UNDERDRAIN SYSTEM. WHERE SOIL CONDITIONS ALLOW, OMIT THE UNDERDRAIN AND INSTALL AN APPROPRIATELY SIZED GRAVEL DRAINAGE LAYER (TYPICALLY A WASHED 57 STONE) BENEATH THE PLANTING MEDIA FOR ENHANCED INFILTRATION.
- ③ OPTIONAL CHOKING GRAVEL LAYER.
- ④ 2' MIN PLANTING MIX; 3' PREFERRED.

**Figure E-7. Biofiltration Area Schematic**

## **Appendix A**



### ***Excerpt from Geotechnical Report***

### 5.11.1 Flexible Pavement Thicknesses

The following flexible pavement thicknesses for Traffic Index (TI) values of 5, 6 and 7 may be used:

**Table 8 – Minimum Flexible (AC) Pavement Thicknesses**

Traffic Index (TI)	Pavement Section (feet)	
	Asphaltic Concrete	Aggregate Base
4 to 5	0.3	0.55
6 to 7	0.4	0.65
7 to 8	0.5	0.75

### 5.11.2 Concrete Flatwork / Hardscape and Sidewalks

For PCC pavements in pedestrian areas, a pavement section of 4 inches PCC over 6 inches of aggregate base is typical for the kinds of soils to be expected at the site.

It should be noted that the above recommendations apply to parking lot, driveway and street areas only. Loading docks and trash enclosures should be paved with PCC pavement. We recommend that the section consist of a minimum of 6 inches of reinforced Portland cement concrete over 4 inches of Caltrans Class 2 Base with a minimum R-value of 78. The aggregate base should be compacted to at least 95 percent of the maximum dry density per ASTM D-1557 over unyielding subgrade.

## 5.12 INFILTRATION FEASIBILITY

Preliminary percolation tests were conducted at five (5) selected locations at the site (P-1 through P-5). The results of percolation testing are summarized in Appendix D.

Based on the results, infiltration rates for the soils in the upper 10 feet ranged from 0.32 to 3.52 in/hr. The test results represent a sampling of the upper materials which consist of variable and predominately clayey and silty sands. The upper value may be due to localized presence of more granular soils at the particular test location (P-2).

However, as discussed in this report, the subsurface native soils at the site consist predominately of clayey soils with estimated infiltration rates lower than 0.3 in/hr and with few or no connectivity to permeable soil horizons of adequate thickness. Moreover, the underlying, predominately clayey soils have never experienced saturation and have been found to exhibit more compressibility when inundated; therefore any infiltration of water into the subsurface soils, particularly within the areas to be occupied by permanent structures, is highly discouraged from a foundation performance stand-point. Given these constraints, infiltration practices might not be feasible at the site.

## **Appendix B**



### ***Post-Development Hydrological Conditions***

## Peak Flow Hydrologic Analysis

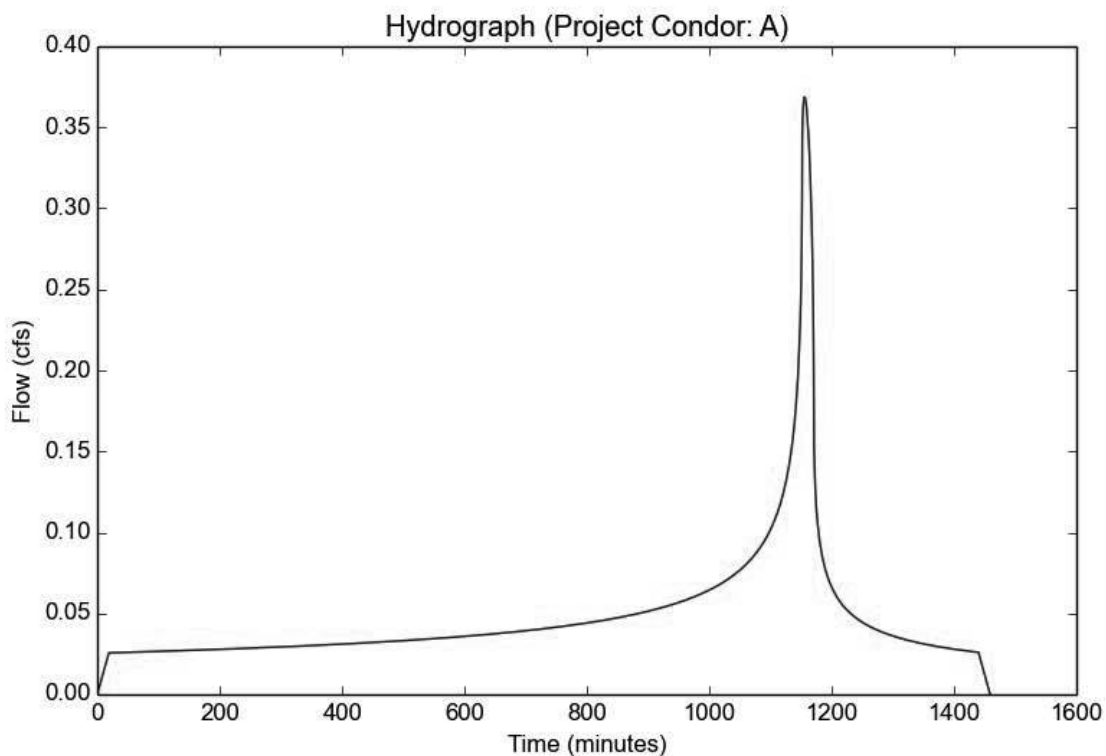
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	A
Area (ac)	1.27
Flow Path Length (ft)	370.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.96
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3345
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.868
Time of Concentration (min)	19.0
Clear Peak Flow Rate (cfs)	0.3687
Burned Peak Flow Rate (cfs)	0.3687
24-Hr Clear Runoff Volume (ac-ft)	0.0957
24-Hr Clear Runoff Volume (cu-ft)	4166.9399



## Peak Flow Hydrologic Analysis

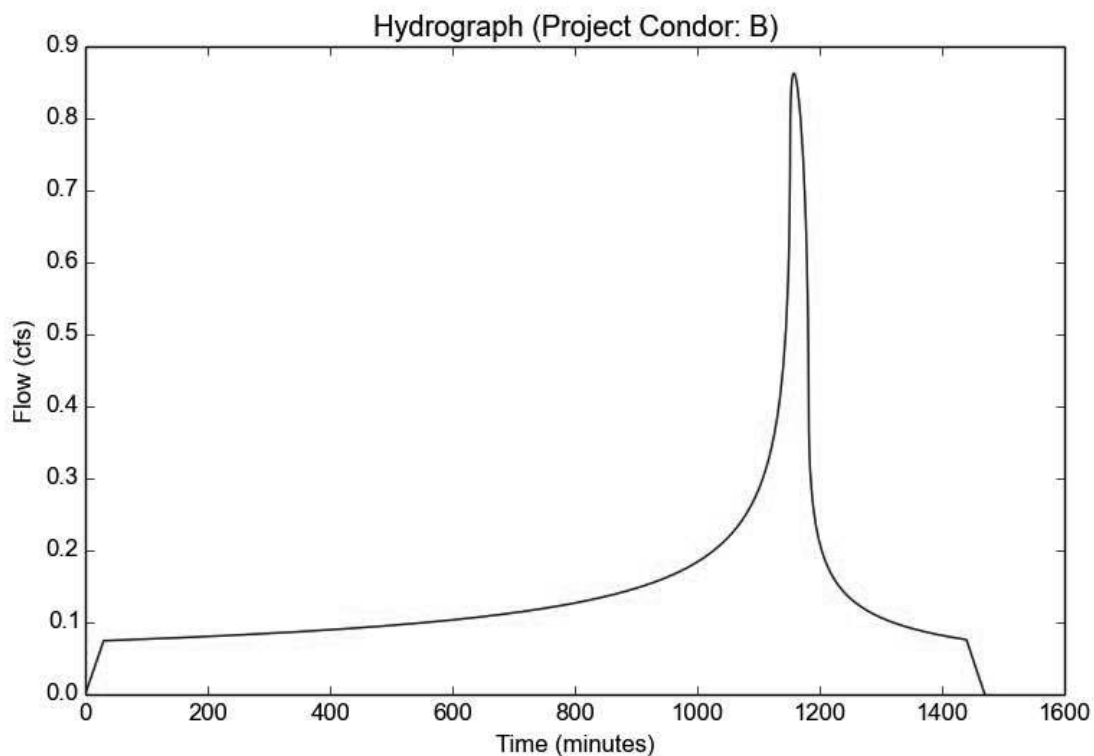
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	B
Area (ac)	3.86
Flow Path Length (ft)	700.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.91
Soil Type	13
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.2699
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.828
Time of Concentration (min)	30.0
Clear Peak Flow Rate (cfs)	0.8625
Burned Peak Flow Rate (cfs)	0.8625
24-Hr Clear Runoff Volume (ac-ft)	0.2773
24-Hr Clear Runoff Volume (cu-ft)	12081.3211



## Peak Flow Hydrologic Analysis

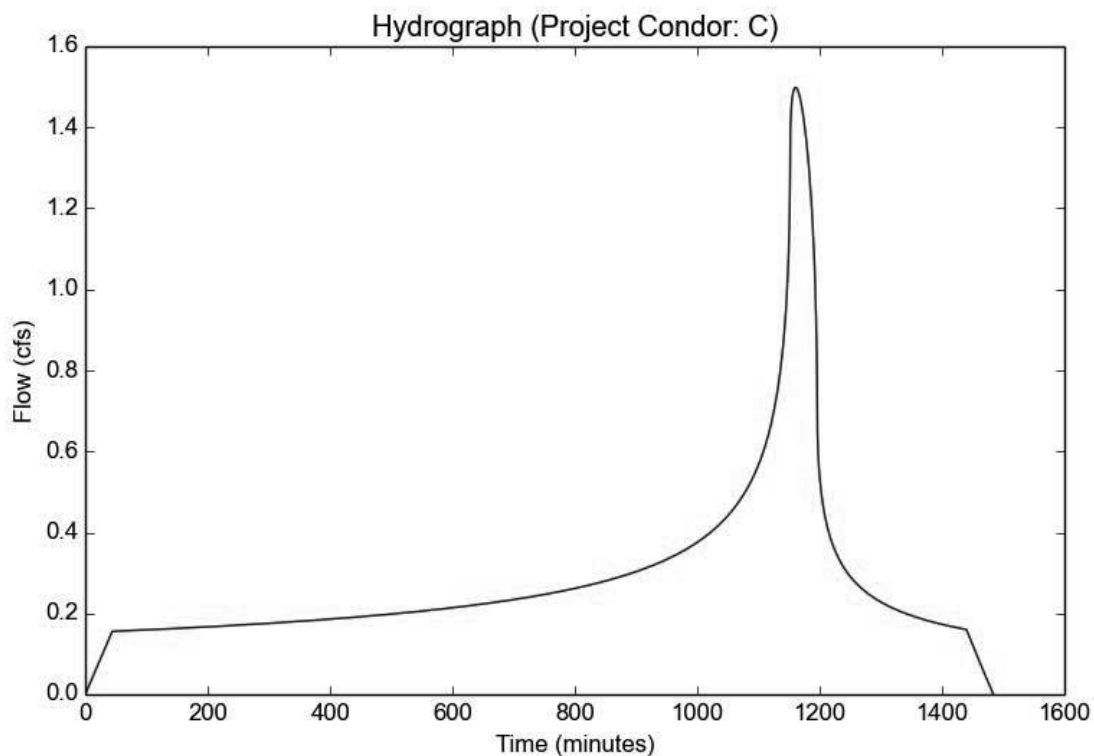
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	C
Area (ac)	7.73
Flow Path Length (ft)	1050.0
Flow Path Slope (vft/hft)	0.004
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	16
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.2254
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	44.0
Clear Peak Flow Rate (cfs)	1.4985
Burned Peak Flow Rate (cfs)	1.4985
24-Hr Clear Runoff Volume (ac-ft)	0.5769
24-Hr Clear Runoff Volume (cu-ft)	25129.3103



## Peak Flow Hydrologic Analysis

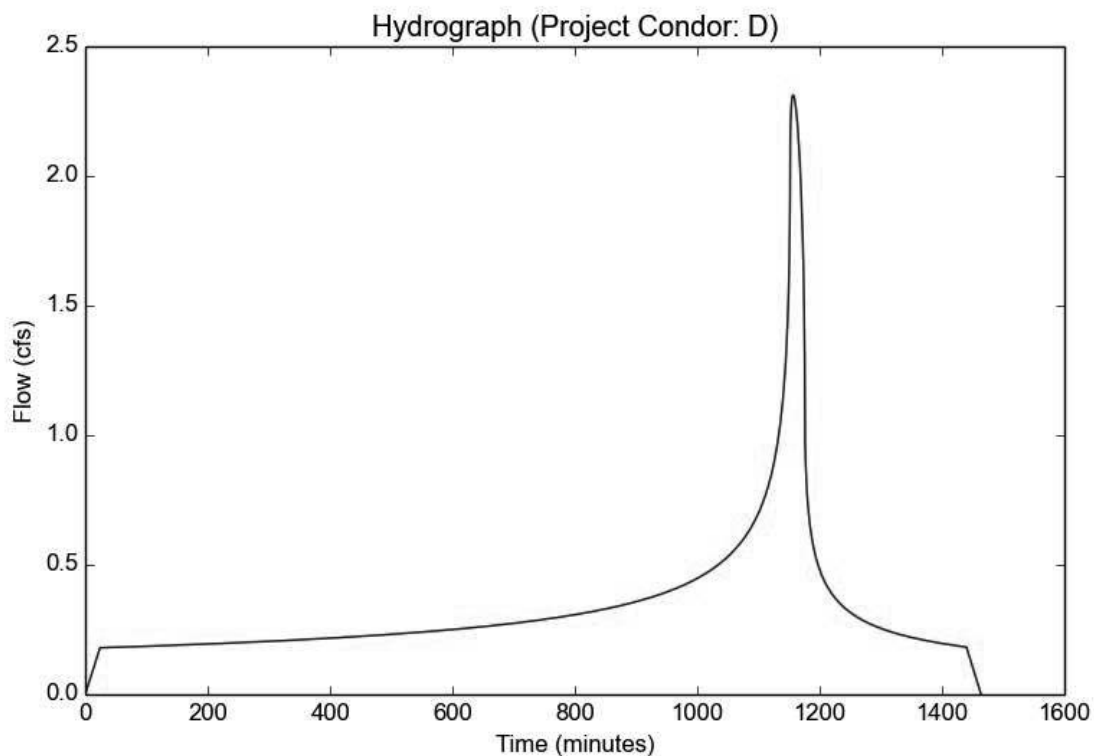
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	D
Area (ac)	8.97
Flow Path Length (ft)	490.0
Flow Path Slope (vft/hft)	0.008
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.95
Soil Type	16
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.2997
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.86
Time of Concentration (min)	24.0
Clear Peak Flow Rate (cfs)	2.3121
Burned Peak Flow Rate (cfs)	2.3121
24-Hr Clear Runoff Volume (ac-ft)	0.6694
24-Hr Clear Runoff Volume (cu-ft)	29159.8894





## Peak Flow Hydrologic Analysis

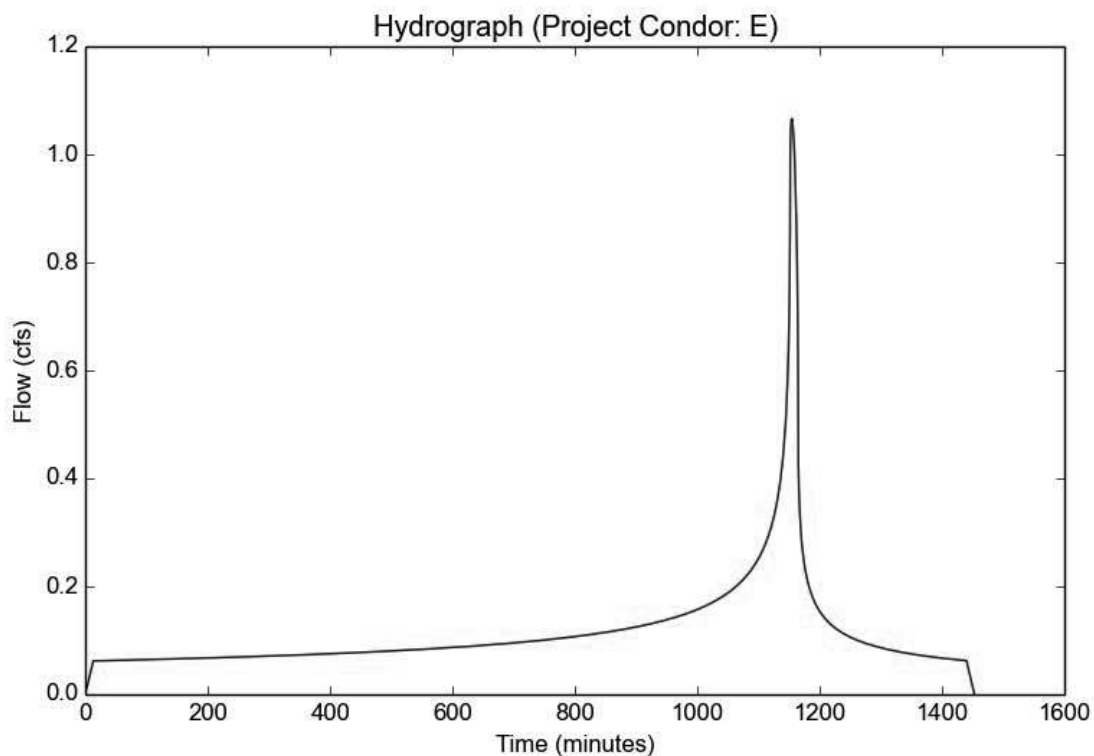
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	E
Area (ac)	3.19
Flow Path Length (ft)	190.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.92
Soil Type	16
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.3998
Undeveloped Runoff Coefficient (Cu)	0.1
Developed Runoff Coefficient (Cd)	0.836
Time of Concentration (min)	13.0
Clear Peak Flow Rate (cfs)	1.0662
Burned Peak Flow Rate (cfs)	1.0662
24-Hr Clear Runoff Volume (ac-ft)	0.2314
24-Hr Clear Runoff Volume (cu-ft)	10080.6767



## Peak Flow Hydrologic Analysis

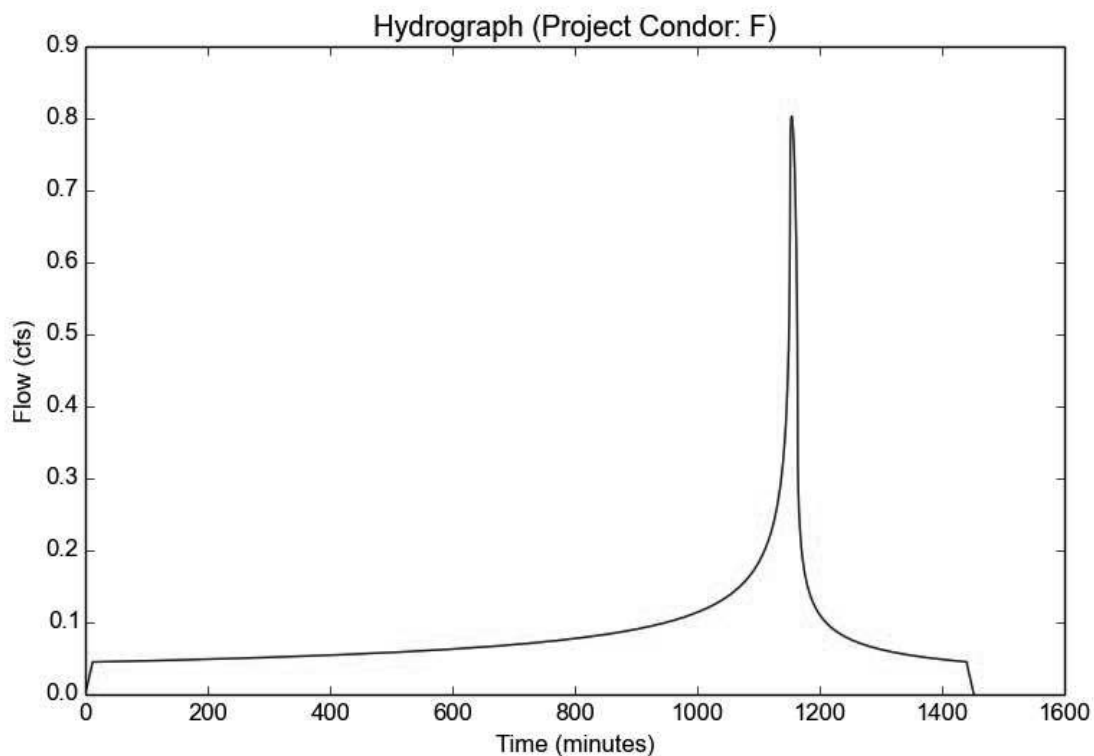
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/LID/Calcs/85th Percentile Hydrocalc.pdf  
Version: HydroCalc 1.0.3

### Input Parameters

Project Name	Project Condor
Subarea ID	F
Area (ac)	2.31
Flow Path Length (ft)	180.0
Flow Path Slope (vft/hft)	0.01
85th Percentile Rainfall Depth (in)	1.05
Percent Impervious	0.92
Soil Type	16
Design Storm Frequency	85th percentile storm
Fire Factor	0
LID	True

### Output Results

Modeled (85th percentile storm) Rainfall Depth (in)	1.05
Peak Intensity (in/hr)	0.4151
Undeveloped Runoff Coefficient (Cu)	0.1138
Developed Runoff Coefficient (Cd)	0.8371
Time of Concentration (min)	12.0
Clear Peak Flow Rate (cfs)	0.8028
Burned Peak Flow Rate (cfs)	0.8028
24-Hr Clear Runoff Volume (ac-ft)	0.1676
24-Hr Clear Runoff Volume (cu-ft)	7300.0099



## **Appendix C**



### ***Bio-Filtration Sizing Calculations***

**IBEC PROJECT**  
**INGLEWOOD, CA**  
**LID CALCULATIONS**

**DRAINAGE AREA**

**PLANTER**

A

A1, A2

Site area:	1.27	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V <sub>m</sub> ):	4167	cf
V <sub>design</sub> = V <sub>m</sub> * 1.5	6251	cf

Note: For Flow Through Planters

$$V_{\text{design}} = 1.5 * V_m$$

Sizing		Units
K <sub>sat</sub>	12	in/hour
FS	2	-
K <sub>sat,des</sub> = (K <sub>sat</sub> /FS)	6	in/hour
T	3	hrs
d <sub>p</sub>	12	in
A <sub>min</sub> =	<b>2,500</b>	<b>sf</b>

$$A_{\text{min}} = \frac{V_{\text{design}}}{\frac{T * K_{\text{sat,des}} + d_p}{12}}$$

T= Drawdown Time

d<sub>p</sub> = Ponding Depth

A<sub>min</sub> = Minimum Area Required

**IBEC PROJECT**  
**INGLEWOOD, CA**  
**LID CALCULATIONS**

**DRAINAGE AREA**

**PLANTER**

B

B1, B2, B3, B4

Site area:	3.86	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V <sub>m</sub> ):	12081	cf
V <sub>design</sub> = V <sub>m</sub> * 1.5	18122	cf

Note: For Flow Through Planters

$$V_{\text{design}} = 1.5 * V_m$$

Sizing		Units
K <sub>sat</sub>	12	in/hour
FS	2	-
K <sub>sat,des</sub> = (K <sub>sat</sub> /FS)	6	in/hour
T	3	hrs
d <sub>p</sub>	12	in
A <sub>min</sub> =	<b>7,249</b>	<b>sf</b>

$$A_{\text{min}} = \frac{V_{\text{design}}}{\frac{T * K_{\text{sat,des}} + d_p}{12}}$$

T= Drawdown Time

d<sub>p</sub> = Ponding Depth

A<sub>min</sub> = Minimum Area Required

**IBEC PROJECT**  
**INGLEWOOD, CA**  
**LID CALCULATIONS**

**DRAINAGE AREA**

**PLANTER**

C

CD1-CD11

Site area:	7.73	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V <sub>m</sub> ):	25129	cf
V <sub>design</sub> = V <sub>m</sub> * 1.5	37694	cf

Note: For Flow Through Planters

$$V_{\text{design}} = 1.5 * V_m$$

Sizing		Units
K <sub>sat</sub>	12	in/hour
FS	2	-
K <sub>sat,des</sub> = (K <sub>sat</sub> /FS)	6	in/hour
T	3	hrs
d <sub>p</sub>	12	in
A <sub>min</sub> =	<b>15,077</b>	<b>sf</b>

$$A_{\text{min}} = \frac{V_{\text{design}}}{\frac{T * K_{\text{sat,des}} + d_p}{12}}$$

T= Drawdown Time

d<sub>p</sub> = Ponding Depth

A<sub>min</sub> = Minimum Area Required

**IBEC PROJECT**  
**INGLEWOOD, CA**  
**LID CALCULATIONS**

**DRAINAGE AREA**

**PLANTER**

D

CD1-CD11

Site area:	8.97	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume (V <sub>m</sub> ):	29160	cf
V <sub>design</sub> = V <sub>m</sub> * 1.5	43740	cf

Note: For Flow Through Planters

$$V_{\text{design}} = 1.5 * V_m$$

Sizing		Units
K <sub>sat</sub>	12	in/hour
FS	2	-
K <sub>sat,des</sub> = (K <sub>sat</sub> /FS)	6	in/hour
T	3	hrs
d <sub>p</sub>	12	in
A <sub>min</sub> =	<b>17,496</b>	<b>sf</b>

$$A_{\text{min}} = \frac{V_{\text{design}}}{\frac{T * K_{\text{sat,des}} + d_p}{12}}$$

T = Drawdown Time

d<sub>p</sub> = Ponding Depth

A<sub>min</sub> = Minimum Area Required

**IBEC PROJECT**  
**INGLEWOOD, CA**  
**LID CALCULATIONS**

**DRAINAGE AREA**

**PLANTER**

E

E1, E2

Site area:	3.19	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume ( $V_m$ ):	10081	cf
$V_{design} = V_m * 1.5$	15122	cf

Note: For Flow Through Planters

$$V_{design} = 1.5 * V_m$$

Sizing		Units
$K_{sat}$	12	in/hour
FS	2	-
$K_{sat,des} = (K_{sat}/FS)$	6	in/hour
T	3	hrs
$d_p$	12	in
$A_{min} =$	<b>6,049</b>	<b>sf</b>

$$A_{min} = \frac{V_{design}}{\frac{T * K_{sat,des} + d_p}{12}}$$

T= Drawdown Time  
 $d_p$  = Ponding Depth  
 $A_{min}$  = Minimum Area Required



# IBEC PROJECT

## INGLEWOOD, CA

### LID CALCULATIONS

#### DRAINAGE AREA

#### PLANTER

F

F1, F2

Site area:	2.31	ac
Impervious	0.95	%
85th Percentile:	1.05	in
Volume ( $V_m$ ):	7300	cf
$V_{design} = V_m * 1.5$	10950	cf

Note: For Flow Through Planters

$$V_{design} = 1.5 * V_m$$

Sizing		Units
$K_{sat}$	12	in/hour
FS	2	-
$K_{sat,des} = (K_{sat}/FS)$	6	in/hour
T	3	hrs
$d_p$	12	in
$A_{min} =$	<b>4,380</b>	<b>sf</b>

$$A_{min} = \frac{V_{design}}{\frac{T * K_{sat,des} + d_p}{12}}$$

T= Drawdown Time  
 $d_p$  = Ponding Depth  
 $A_{min}$  = Minimum Area Required



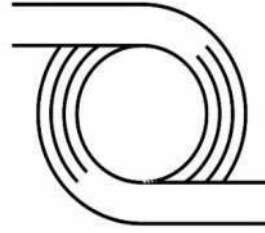
Inglewood Basketball and  
Entertainment Center  
Preliminary Hydrology  
Report

---



**AECOM**

**WILSON  
MEANY**



D & D ENGINEERING, INC.

# INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER PRELIMINARY HYDROLOGY REPORT

May 1, 2019

D & D Engineering, Inc.  
8901 S. La Cienega Blvd.  
Inglewood, CA 90301  
424-351-6800



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II. Site Description .....	3
III. Existing Storm Drain Systems Description and Capacity .....	4
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V. Hydrology Analysis and Calculations .....	5
VI. Post Development runoff .....	5
VII. Summary and Conclusion .....	6

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*Table 1 — Allowable Runoff, Existing and Proposed Flows*

## **FIGURES**

*Figure 1 — Vicinity Map*

*Figure 2 — Existing Storm Drains*

*Figure 3 — Pre-Development Hydrology Map*

*Figure 4 — Post-Development Hydrology Map*

*Figure 5— Proposed Onsite Runoff Distribution to Existing Storm Drain Lines*

## **APPENDICES**

### **Appendix A**

*Off-Site Hydrology and LACDOW Information Request Summary*

- *Figure 2 — Existing Storm Drains*
- *Offsite Tributary Area Map for Project 4402 & 681*
- *Offsite Tributary Area Map for Project DDI #8*
- *Information Request Summary*

#### Appendix B

- *LACDPW, 2006 Hydrology Manual, Appendix B Hydrologic Maps, 08 Inglewood*

#### Appendix C

##### *Pre-Development Runoff Calculations*

- *Figure 3 — Pre-Development Hydrology Map*
- *Sub-areas HydroCalc Worksheets*

#### Appendix D

##### *Post-Development Runoff Calculations and Basin Routing*

- *Figure 4 — Post-Development Hydrology Map*
- *Figure 5 — Proposed Onsite Runoff Distribution to Existing Storm Drain Lines*
- *Sub-Areas HydroCalc Worksheets*
- *Summary of Post-Development Runoff Distribution to Existing Storm Drain Systems*

#### Appendix E

##### *Los Angeles County As-Built Plans*

- *LACDPW Project 4402 & 681 As-Built Plans*
- *LACDPW Project 4401, Line A As-Built Plans*
- *LACDPW DDI # 8 As-Built Plans*

## **I. INTRODUCTION**

The purpose of this report is to outline and describe the onsite hydrology and existing storm drain infrastructure serving the existing site where Inglewood Basketball and Entertainment Center (IBEC) Project is to be constructed on. Additionally, this report will present the on-site hydrology of the proposed project, quantify the proposed storm runoff flows, the proposed, and the new storm drain infrastructure necessary to accommodate the proposed project. New infrastructure design is to adhere to the approved Los Angeles County Department of Public Works (LACDPW) allowable storm drain discharges from the site.

## **II. SITE DESCRIPTION**

IBEC Project is comprised of three sites located near the intersection of Century Boulevard and Prairie Avenue in the city of Inglewood. The first and main project site is located to the southeast of the intersection, the second is located to the southwest of the intersection, and the third site is further east, just east of Doty avenue. The first site of the proposed development includes a multi-purpose sport arena, a parking structure and other miscellaneous use buildings. The site is located on an approximately 17-acre parcel bound by Century Blvd on the North, Prairie Ave on the West, Doty Ave on the East and 103th Street on the South. The second site includes proposed parking structure over an approximately 5.5-acre site, just west of Prairie Avenue. The third site includes proposed approximately 2.9-acre surface parking and portion of vacant land over an approximately 5-acre site, not contiguous to the main project site, just east of Doty Avenue. Refer to the project site map, *Figure 1 — Vicinity Map*, for project site locations.

The existing site over the proposed main project site currently contains commercial buildings, a hotel, a fast-food restaurant and vacant land for significant portion. The existing site over the proposed parking structure site consists of twenty-seven parcels that are all currently vacant lots. The existing site over the proposed surface parking site consists of five parcels that are all currently vacant lots.

The site topography generally slopes from the north-east to south-west corner.

Currently, the existing site runoff is discharging to surrounding public streets where it is collected by the existing storm drain system. There is currently no existing on-site storm drain system in place. The existing runoff breakdown from project sites to the existing storm drain systems is as follows:

- Majority of main site runoff of 18.4 cfs to Project 4402 and Project 681 County storm drain lines.



- Parking structure site runoff is split to two systems – portion north of 101<sup>st</sup> Street runoff of 2.8 cfs to Project 4402 Line B and portion south of 101<sup>st</sup> Street runoff of 4.8 cfs to DDI#0008 Freeman Avenue County storm drain lines.
- Surface parking runoff of 6.3 cfs to DDI # 0008 Yukon County storm drain line.

### **III. EXISTING STORM DRAIN SYSTEMS DESCRIPTION AND CAPACITY**

Existing as-built record drawings and hydrology maps were obtained from LACDPW to characterize the storm drains that currently serve the project sites. The as-built plans can be found in [Appendix E](#).

The existing storm drain systems serving the project sites are maintained by the LACDPW and include Project 4401 Line A, Project 4402 & 681 and Project DDI # 8. These are located adjacent to the project site along Prairie and Doty Avenues. Refer to *Figure 2 — Existing Storm Drains* for existing off-site storm drain infrastructure.

The table below summarizes the storm drain infrastructure adjacent to the project site based on the latest available as-built and record drawings reviewed to date.

Location	Size	Notes
Prairie Avenue	LACDPW Project 4402 & 681- 60" diameter storm drain that flows south along Prairie Avenue.	Collects runoff flowing to Prairie from offsite properties as well as majority of proposed site
Doty Avenue	LACDPW Project 4401, Line A – 7'-0" W x 9'-0" H RCB that flows south along Doty Ave	Accepts flows from Projects 4401, Line B and MTD 922 north of Century Avenue and runoff to Doty Avenue from adjacent properties
East of Doty Avenue	LACDPW Project DDI # 8 – 4'-3" W x 4'-0" H RCB	Flowing south parallel and to the east of Doty Avenue

An information request was submitted to the LACDPW to obtain information regarding capacities of the existing storm drain systems listed above and the allowable Q's that can be discharged from the project sites to these storm drain systems. Refer to [Appendix A](#) for a summary of the allowable storm water discharges to Project 4401, Project 4402 and DDI #8 prepared and approved on October 2017 by the LACDPW Design Division.

#### **IV. PROJECT DESCRIPTION**

IBEC Project is a mixed-use project that includes a multi-purpose sport arena with auxiliary structures including retail, office buildings, restaurants, parking structures and plaza areas. The project consists of 71,000 sq. ft. of office space, 48,000 sq. ft. of retail and food services space, a 150-room hotel, 85,000 sq. ft. of practice facilities, 15,000 sq. ft. of community space, 25,000 sq. ft. of sports medicine clinic and an 18,000-fixed seat arena with an additional 500 temporary seats, a parking structures and surface parking.

#### **V. HYDROLOGY ANALYSIS AND CALCULATIONS**

Hydrologic calculations were performed utilizing the LACDPW Hydrology Manual dated January 2006 and county HydroCalc Program Method. Per the LACDPW hydrology Manual, The Capital Flood Level of Protection produced by a 50-year frequency design storm is applied to proposed on-site drainage areas and facilities in sump conditions.

The existing and post-development flow rates generated by the Condor project site were calculated using the LACDPW Inglewood 50-year, 24-hour isohyet (5.15 inches rainfall depth) and associated runoff coefficient curve (Soil Type No.16 for the main site and No.13 for the hotel and eastern parking site) and are shown in [Appendix C](#) and [Appendix D](#).

#### **VI. POST DEVELOPMENT RUNOFF AND BASIN ROUTING**

IBEC Project consists of three major subareas as shown in *Figure 4 — Post-Development Hydrology Map*, with each of the project sites consisting of separate subareas. The main project site consists of two major drainage area, denoted as DA “A-3” and DA “A-4”, with a contributing runoff to the existing Project 681 storm drain lines. The west parking structure site consists of another two major drainage area denoted as DA “A-5” and DA “A-6” with a contributing runoff to the existing Project 4402 & 681 storm drain lines. The east parking structure and hotel site consists of another two major drainage area denoted as DA “A-1” and DA “A-2”, with a contributing runoff to the existing DDI #8 storm drain system. Design peak flows were calculated for a 50-year frequency design storm for basin routing, refer to [Appendix D](#) for supporting calculations.

As shown in [Appendix C](#)- Pre-Development Runoff Calculations and [Appendix D](#) – Post-Development Runoff Calculations, the post-development runoff quantities exceed the pre-development runoff quantities. Additionally, the post-development peak flows for proposed drainage sub-areas exceed the approved allowable discharge rates to existing LACDPW Project 4402 & 681 and DDI #8 systems. Therefore, on-site detention is required for all three

project's sites. For the arena site, an underground precast detention facility with an approximately 100,800 cu.ft. volume is estimated. A similar detention facility will be required for the hotel and eastern parking site with a combined detention of approximately 8,900 cu. ft volume and for northerly portion of the west parking structure with approximately volume of 5,300 cu. ft. volume. The southerly portion of the parking structure drainage is anticipated to be diverted to the Prairie Avenue project # 681 storm drain instead of the Freeman storm drain system. A similar detention facility will not be feasible for the southerly parking structure site, therefore the additional detention from the arena site will compensate for the southerly portion of the parking structure. The arena site detention facility outfall will be restricted to a maximum 5.52 cfs and with the southerly parking structure peak runoff of 8.78 cfs, the total discharge to project # 681 of 14.30 cfs will not exceed the allowable flow rate of 14.32 cfs. The east parking structure and hotel site and northerly portion of the west parking structure detention facilities will have maximum outfall rates of 5.11 cfs and 1.96 cfs, respectfully.

Summary of allowable flow rates and project contributing flow rates table from all detention facilities can be found in *Appendix D Post-Development Runoff Calculations and Figure 5- Proposed Onsite Runoff Detention to Existing Storm Drain Lines.*

## **VII. Summary and Conclusion**

The results of this study are summarized in following table.

Table 1- Allowable Runoff, existing and proposed flows

ITEM	Project 4402 (CFS)	Project 681 (CFS)	DDI#8 (CFS)	TOTAL (CFS)
Proposed Onsite 50-year Flow into Pipeline-prior to detention (Figure 4)	6.36 (Sub-area A6)	41.63 (Sub-areas A3, A4 & A5)	11.29 (Sub-areas A1 & A2)	59.28
Proposed Onsite 50-year Flow into Pipeline (HydroCalc, Figure 5) *	<b>1.96</b> (Sub-area A6 detention outfall)	<b>14.30</b> (Sub-areas A3 & A4 detention outfall & A5)	<b>5.11</b> (Sub-areas A1 & A2 detention outfall)	<b>21.37</b>
LACDPW Allowable Flow Rates (Appendix B)	2.31	14.32	5.13	21.76

\*Proposed runoff shown in the table are the maximum outfalls from detention facilities or proposed sites.

The Los Angeles County Department of Public Works, Design Division provided a confirmation of the allowable flow rates that may be discharged to each of the downstream storm drains adjacent to the project site, refer to Appendix A for the summary noticed provided by the LACDPW.

Based on our preliminary post-developed hydrology calculations the following has been observed:

- The design outfall from the arena site detention facility and southerly portion of the west parking structure for Project 681 is approximately 14.30 cfs and the LACDPW allowable limit is 14.32 cfs.
- The design outfall from the northerly portion of the west parking structure facility for Project 4402, Line C is approximately 1.96 cfs and the LACDPW allowable limit is 2.31 cfs.
- The design outfall from the east parking structure and hotel detention facilities for DDI #8 is approximately 5.11 cfs and the LACDPW allowable limit is 5.13 cfs.

In summary, Project Condor will discharge 1.96 cfs and 14.30 cfs to Project 4402 & 681 and 5.11 cfs to DDI # 8, all discharge rates being within the allowable limits of 2.31cfs, 14.32 cfs and 5.13 cfs, respectively, as set by the LACDPW. Therefore, the existing downstream storm drain lines have adequate capacity for the proposed discharge from the project site. On-site storm drain pipelines and detention facilities should be designed to provide the capital flood level of protection from runoff from a 50-year frequency design storm.

The information contained within this report will be used for obtaining future connection permits to Los Angeles County Flood Control District (LACFCD) facilities and represents the existing hydrology and hydraulic data that will be used for future on-site storm drainage design.



## Figures

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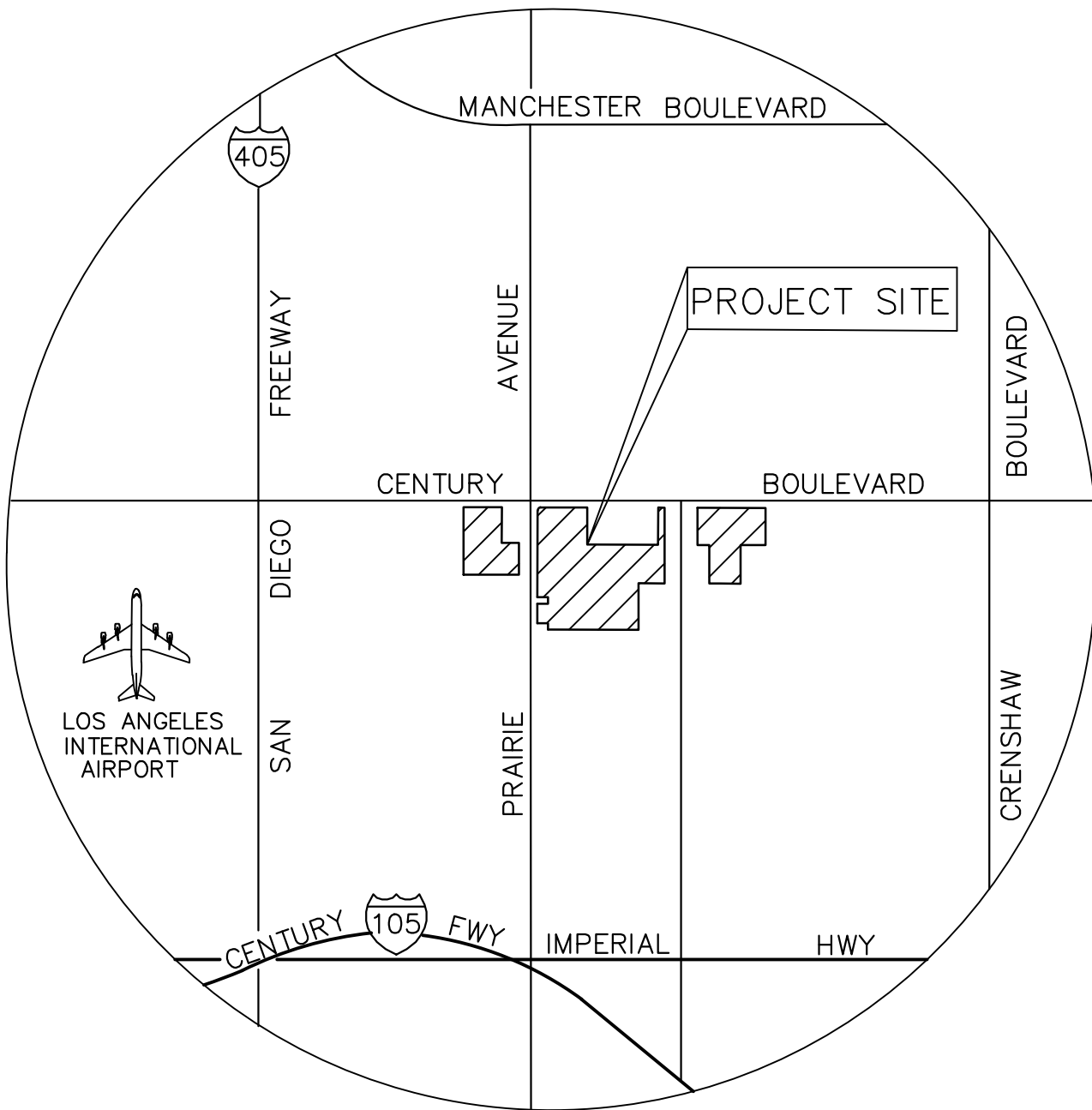
*Figure 1 — Vicinity Map*

*Figure 2 — Existing Storm Drains*

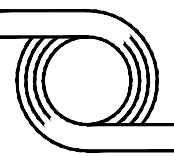
*Figure 3 — Pre-Development Hydrology Map*

*Figure 4 — Post-Development Hydrology Map*

*Figure 5 — Proposed Onsite Runoff Distribution to  
Existing Storm Drain Lines*



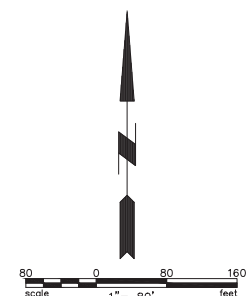
**FIGURE 1**

	<b>D &amp; D ENGINEERING, INC.</b> 8901 S. LA CIENEGA BLVD, SUITE 106 INGLEWOOD, CA 90301 Phone: 424-351-6800	<b>INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER</b>		SCALE: AS SHOWN
		<b>VICINITY MAP</b>		DATE: 05/01/19
				SHT NO.: 01 OF 01





- LEGEND**
- PROJECT STUDY LIMITS
  - EXISTING STORM DRAIN LINES
  - EXISTING CITY OF INGLEWOOD STORM DRAIN LINE




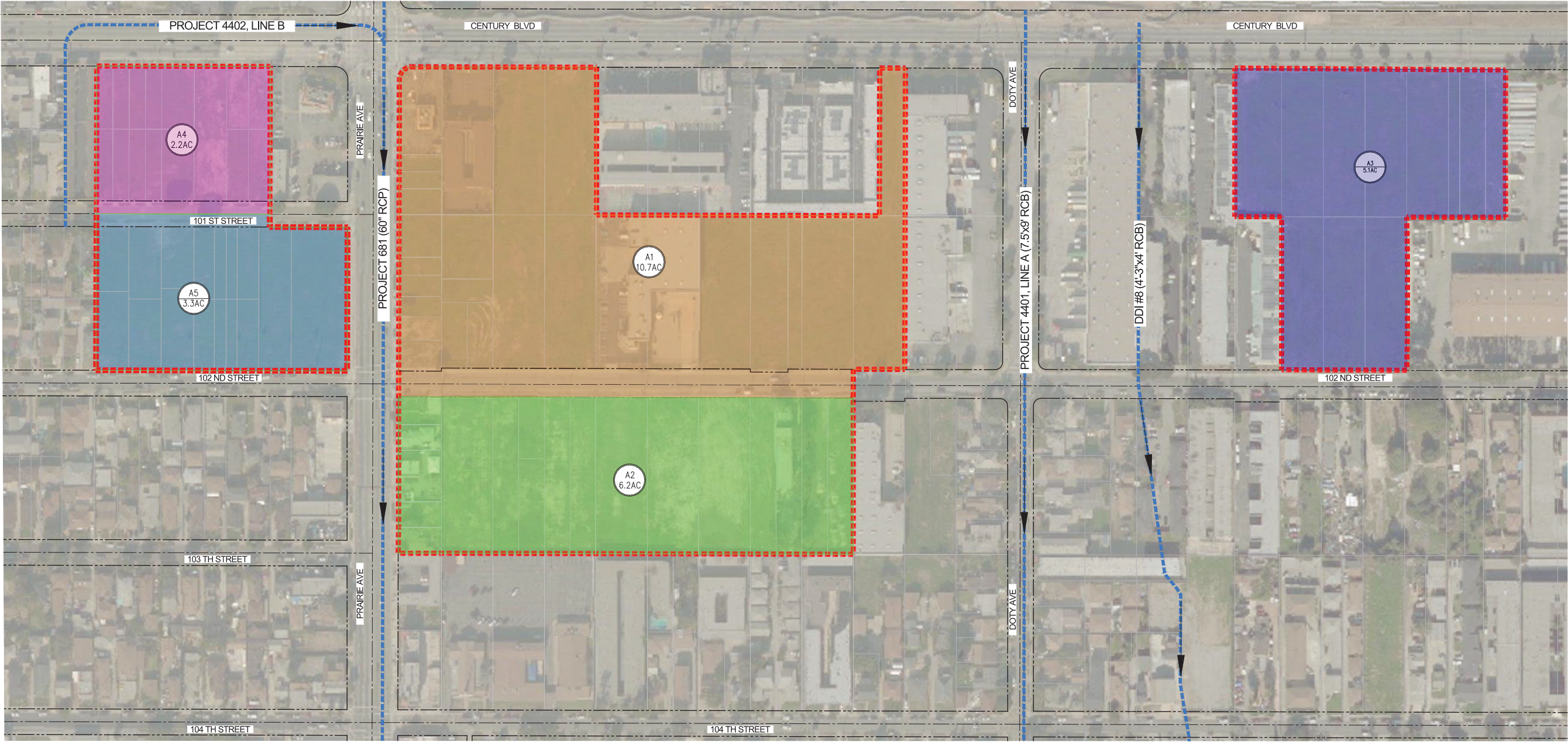
 <div>D &amp; D ENGINEERING, INC. 8901 S. LA CIENEGA BLVD, SUITE 106 INGLEWOOD, CA 90301 Phone: 424-351-6800</div>	INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER	
	EXISTING STORM DRAINS	
	SCALE: 1" = 80' DATE: 04/29/19 SHEET NO.: 1 OF 1	

FIGURE 2

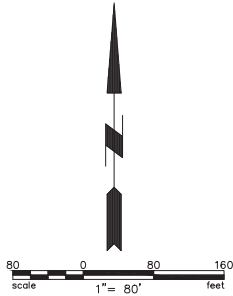





SUBAREA	ACREAGE	SOIL TYPE	LENGTH	SLOPE	Q2s
A1	10.7	16	965'	0.004	11.8 cfs
A2	6.2	16	910'	0.004	6.6 cfs
A3	5.1	13	685'	0.004	6.3 cfs
A4	3.3	16	427'	0.005	4.8 cfs
A5	2.2	16	600'	0.003	2.6 cfs
TOTAL	27.5	---	---	---	32.1 cfs

LEGEND

- PROJECT STUDY LIMITS
- EXISTING STORM DRAIN LINES
- AREA ACRES
- DRAINAGE SUBAREA





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INGLEWOOD, CA 90301  
Phone: 424-351-6800

INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER

PRE-DEVELOPMENT  
HYDROLOGY MAP

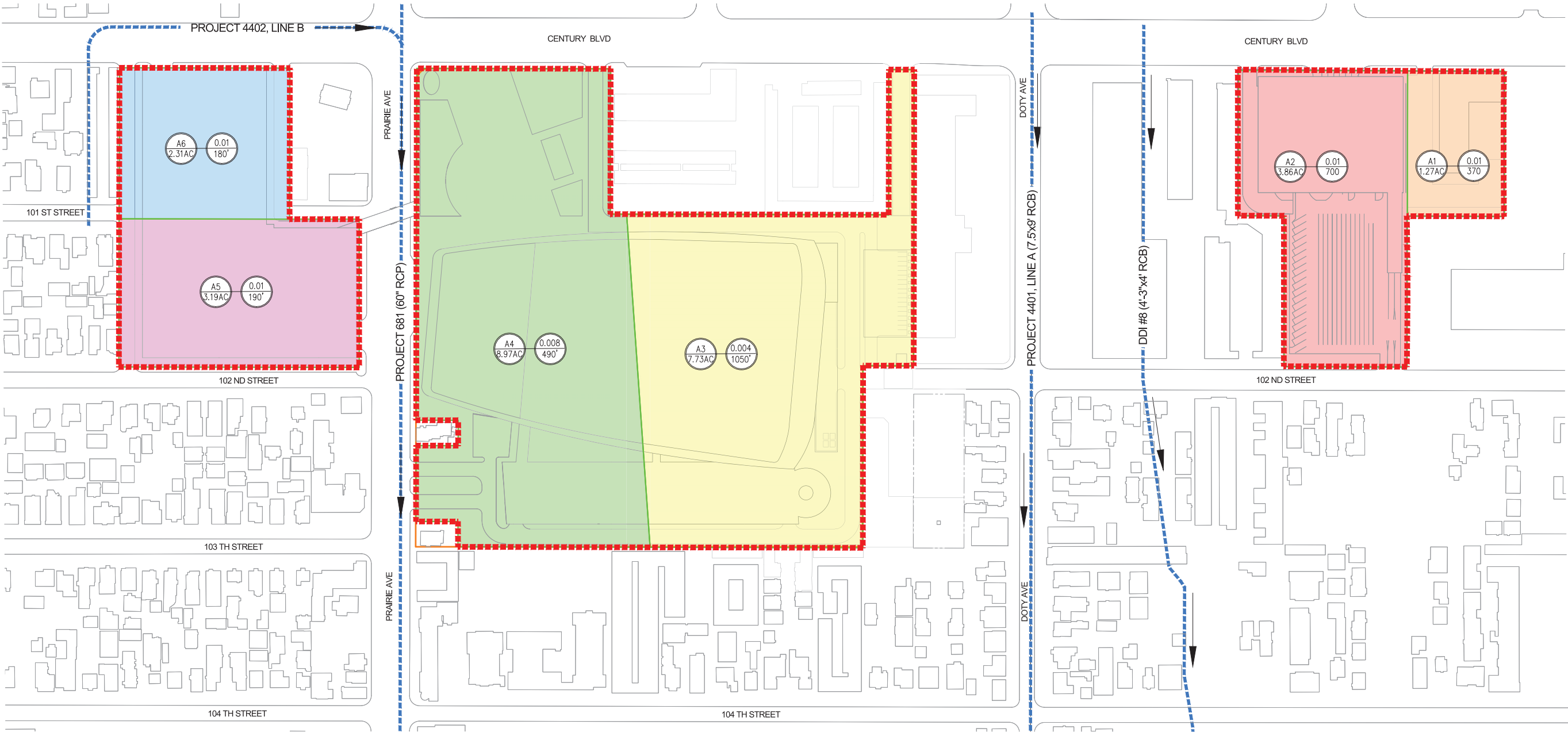
SCALE:  
1" = 80'

DATE:  
04/29/19

SHEET NO.:  
1 OF 1

FIGURE 3

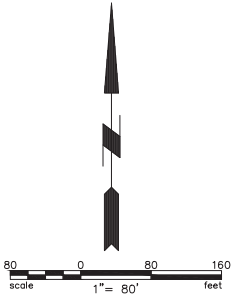




SUBAREA	ACREAGE [AC.]	LENGTH [FT.]	SLOPE	Q <sub>50</sub>
A1	1.3	370'	0.010	3.22 cfs
A2	3.9	700'	0.010	8.07 cfs
A3	7.7	1050'	0.004	13.06 cfs
A4	9.0	490'	0.008	19.79 cfs
A5	3.2	190'	0.010	8.78 cfs
A6	2.3	180'	0.010	6.36 cfs
TOTAL	27.4	---	---	59.28 cfs

**LEGEND**

- PROJECT STUDY LIMITS
  - EXISTING STORM DRAIN LINES
  - DRAINAGE AREA
- AREA ACRES      SLOPE LENGTH



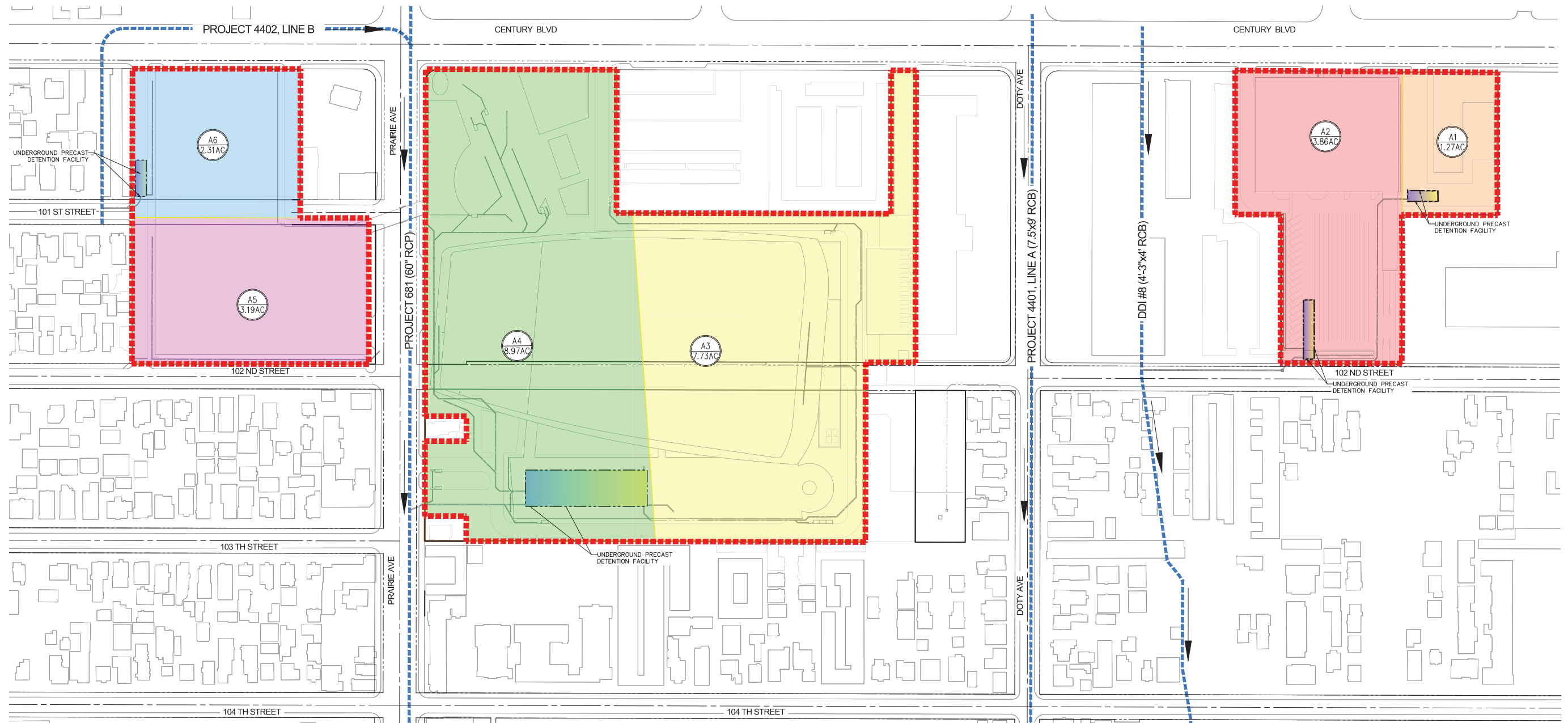
**D & D ENGINEERING, INC.**  
 8901 S. LA CIENEGA BLVD, SUITE 106  
 INGLEWOOD, CA 90301  
 Phone: 424-351-6800

**INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER**

**POST-DEVELOPMENT  
HYDROLOGY MAP**

SCALE:  
 1" = 80'  
 DATE:  
 04/29/19  
 SH. NO.:  
 1 OF 1

**FIGURE 4**



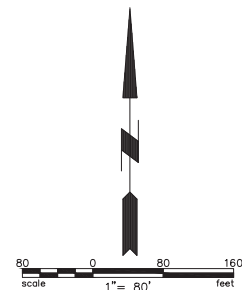
SUBAREA	ACREAGE [AC.]	LENGTH [FT.]	SLOPE	Q <sub>o</sub>
A1	1.3	370'	0.010	3.22 cfs
A2	3.9	700'	0.010	8.07 cfs
A3	7.7	1050'	0.004	13.06 cfs
A4	9.0	490'	0.008	19.79 cfs
A5	3.2	190'	0.010	8.78 cfs
A6	2.3	180'	0.010	6.36 cfs
TOTAL	27.4	---	---	59.28 cfs


EXISTING STORM DRAIN LINE	CONTRIBUTING ON-SITE DRAINAGE AREA	ALLOWABLE DISCHARGE TO EXISTING LINE [CFS/AC.]	TOTAL ALLOWABLE DISCHARGE TO EXISTING LINE [CFS]	PROPOSED Q <sub>50</sub> FLOW [CFS]	REQUIRED FLOW TO BE MITIGATED WITH STORAGE [CFS]	STORAGE PROVIDED [CF]	OUTFLOW [CFS]	NOTE
PROJECT DDI #8	A1 & A2	1.00	5.13	11.29	6.16	8900	5.11	SUFFICIENT SD CAPACITY
PROJECT 4402 LINE C	A6	1.00	2.31	6.36	4.05	5300	1.96	SUFFICIENT SD CAPACITY
PROJECT 681	A3, A4 & A5	0.72	14.32	41.63	27.31	100800	14.30	SUFFICIENT SD CAPACITY

\* TOTAL RUNOFF FROM DRAINAGE AREAS A3 & A4 DETENTION FACILITY OUTFALL OF 5.52 CFS AND DRAINAGE AREA A5 RUNOFF OF 8.78 CFS.

LEGEND

- PROJECT STUDY LIMITS
- EXISTING STORM DRAIN LINES
- DRAINAGE SUB-AREA





D & D ENGINEERING, INC.

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INGLEWOOD, CA 90301  
Phone: 424-351-6800

INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER

PROPOSED ONSITE RUNOFF  
DISTRIBUTION TO EXISTING STORM  
DRAIN LINES

SCALE:  
1" = 80'

DATE: 04/29/19

SHEET NO.: 1 OF 1

FIGURE 5



## **Appendix A**

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### ***Off-Site Hydrology and LACDOW Information Request Summary***

*Figure 2 — Existing Storm Drains*

*Offsite Tributary Area Map for Project 4402 & 681*

*Offsite Tributary Area Map for Project DDI #8*

*Information Request Summary*

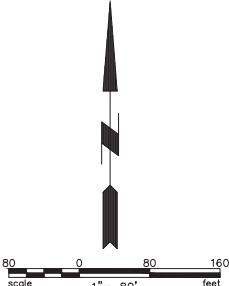







**LEGEND**

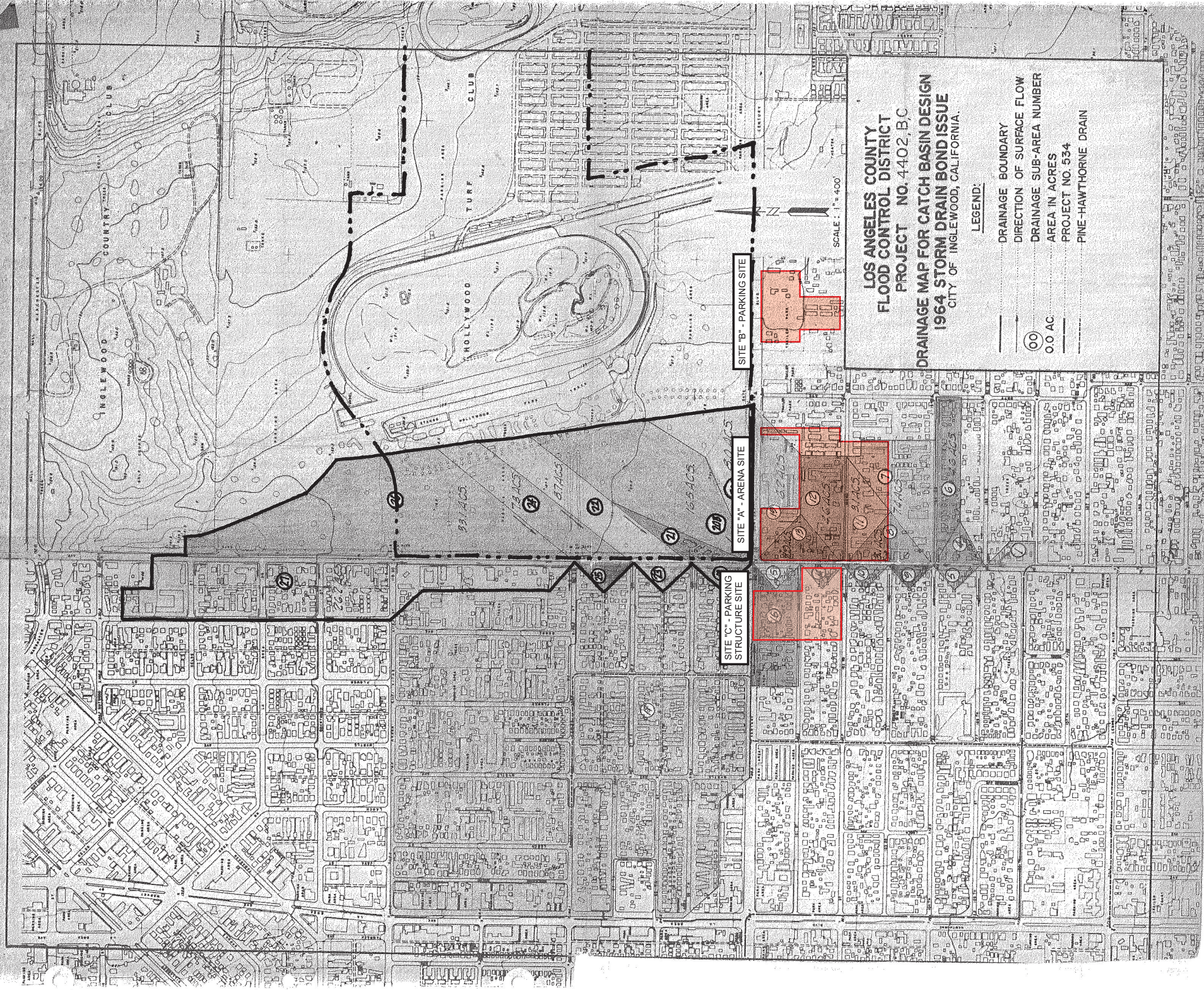
- PROJECT STUDY LIMITS
- EXISTING STORM DRAIN LINES
- EXISTING CITY OF INGLEWOOD STORM DRAIN LINE



 <div><b>D &amp; D ENGINEERING, INC.</b> 8901 S. LA CIENEGA BLVD, SUITE 106 INGLEWOOD, CA 90301 Phone: 424-351-6800</div>	<b>INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER</b>	
	<b>EXISTING STORM DRAINS</b>	
	SCALE: 1" = 80' DATE: 04/29/19 SHEET NO.: 1 OF 1	

**FIGURE 2**





LOS ANGELES COUNTY  
FLOOD CONTROL DISTRICT  
PROJECT NO. 4402, BC  
DRAINAGE MAP FOR CATCH BASIN DESIGN  
1964 STORM DRAIN BOND ISSUE  
CITY OF INGLEWOOD, CALIFORNIA.

- LEGEND:
- DRAINAGE BOUNDARY
  - DIRECTION OF SURFACE FLOW
  - DRAINAGE SUB-AREA NUMBER
  - 0.0 AC AREA IN ACRES
  - PROJECT NO. 534
  - PINE-HAWTHORNE DRAIN













Public Service That Works  
Issued By: 9/26/17  
Date: 9/26/17

Office Use Only	
<input type="checkbox"/> Sent	Initials: _____
<input type="checkbox"/> Fax <input checked="" type="checkbox"/> Email <input type="checkbox"/> Other:	_____
Date: _____	Time: _____

**LOS ANGELES COUNTY**  
**DEPARTMENT OF PUBLIC WORKS**  
**DESIGN DIVISION - HYDRAULIC ANALYSIS UNIT**

**INFORMATION REQUEST SUMMARY**

**INFORMATION REQUESTED BY**

\*Requester's Name: Boris Tantchev

Company: D & D Engineering, Inc.

\*Phone Number: 8182-653-8666 Fax Number: 424-393-4122

\*Email: BTantchev@DandDEngineeringInc.com

Method of Contact: ☐ Walk-in ☐ Phone ☐ Fax ☒ Email ☐ Prelim. Mtg. Date: 10/18/17

Intended Use: Research and Due Diligence

Proposed Project Type: Land Development - Mixed Use and Retail/Com Acreage Involved: 26

\*Will information be used in any litigation? ☐ YES ☒ NO

Case Info. Name: \_\_\_\_\_ No: \_\_\_\_\_ Location: \_\_\_\_\_

**INFORMATION REQUESTED (Attach Assessor Map)**

LACFCD Facility: Name: LACFCD Proj #681 and Proj #4401-U1 Line A, and DDI 0008

Unit: \_\_\_\_\_ Line: \_\_\_\_\_ Station: \_\_\_\_\_

City: Inglewood

\*Street/Cross-street: Century Blvd and Prairie Avenue

\*Thomas Guide: Page: 703 Grid: E5 ☒ Site Map/Plans Submitted

Info. Requested: Allowable Q

\*Required Information. See Page 2 of 2 for Instructions.

BELOW SECTION TO BE COMPLETED BY THE HYDRAULIC ANALYSIS UNIT

INFORMATION PROVIDED: Allowable q per acre.

REFERENCES SEARCHED: Projects 534, 4401, 4402 and DDI 8 Hydrology.

**COMMENTS, ETC:**

Allowable q per acre for connection to Project 4402 = 1.00 cfs.

Allowable q per acre for connection to Project 4401 = 0.70 cfs

Allowable q per acre for connection to DDI 8 = 1.00 cfs.

\* Allowable Discharge into Project 681 is limited to 0.72 cfs/acre.  
Revised on Project No 534 Hydrology.

INFORMATION PROVIDED BY: Ambrose C Ajaelo PE

Date: 10/26/2017

INFORMATION REVIEWED BY: George Aintablian

Date: 9/26/2018

Print

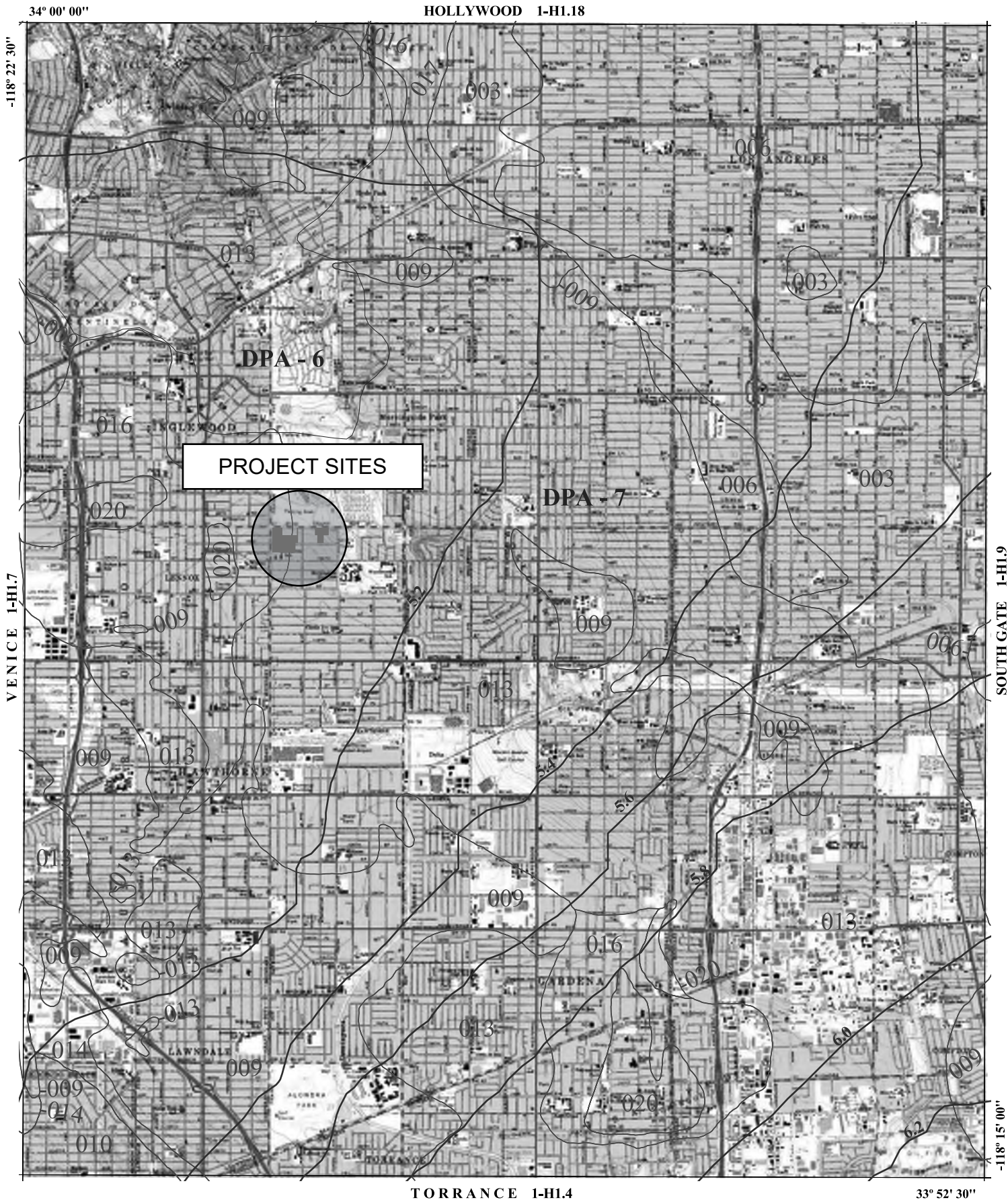
Save a Copy



## **Appendix B**

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*LACDPW, 2006 Hydrology Manual, Appendix B  
Hydrologic Maps, 08 Inglewood*



**016** SOIL CLASSIFICATION AREA

**7.2** INCHES OF RAINFALL

**DPA - 6** DEBRIS POTENTIAL AREA

1 0 1 2 Miles

25-YEAR 24-HOUR ISOHYET REDUCTION FACTOR: 0.878  
10-YEAR 24-HOUR ISOHYET REDUCTION FACTOR: 0.714

**INGLEWOOD**

**50-YEAR 24-HOUR ISOHYET**

**1-H1.8**





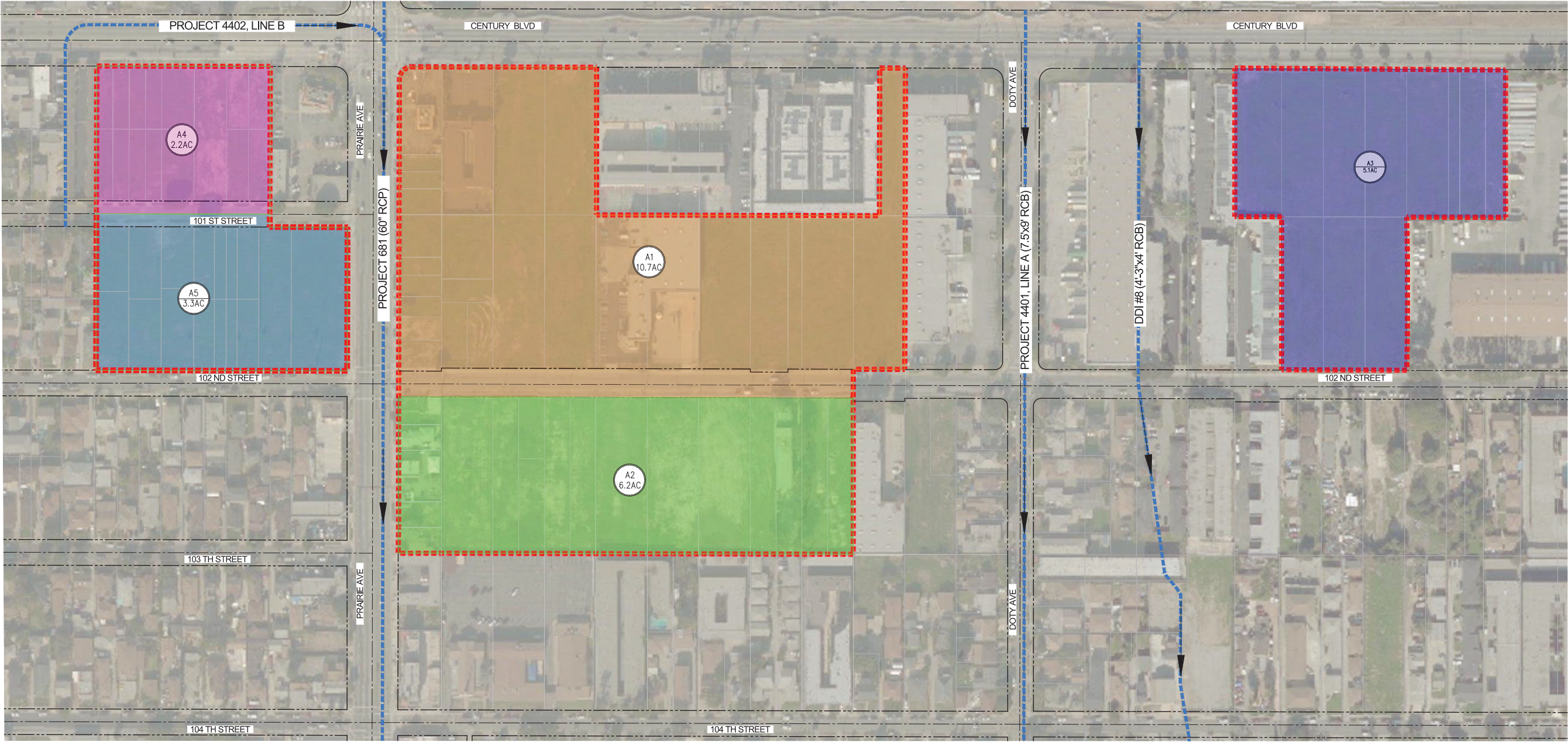
## **Appendix C**

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### ***Pre-Development Runoff Calculations***

*Figure 3 — Pre-Development Hydrology Map  
Sub-areas HydroCalc Worksheets*

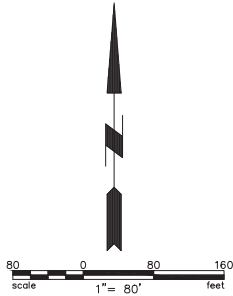





SUBAREA	ACREAGE	SOIL TYPE	LENGTH	SLOPE	Q2s
A1	10.7	16	965'	0.004	11.8 cfs
A2	6.2	16	910'	0.004	6.6 cfs
A3	5.1	13	685'	0.004	6.3 cfs
A4	3.3	16	427'	0.005	4.8 cfs
A5	2.2	16	600'	0.003	2.6 cfs
TOTAL	27.5	---	---	---	32.1 cfs

LEGEND

- PROJECT STUDY LIMITS
- EXISTING STORM DRAIN LINES
- AREA ACRES
- DRAINAGE SUBAREA





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8901 S. LA CIENEGA BLVD., SUITE 106  
INGLEWOOD, CA 90301  
Phone: 424-351-6800

INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER

PRE-DEVELOPMENT  
HYDROLOGY MAP

SCALE:  
1" = 80'

DATE:  
04/29/19

SHEET NO.:  
1 OF 1

FIGURE 3



## Peak Flow Hydrologic Analysis

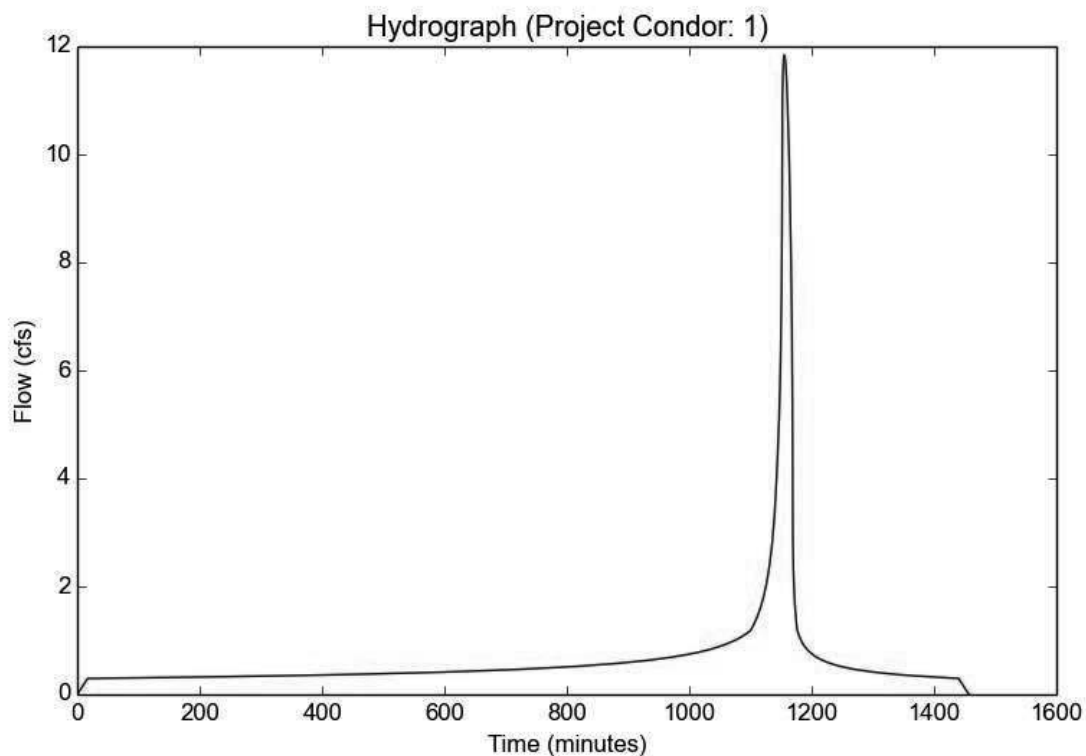
File location: M:/17001/Eng/17001/Hm/Hydrology/Conceptual Hydrocalc/EIR/Project Condor Existing Drainage Area Report.pdf  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	1
Area (ac)	10.7
Flow Path Length (ft)	965.0
Flow Path Slope (vft/hft)	0.004
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.22
Soil Type	16
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

### Output Results

Modeled (25-yr) Rainfall Depth (in)	4.5217
Peak Intensity (in/hr)	1.5178
Undeveloped Runoff Coefficient (Cu)	0.6806
Developed Runoff Coefficient (Cd)	0.7289
Time of Concentration (min)	17.0
Clear Peak Flow Rate (cfs)	11.8372
Burned Peak Flow Rate (cfs)	11.8372
24-Hr Clear Runoff Volume (ac-ft)	1.3194
24-Hr Clear Runoff Volume (cu-ft)	57473.0735



## Peak Flow Hydrologic Analysis

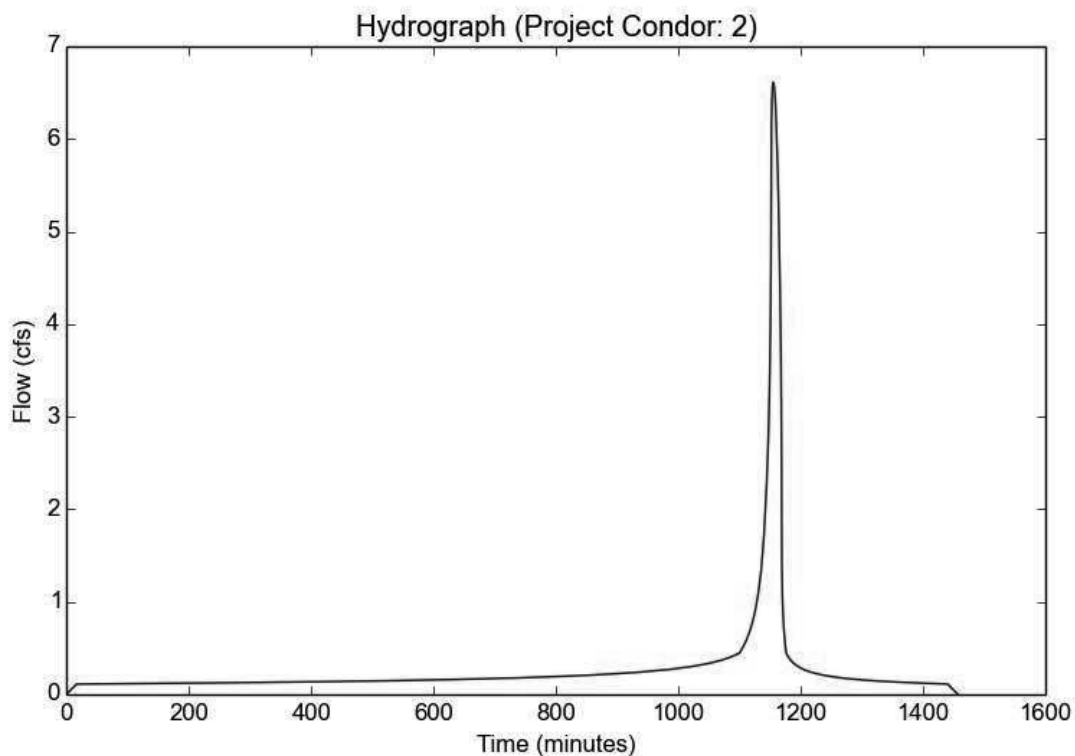
File location: M:/17001/Eng/17001/Hm/Hydrology/Conceptual Hydrocalc/EIR/Project Condor Existing Drainage Area Report.pdf  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	2
Area (ac)	6.2
Flow Path Length (ft)	910.0
Flow Path Slope (vft/hft)	0.004
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.1
Soil Type	16
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

### Output Results

Modeled (25-yr) Rainfall Depth (in)	4.5217
Peak Intensity (in/hr)	1.5178
Undeveloped Runoff Coefficient (Cu)	0.6806
Developed Runoff Coefficient (Cd)	0.7026
Time of Concentration (min)	17.0
Clear Peak Flow Rate (cfs)	6.6112
Burned Peak Flow Rate (cfs)	6.6112
24-Hr Clear Runoff Volume (ac-ft)	0.5613
24-Hr Clear Runoff Volume (cu-ft)	24451.3721





## Peak Flow Hydrologic Analysis

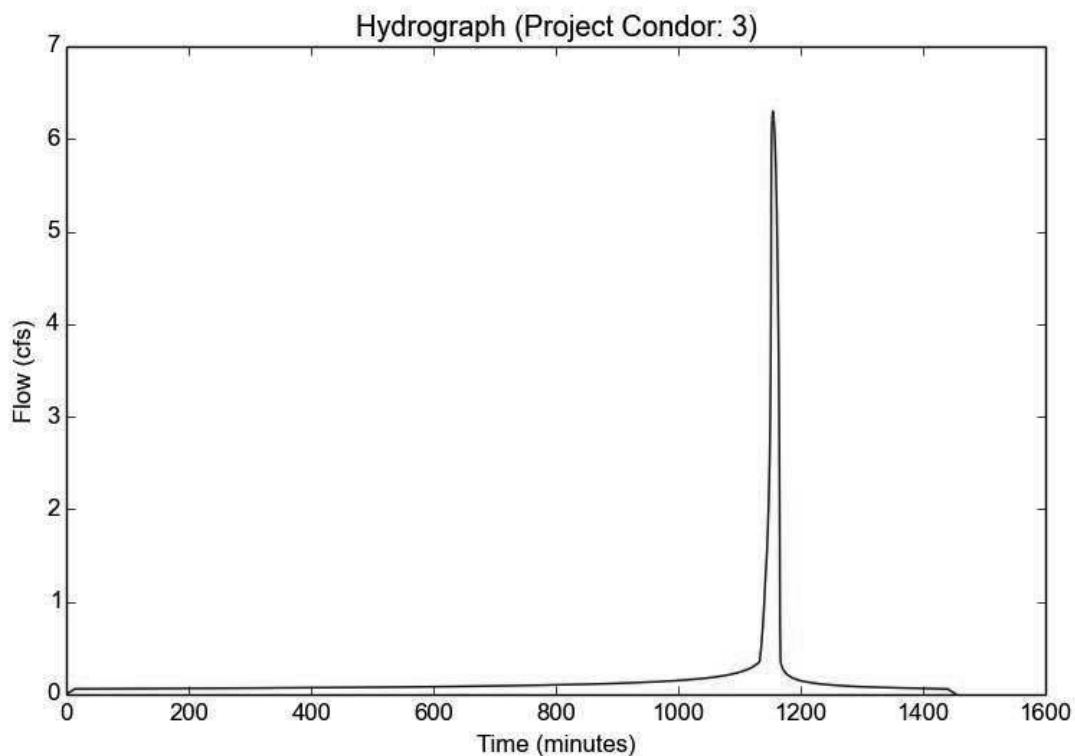
File location: M:/17001/Eng/17001/Hm/Hydrology/Conceptual Hydrocalc/EIR/Project Condor Existing Drainage Area Report.pdf  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	3
Area (ac)	5.1
Flow Path Length (ft)	685.0
Flow Path Slope (vft/hft)	0.004
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.02
Soil Type	13
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

### Output Results

Modeled (25-yr) Rainfall Depth (in)	4.5217
Peak Intensity (in/hr)	1.6628
Undeveloped Runoff Coefficient (Cu)	0.7394
Developed Runoff Coefficient (Cd)	0.7426
Time of Concentration (min)	14.0
Clear Peak Flow Rate (cfs)	6.2979
Burned Peak Flow Rate (cfs)	6.2979
24-Hr Clear Runoff Volume (ac-ft)	0.3313
24-Hr Clear Runoff Volume (cu-ft)	14431.2809



## Peak Flow Hydrologic Analysis

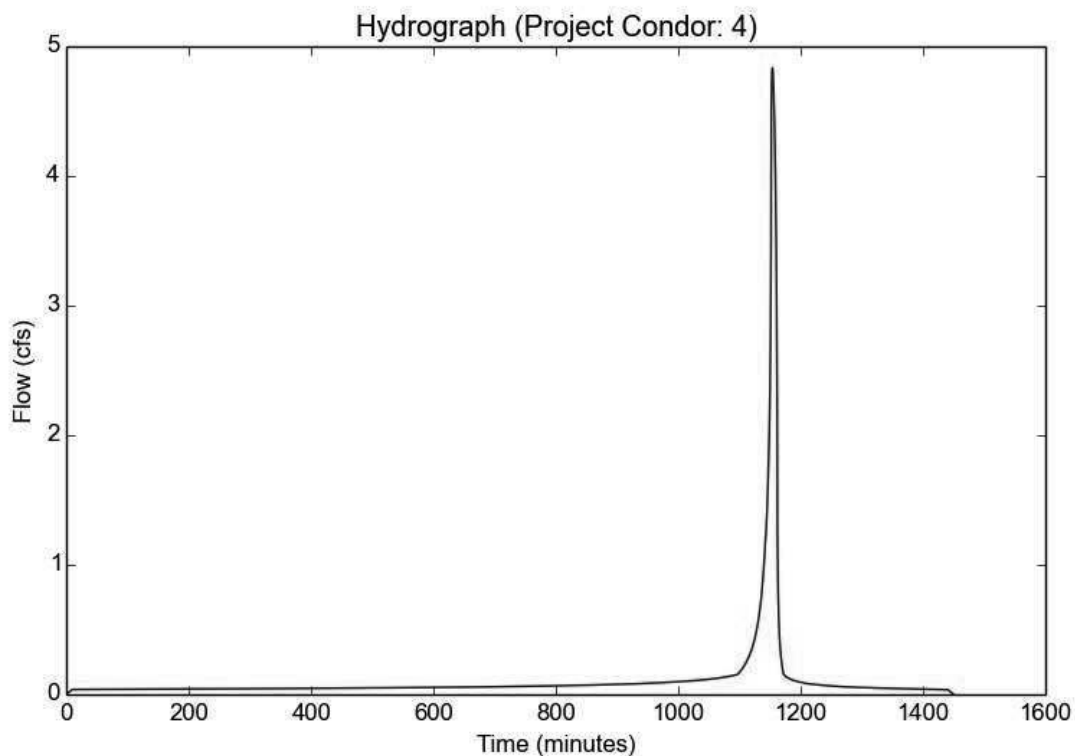
File location: M:/17001/Eng/17001/Hm/Hydrology/Conceptual Hydrocalc/EIR/Project Condor Existing Drainage Area Report.pdf  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	4
Area (ac)	3.3
Flow Path Length (ft)	427.0
Flow Path Slope (vft/hft)	0.0047
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.02
Soil Type	16
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

### Output Results

Modeled (25-yr) Rainfall Depth (in)	4.5217
Peak Intensity (in/hr)	1.9477
Undeveloped Runoff Coefficient (Cu)	0.749
Developed Runoff Coefficient (Cd)	0.752
Time of Concentration (min)	10.0
Clear Peak Flow Rate (cfs)	4.8336
Burned Peak Flow Rate (cfs)	4.8336
24-Hr Clear Runoff Volume (ac-ft)	0.2283
24-Hr Clear Runoff Volume (cu-ft)	9945.7762



## Peak Flow Hydrologic Analysis

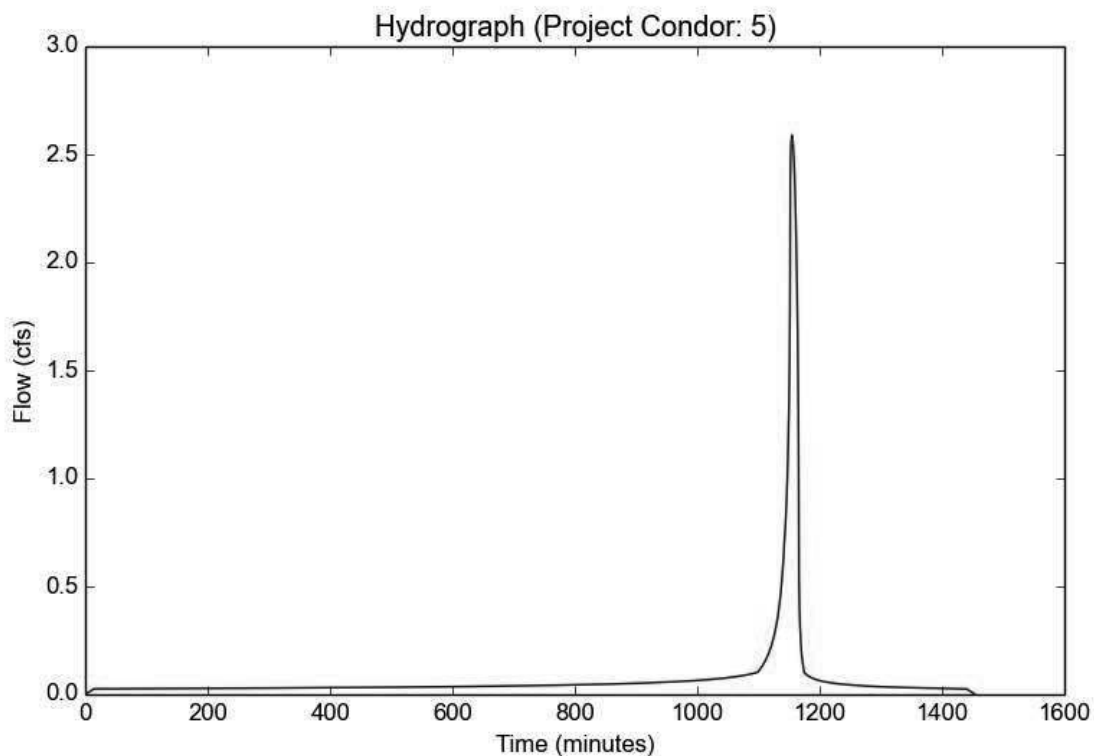
File location: M:/17001/Eng/17001/Hm/Hydrology/Conceptual Hydrocalc/EIR/Project Condor Existing Drainage Area Report.pdf  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	5
Area (ac)	2.2
Flow Path Length (ft)	600.0
Flow Path Slope (vft/hft)	0.003
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.02
Soil Type	16
Design Storm Frequency	25-yr
Fire Factor	0
LID	False

### Output Results

Modeled (25-yr) Rainfall Depth (in)	4.5217
Peak Intensity (in/hr)	1.6628
Undeveloped Runoff Coefficient (Cu)	0.7037
Developed Runoff Coefficient (Cd)	0.7076
Time of Concentration (min)	14.0
Clear Peak Flow Rate (cfs)	2.5886
Burned Peak Flow Rate (cfs)	2.5886
24-Hr Clear Runoff Volume (ac-ft)	0.1516
24-Hr Clear Runoff Volume (cu-ft)	6601.9462





## **Appendix D**

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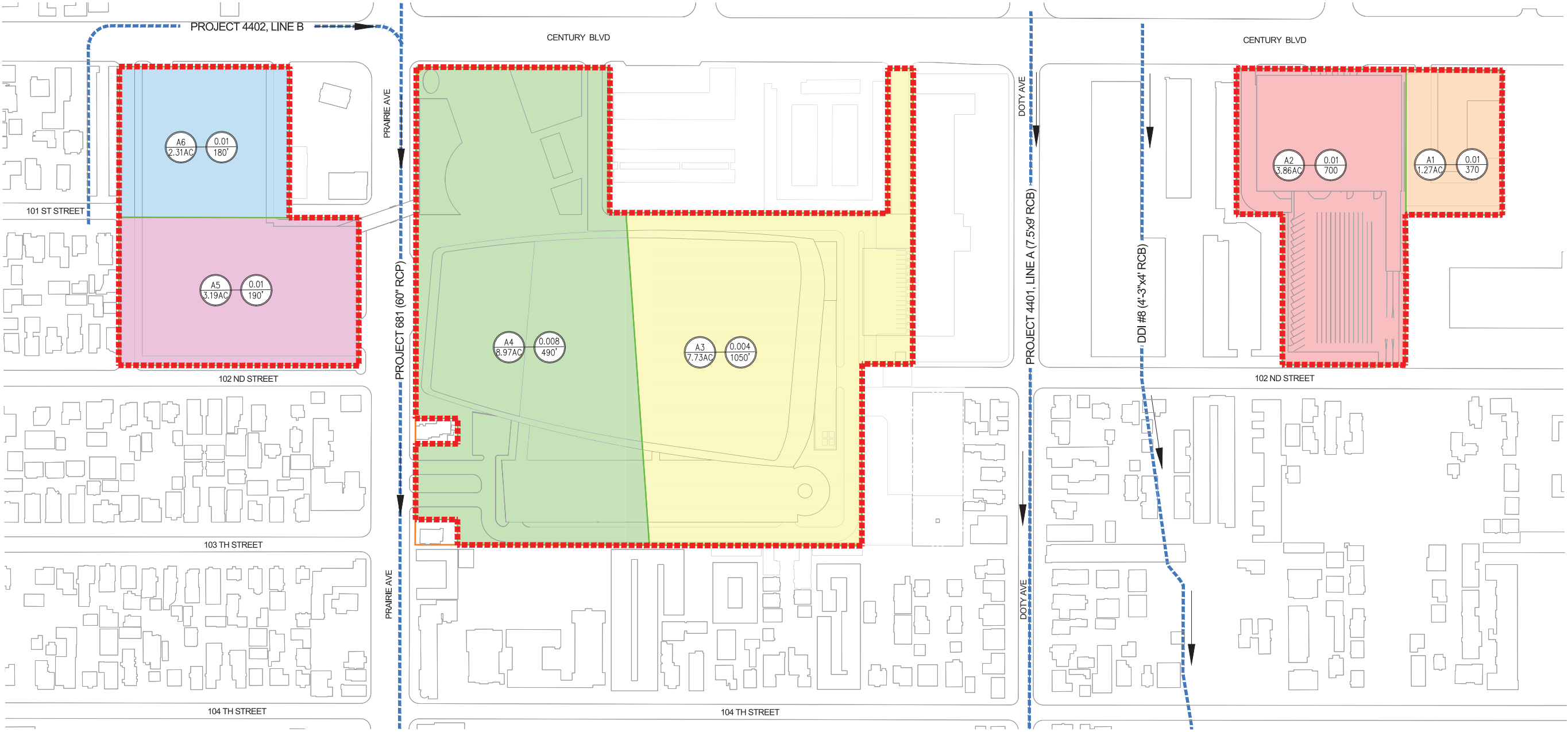
### ***Post-Development Runoff Calculations and Basin Routing***

*Figure 4 — Post-Development Hydrology Map*

*Figure 5 — Proposed Onsite Runoff Distribution to Existing Storm Drain Lines*

*Sub-Areas HydroCalc Worksheets*

*Summary of Post-Development Runoff Distribution to Existing Storm Drain Systems*



SUBAREA	ACREAGE [AC.]	LENGTH [FT.]	SLOPE	Q <sub>50</sub>
A1	1.3	370'	0.010	3.22 cfs
A2	3.9	700'	0.010	8.07 cfs
A3	7.7	1050'	0.004	13.06 cfs
A4	9.0	490'	0.008	19.79 cfs
A5	3.2	190'	0.010	8.78 cfs
A6	2.3	180'	0.010	6.36 cfs
TOTAL	27.4	---	---	59.28 cfs

**LEGEND**

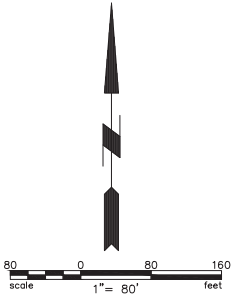
PROJECT STUDY LIMITS


EXISTING STORM DRAIN LINES

DRAINAGE AREA

AREA  
ACRES

SLOPE  
LENGTH





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INGLEWOOD, CA 90301  
Phone: 424-351-6800

**INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER**

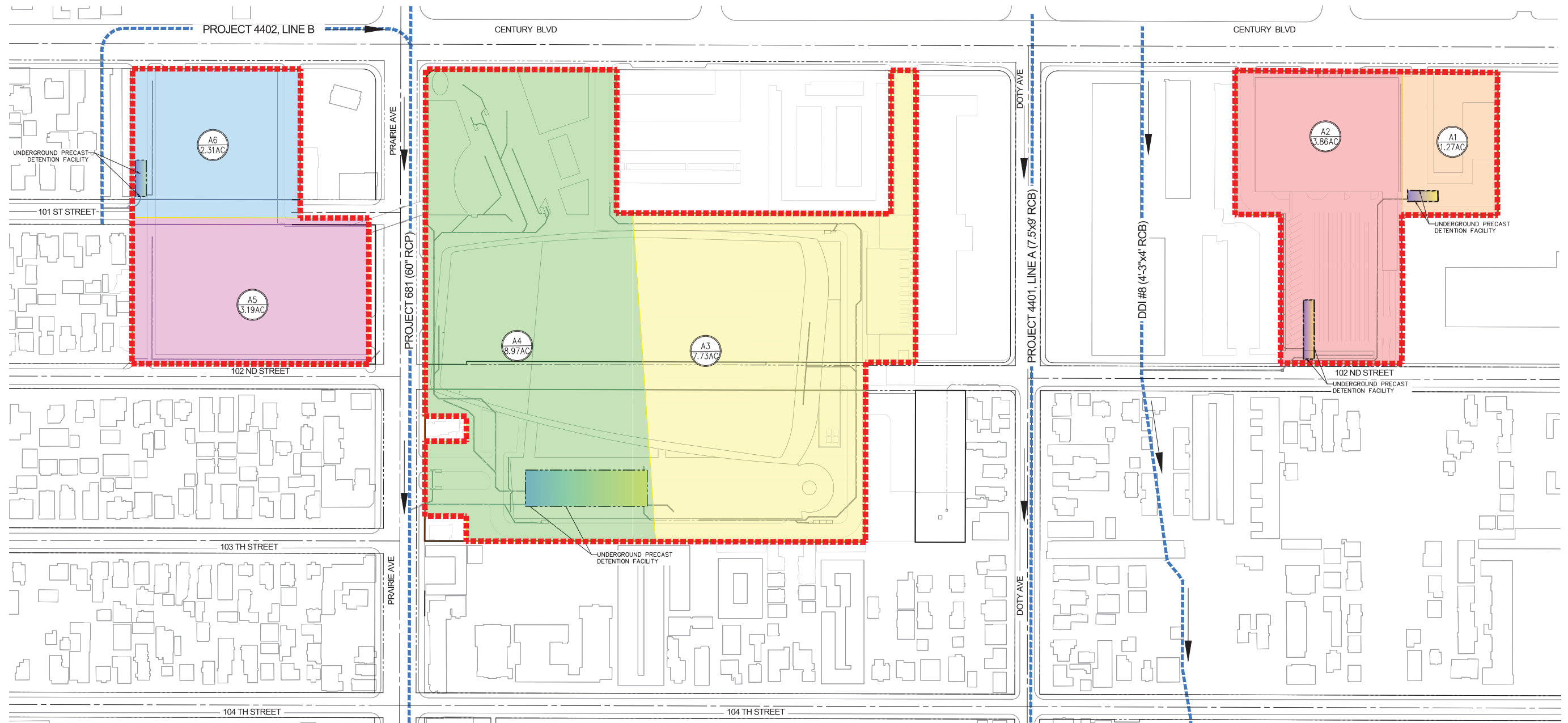
**POST-DEVELOPMENT  
HYDROLOGY MAP**

SCALE:  
1" = 80'

DATE:  
04/29/19

SHEET NO.:  
1 OF 1

FIGURE 4



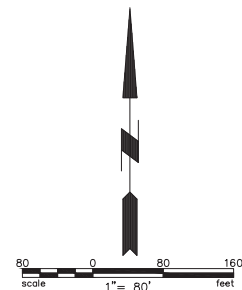
SUBAREA	ACREAGE [AC.]	LENGTH [FT.]	SLOPE	Q <sub>o</sub>
A1	1.3	370'	0.010	3.22 cfs
A2	3.9	700'	0.010	8.07 cfs
A3	7.7	1050'	0.004	13.06 cfs
A4	9.0	490'	0.008	19.79 cfs
A5	3.2	190'	0.010	8.78 cfs
A6	2.3	180'	0.010	6.36 cfs
TOTAL	27.4	---	---	59.28 cfs


EXISTING STORM DRAIN LINE	CONTRIBUTING ON-SITE DRAINAGE AREA	ALLOWABLE DISCHARGE TO EXISTING LINE [CFS/AC.]	TOTAL ALLOWABLE DISCHARGE TO EXISTING LINE [CFS]	PROPOSED Q <sub>50</sub> FLOW [CFS]	REQUIRED FLOW TO BE MITIGATED WITH STORAGE [CFS]	STORAGE PROVIDED [CF]	OUTFLOW [CFS]	NOTE
PROJECT DDI #8	A1 & A2	1.00	5.13	11.29	6.16	8900	5.11	SUFFICIENT SD CAPACITY
PROJECT 4402 LINE C	A6	1.00	2.31	6.36	4.05	5300	1.96	SUFFICIENT SD CAPACITY
PROJECT 681	A3, A4 & A5	0.72	14.32	41.63	27.31	100800	14.30	SUFFICIENT SD CAPACITY

\* TOTAL RUNOFF FROM DRAINAGE AREAS A3 & A4 DETENTION FACILITY OUTFALL OF 5.52 CFS AND DRAINAGE AREA A5 RUNOFF OF 8.78 CFS.

LEGEND

- PROJECT STUDY LIMITS
- EXISTING STORM DRAIN LINES
- DRAINAGE SUB-AREA





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INGLEWOOD, CA 90301  
Phone: 424-351-6800

INGLEWOOD BASKETBALL AND ENTERTAINMENT CENTER

PROPOSED ONSITE RUNOFF  
DISTRIBUTION TO EXISTING STORM  
DRAIN LINES

SCALE:  
1" = 80'

DATE:  
04/29/19

SHEET NO.:  
1 OF 1

FIGURE 5

## Peak Flow Hydrologic Analysis

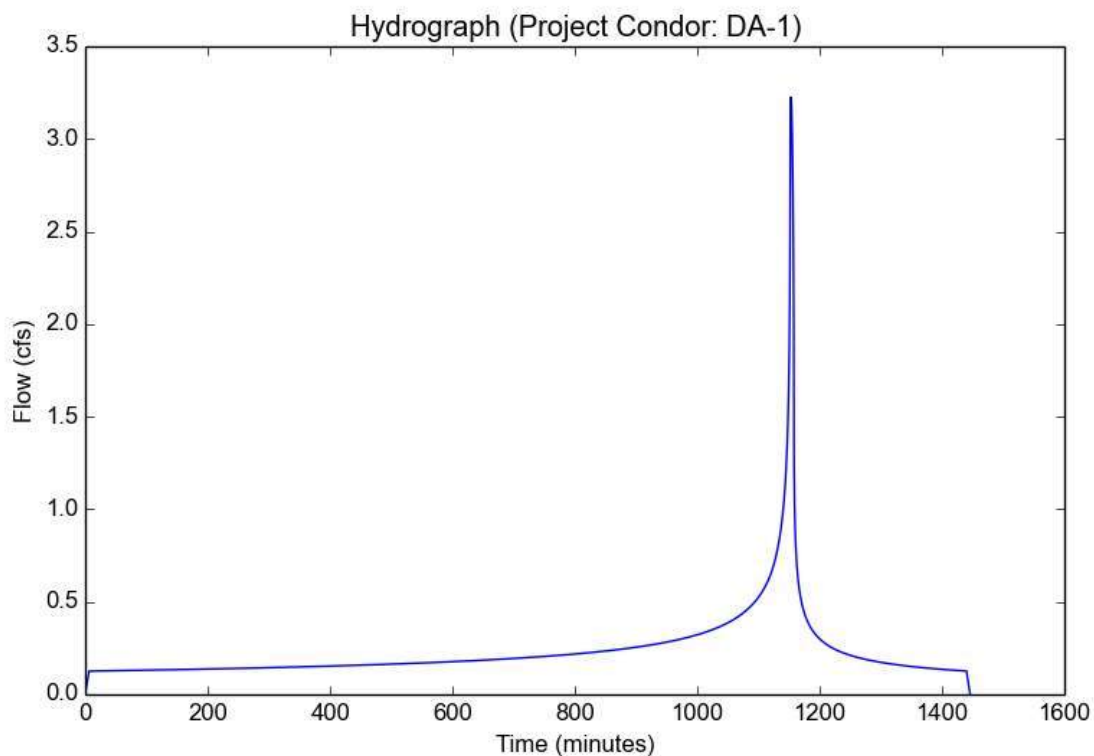
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-1
Area (ac)	1.27
Flow Path Length (ft)	370.0
Flow Path Slope (vft/hft)	0.01
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.96
Soil Type	13
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	2.8203
Undeveloped Runoff Coefficient (Cu)	0.9139
Developed Runoff Coefficient (Cd)	0.9
Time of Concentration (min)	6.0
Clear Peak Flow Rate (cfs)	3.2236
Burned Peak Flow Rate (cfs)	3.2236
24-Hr Clear Runoff Volume (ac-ft)	0.4707
24-Hr Clear Runoff Volume (cu-ft)	20505.3648



## Peak Flow Hydrologic Analysis

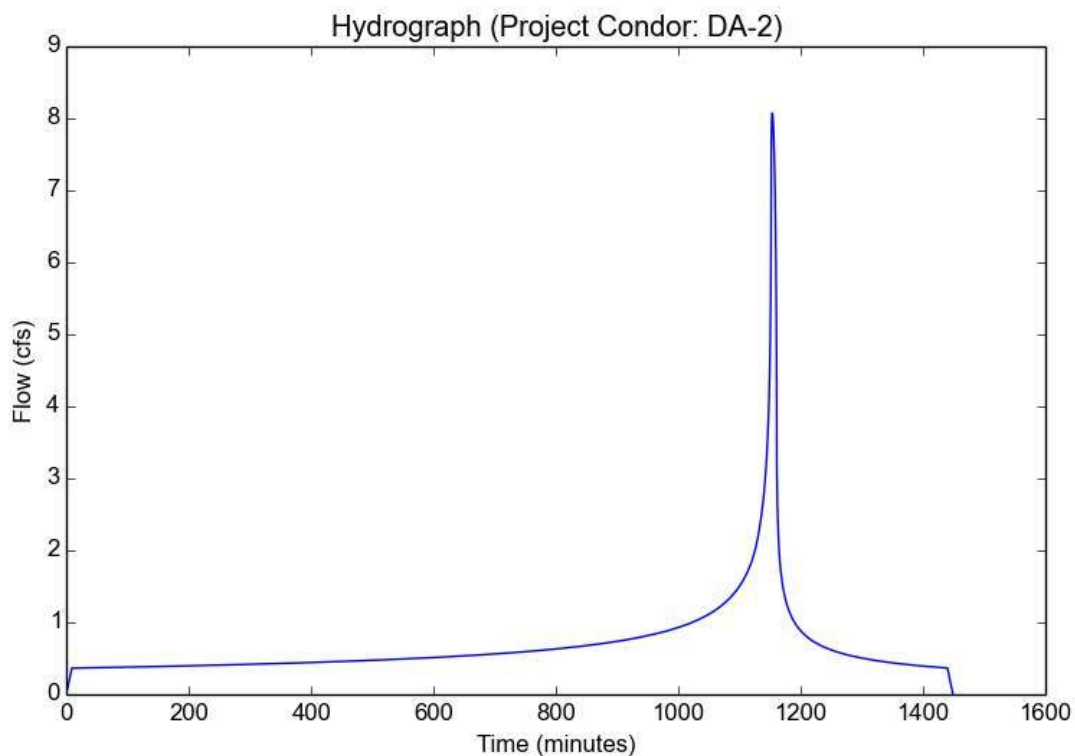
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-2
Area (ac)	3.86
Flow Path Length (ft)	700.0
Flow Path Slope (vft/hft)	0.01
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.91
Soil Type	13
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	2.3309
Undeveloped Runoff Coefficient (Cu)	0.8687
Developed Runoff Coefficient (Cd)	0.8972
Time of Concentration (min)	9.0
Clear Peak Flow Rate (cfs)	8.0724
Burned Peak Flow Rate (cfs)	8.0724
24-Hr Clear Runoff Volume (ac-ft)	1.3709
24-Hr Clear Runoff Volume (cu-ft)	59716.2134





## Peak Flow Hydrologic Analysis

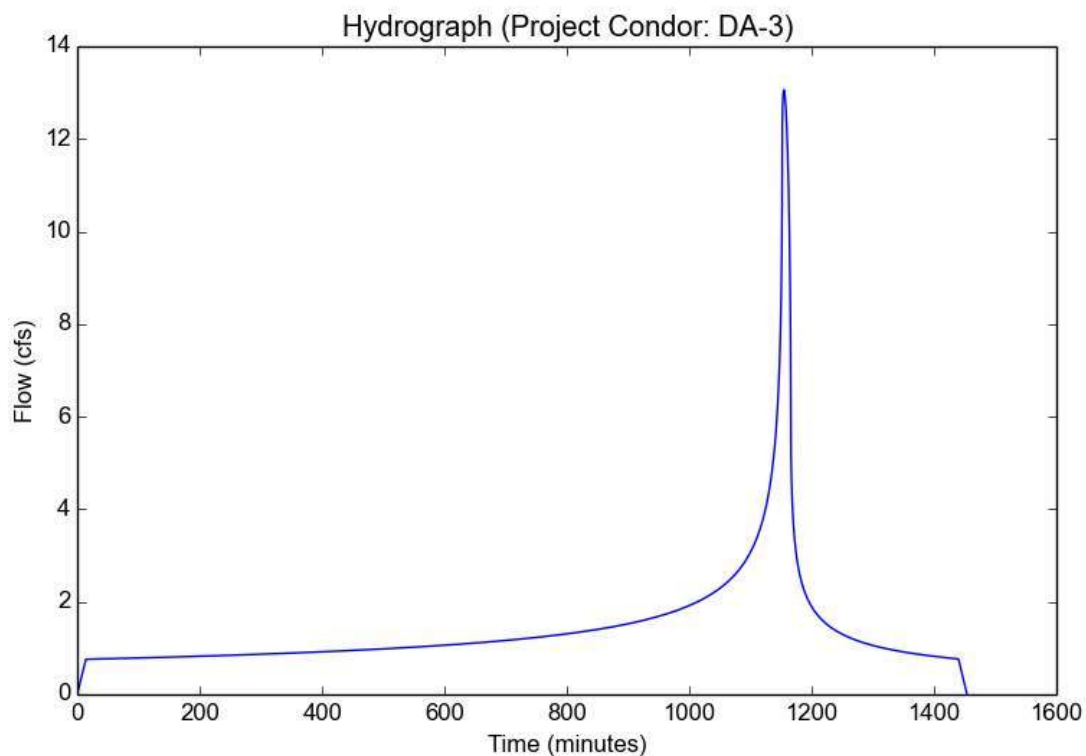
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-3
Area (ac)	7.73
Flow Path Length (ft)	1050.0
Flow Path Slope (vft/hft)	0.004
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.95
Soil Type	16
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	1.8939
Undeveloped Runoff Coefficient (Cu)	0.7404
Developed Runoff Coefficient (Cd)	0.892
Time of Concentration (min)	14.0
Clear Peak Flow Rate (cfs)	13.0587
Burned Peak Flow Rate (cfs)	13.0587
24-Hr Clear Runoff Volume (ac-ft)	2.8429
24-Hr Clear Runoff Volume (cu-ft)	123834.7286



## Peak Flow Hydrologic Analysis

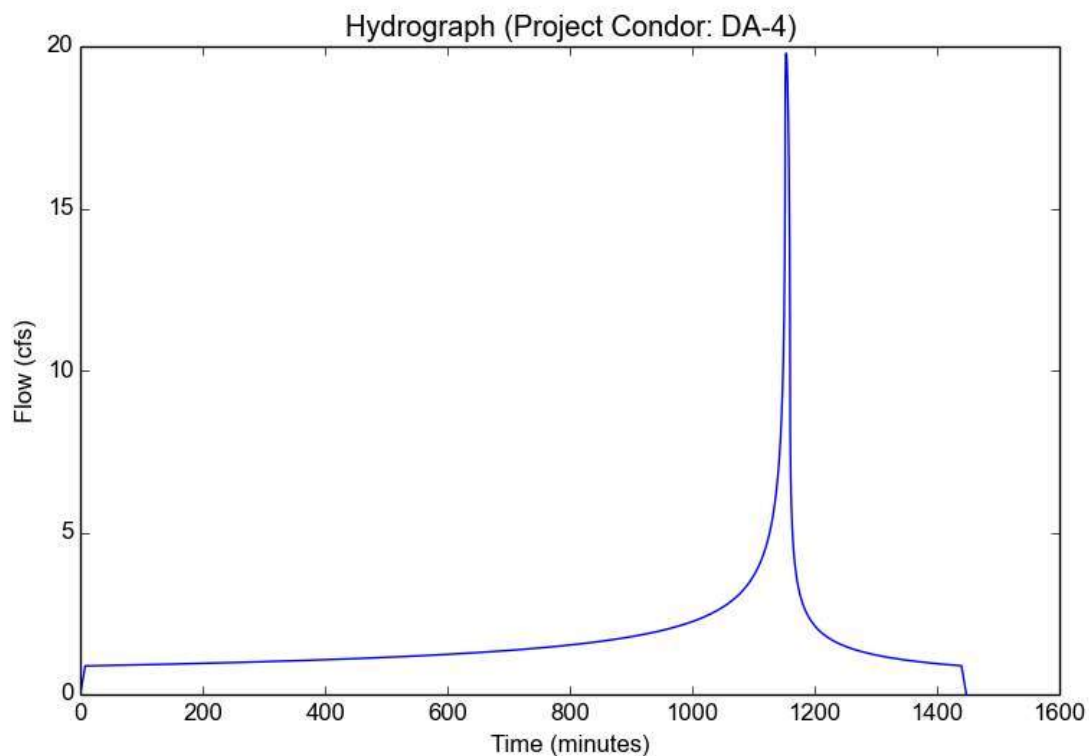
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-4
Area (ac)	8.97
Flow Path Length (ft)	490.0
Flow Path Slope (vft/hft)	0.008
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.95
Soil Type	16
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	2.4636
Undeveloped Runoff Coefficient (Cu)	0.8069
Developed Runoff Coefficient (Cd)	0.8953
Time of Concentration (min)	8.0
Clear Peak Flow Rate (cfs)	19.7859
Burned Peak Flow Rate (cfs)	19.7859
24-Hr Clear Runoff Volume (ac-ft)	3.2991
24-Hr Clear Runoff Volume (cu-ft)	143708.9552



## Peak Flow Hydrologic Analysis

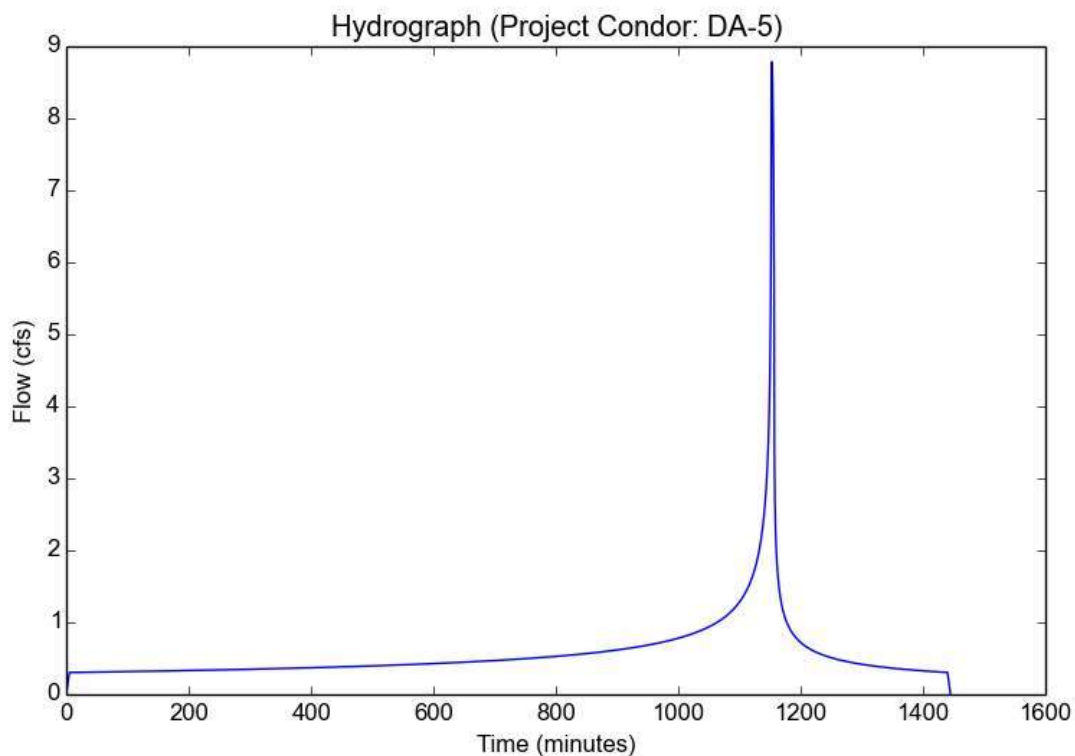
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-5
Area (ac)	3.19
Flow Path Length (ft)	190.0
Flow Path Slope (vft/hft)	0.01
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.92
Soil Type	16
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	3.0726
Undeveloped Runoff Coefficient (Cu)	0.8531
Developed Runoff Coefficient (Cd)	0.8962
Time of Concentration (min)	5.0
Clear Peak Flow Rate (cfs)	8.7848
Burned Peak Flow Rate (cfs)	8.7848
24-Hr Clear Runoff Volume (ac-ft)	1.1441
24-Hr Clear Runoff Volume (cu-ft)	49837.1138



## Peak Flow Hydrologic Analysis

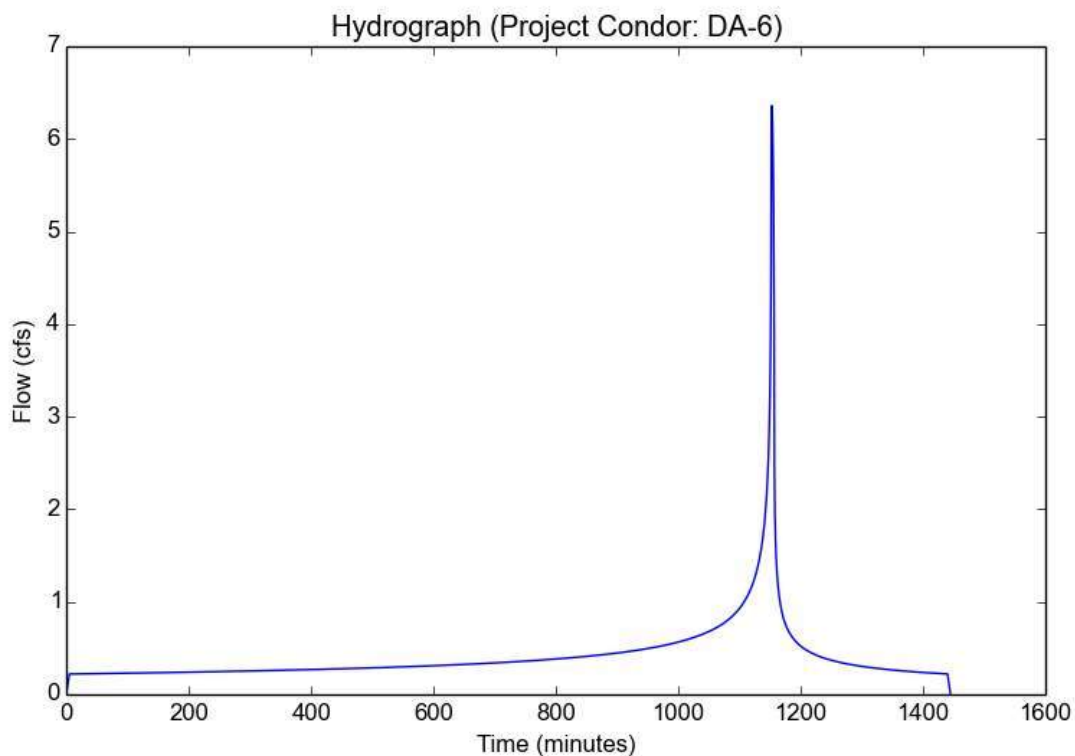
File location: M:/17001/Admin/17001-100/Reports/03\_Third round fo the reports March 2019/Hydrology/Calculations/Project Condor Proposed Drainage  
Version: HydroCalc 1.0.2

### Input Parameters

Project Name	Project Condor
Subarea ID	DA-6
Area (ac)	2.31
Flow Path Length (ft)	180.0
Flow Path Slope (vft/hft)	0.01
50-yr Rainfall Depth (in)	5.15
Percent Impervious	0.92
Soil Type	16
Design Storm Frequency	50-yr
Fire Factor	0
LID	False

### Output Results

Modeled (50-yr) Rainfall Depth (in)	5.15
Peak Intensity (in/hr)	3.0726
Undeveloped Runoff Coefficient (Cu)	0.8531
Developed Runoff Coefficient (Cd)	0.8962
Time of Concentration (min)	5.0
Clear Peak Flow Rate (cfs)	6.3614
Burned Peak Flow Rate (cfs)	6.3614
24-Hr Clear Runoff Volume (ac-ft)	0.8285
24-Hr Clear Runoff Volume (cu-ft)	36088.9445



EXISTING STORM DRAIN LINE	CONTRIBUTING ON-SITE DRAINAGE AREA	ALLOWABLE DISCHARGE TO EXISTING LINE [CFS/AC.]	TOTAL ALLOWABLE DISCHARGE TO EXISTING LINE [CFS]	PROPOSED Q <sub>50</sub> FLOW [CFS]	REQUIRED FLOW TO BE MITIGATED WITH STORAGE [CFS]	STORAGE PROVIDED [CF]	OUTFLOW [CFS]	NOTE
PROJECT DDI #8	A1 & A2	1.00	5.13	11.29	6.16	8900	5.11	SUFFICIENT SD CAPACITY
PROJECT 4402 LINE C	A6	1.00	2.31	6.36	4.05	5300	1.96	SUFFICIENT SD CAPACITY
PROJECT 681	A3, A4 & A5	0.72	14.32	41.63	27.31	100800	14.30	SUFFICIENT SD CAPACITY

\* TOTAL RUNOFF FROM DRAINAGE AREAS A3 & A4 DETENTION FACILITY  
OUTFALL OF 5.52 CFS AND DRAINAGE AREA A5 RUNOFF OF 8.78 CFS.



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## **Appendix E**

---

### ***LA County As-Built Plans***

*LACDPW Project 4402 & 681 As Built Plans*

*LACDPW Project 4401, Line A As Built Plans*

*LACDPW DDI # 8 As Built Plans*





# LEGEND & ABBREVIATIONS

PROPERTY LINE	
CURB	
GUTTER	
SIDE INLET CATCH BASIN	
EXISTING DRAINAGE STRUCTURES	
GRATING TYPE CATCH BASIN	
DRIVEWAY	
LIMIT OF CONCRETE SURFACE	
WALK	
TRAFFIC SIGNAL	
DEAD MAN	
POWER, TELEPHONE OR GUY POLE	
FIRE HYDRANT	
ELECTROLIER	
WATER & GAS METER	
BENCH MARK	
TEST BORING	
TREE	
TREES TO BE REPLACED BY CONTRACTOR	
UNDER EXISTING UTILITY	
OVER EXISTING UTILITY	
TRAFFIC SIGNAL CONDUIT	T.S.C.
TRANSITION STRUCTURE	T.S.
MANHOLE	M.H.
LOCAL DEPRESSION	L.D.
REINFORCED CONCRETE PIPE	R.C.P.
TEST BORING	T.B.
JUNCTION STRUCTURE	J.S.
CATCH BASIN	C.B.
SANITARY SEWER	S.S.
TEMPORARY BENCH MARKS	T.B.M.
SOUTHERN CALIFORNIA GAS CO.	S.C.G.
L.A. DEPT. OF WATER & POWER WATER SYST. - DW&PWS	
SOUTHERN CALIFORNIA WATER CO.	S.C.W.
INGLEWOOD CITY WATER DEPT.	ING. W.
SOUTHERN CALIFORNIA EDISON CO.	S.C.E.
PACIFIC TELEPHONE & TELEGRAPH CO.	P.T.&T.

## LOS ANGELES COUNTY FLOOD CONTROL DISTRICT STANDARD DRAWINGS

DRAWING NO.	TITLE
2-D88	LOCAL DEPRESSION NO. 2
2-D96	STANDARD DROP STEP
2-D107	CONCRETE RINGS, REDUCER AND PIPE
2-D193	JUNCTION STRUCTURE NO. 4
2-D156	MANHOLE FRAME AND COVER FOR CATCH BASINS
2-D163	CATCH BASIN NO. 3 (W=10'; 14'; 21'; 28'; ETC.)
2-D172	CATCH BASIN REINFORCEMENT
2-D173.1 TO .3	PIPE SUPPORTS ACROSS TRENCHES
2-D175	REMOVABLE PROTECTION BAR FOR CATCH BASINS
2-D177	PIPE BEDDING IN TRENCHES
2-D181	STANDARD NON-ROCKING MANHOLE FRAME AND COVER
2-D184	MANHOLE NO. 2 (PIPES, 36" OR LARGER)
2-D213.1 & .2	"D" LOAD TABLE FOR DESIGN OF REINFORCED CONCRETE PIPE
2-D171	STANDARD A-305 REINFORCING BARS
2-D232	DETAIL OF CATCH BASIN OPENING
2-D250	REMODELING OF SANITARY SEWER HOUSE CONNECTIONS
2-D251	PROTECTION FOR MAIN LINE AND HOUSE CONNECTION SEWERS
2-D109	CATCH BASIN NO. 6
2-D224	CONNECTION TO CATCH BASIN FOR PIPES 12" THROUGH 72"
2-D227	FRAME AND GRATING FOR CATCH BASINS
2-D264	ADJUSTABLE PROTECTION BAR STIRRUP
2-D393	CONCRETE COLLAR FOR PIPES 12" THROUGH 66"
2-D413	UNIFIED SOIL CLASSIFICATION SYSTEM
2-D170	CATCH BASIN NO. 7
2-D399	CRITERIA FOR THE DESIGN OF SHORING FOR EXCAVATIONS
2-D400	SAMPLE SHEET FOR USE AS A GUIDE IN PREPARING CALCULATIONS FOR SHORING OF EXCAVATIONS
2-D113	MANHOLE NO. 4
2-D112	JUNCTION STRUCTURE NO. 2
2-D160	CATCH BASIN NO. 1

## GENERAL NOTES

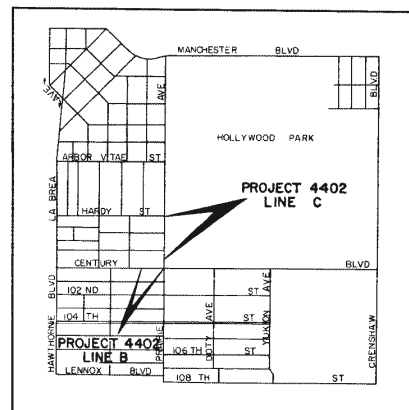
- NUMBERS IN CIRCLES INDICATE ITEMS UNDER WHICH PAYMENT WILL BE MADE.
- ELEVATIONS SHOWN ARE IN FEET ABOVE THE U.S.G.S. MEAN SEA LEVEL DATUM.
- STATIONS SHOWN ON DRAWINGS ARE ALONG CENTER LINE OF CONDUIT OR ON A LINE NORMAL TO CENTER LINE OF CONDUIT.
- STATIONS AND INVERT ELEVATIONS OF PIPE INLETS SHOWN ON THE PROFILES ARE AT THE INSIDE FACE OF THE CONDUIT, UNLESS OTHERWISE SHOWN.
- ALL FIELD BOOK REFERENCES ARE TO CITY OF INGLEWOOD FIELD BOOKS, UNLESS OTHERWISE NOTED.
- ALL PIPE IN OPEN TRENCH SHALL BE BEDDED ACCORDING TO STANDARD DRAWING 2-D177, CASE III, UNLESS OTHERWISE SHOWN OR MODIFIED IN THE SPECIFICATIONS.
- PIPE CONNECTIONS TO STORM DRAIN SHALL CONFORM TO STANDARD DRAWING 2-D193, UNLESS OTHERWISE SHOWN.
- TIES FOR CATCH BASINS AS SHOWN ON THE DRAWINGS ARE FROM CURB RETURN TO CENTER LINE OF CATCH BASIN, UNLESS OTHERWISE SHOWN.
- LOCATIONS OF CATCH BASIN CONNECTOR PIPE JUNCTIONS WITH CATCH BASINS AS SHOWN ON THE DRAWINGS ARE SCHEMATIC. IT IS INTENDED THAT SUCH JUNCTIONS BE LOCATED AT THE DOWNSTREAM ENDS OF THE CATCH BASINS, UNLESS OTHERWISE SHOWN. IN ALL CASES THE EXACT LOCATIONS WILL BE DETERMINED IN THE FIELD BY THE ENGINEER TO MEET FIELD CONDITIONS.
- MONOLITHIC CATCH BASIN CONNECTIONS SHALL BE CONSTRUCTED, WHERE APPLICABLE, PER STANDARD DRAWING 2-D224.
- "V<sub>i</sub>" IS THE DEPTH OF INLET OF CATCH BASINS IN SERIES MEASURED FROM TOP OF CURB TO INVERT OF CONNECTOR PIPE.
- ALL EXISTING SANITARY SEWERS SHOWN ON THE DRAWINGS ARE CITY OF INGLEWOOD SEWERS.
- EXISTING UTILITIES SHALL BE MAINTAINED IN PLACE BY THE CONTRACTOR, UNLESS OTHERWISE NOTED.
- WHERE UTILITIES ARE INDICATED ON THE DRAWINGS TO BE SUPPORTED, SAID SUPPORTS SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D173.1, .2 OR .3, UNLESS OTHERWISE INDICATED.
- LOCATIONS SHOWN ON THE PLANS FOR EXISTING SANITARY SEWER HOUSE CONNECTIONS ARE APPROXIMATE ONLY.
- SANITARY SEWER HOUSE CONNECTION RECONSTRUCTION AND RECONNECTION SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D250, UNLESS OTHERWISE SHOWN.
- SANITARY SEWERS AND HOUSE CONNECTIONS CROSSING OVER THE STORM DRAIN TRENCH SHALL BE SUPPORTED IN ACCORDANCE WITH STANDARD DRAWINGS 2-D173.1 TO .3 AND ENCASED PER GENERAL NOTE 1 ON STANDARD DRAWING 2-D173.1.
- WHEN INDICATED ON THE DRAWINGS, SANITARY SEWERS AND HOUSE CONNECTIONS SHALL BE ENCASED OR BLANKETED IN ACCORDANCE WITH STANDARD DRAWING 2-D251.
- ALL RESURFACING, CURBS, GUTTERS, SIDEWALKS, DRIVEWAYS AND OTHER EXISTING IMPROVEMENTS TO BE RECONSTRUCTED SHALL BE CONSTRUCTED AT THE SAME ELEVATION AND LOCATION AS THE EXISTING IMPROVEMENTS, UNLESS OTHERWISE NOTED.
- SOIL TEST BORINGS FOR THIS PROJECT WERE MADE 8-26-65 AND 8-27-65
- THE DEPTH AT THE UPSTREAM END OF CATCH BASINS 10 FEET OR MORE IN LENGTH SHALL BE CURB FACE PLUS 12 INCHES UNLESS OTHERWISE SHOWN.
- REFER TO SHEET 4 FOR TYPICAL CATCH BASIN CONNECTOR PIPE PROFILE.
- ALL OPENINGS RESULTING FROM THE CUTTING OR PARTIAL REMOVAL OF EXISTING PIPES, CULVERTS, OR SIMILAR STRUCTURES SHALL BE SEALED WITH 8 INCHES OF BRICK AND MORTAR OR 6 INCHES OF CONCRETE.
- THE OPENINGS AND TOP SLABS OF ALL SIDE INLET CATCH BASINS AND CATCH BASINS NO. 6 AND 7 SHALL BE MODIFIED TO MEET THE REQUIREMENTS SHOWN ON STANDARD DRAWING 2-D232.
- WHERE REQUIRED BY STANDARD DRAWING 2-D213.1, CONCRETE BACKFILL SHALL BE USED AROUND CONNECTOR PIPES 36 INCHES OR LESS IN DIAMETER. CONCRETE BACKFILL FOR MAIN LINE PIPE SHALL BE USED ONLY WHEN DIRECTED BY THE ENGINEER.
- THE OPENING OF ALL SIDE INLET CATCH BASINS AND CATCH BASIN NO. 6 THAT HAVE MODIFIED LOCAL DEPRESSIONS TO BE CURB FACE PLUS 1" IN LIEU OF 9".
- CONSTRUCT LOCAL DEPRESSION PER STANDARD DRAWING 2-D109 AND AS MODIFIED ON THE DRAWINGS FOR CATCH BASIN NO. 6.

## INDEX TO DRAWINGS

SHEET NO.	TITLE
1.	LOCATION MAP, GENERAL NOTES, INDEX TO DRAWINGS, STANDARD DRAWINGS, ABBREVIATIONS AND LEGEND.
2.	LINE C, PLAN, PROFILE AND SECTION STA25+00 TO STA34+85
3.	LINE B, PLAN, PROFILE AND SECTION STA39+80 TO STA46+66
4.	LOG OF BORINGS AND RESURFACING PLAN.

## LOS ANGELES COUNTY ROAD DEPARTMENT STANDARD DRAWINGS

DRAWING NO.	TITLE
M57-39R	PARTIAL CONCRETE REPLACEMENT FOR CROSS GUTTERS AND SPANDRELS
M57-45R	SPECIFICATIONS FOR REPAIRS OF CUTS IN CONCRETE PAVEMENT

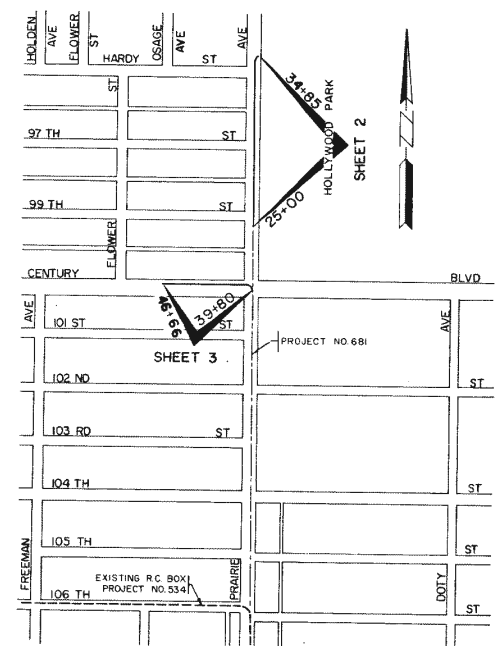


VICINITY MAP  
1000 0 1000 2000 3000 4000  
GRAPHIC SCALE

"AS BUILT DWGS."

REVISIONS	MARK	DATE	DESCRIPTION
INGLEWOOD			
CHECKED BY	Δ	5-4-67	Note Change Of Project Limits
DESIGNED BY			
INGLEWOOD			
SUBMITTED BY			
C. W. H.			

NOTE CHANGE OF PROJECT LIMITS  
Due to bond issue financing requirements, the upstream limit of Project 681, has been changed to Station 14+98. See DWG. NO. 364-681-D23. The downstream limit of Project 4402 Unit I, Line C, has been extended to meet the new upstream limit of Project 681, see DWG NO. 364-4402-D22.

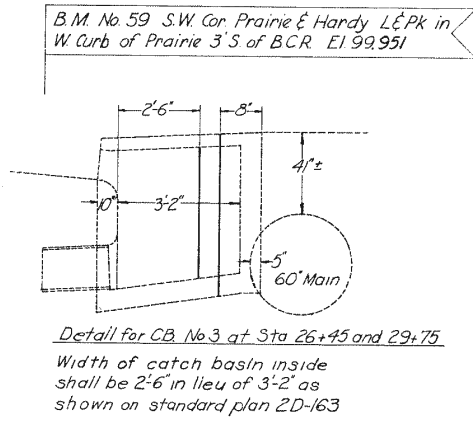
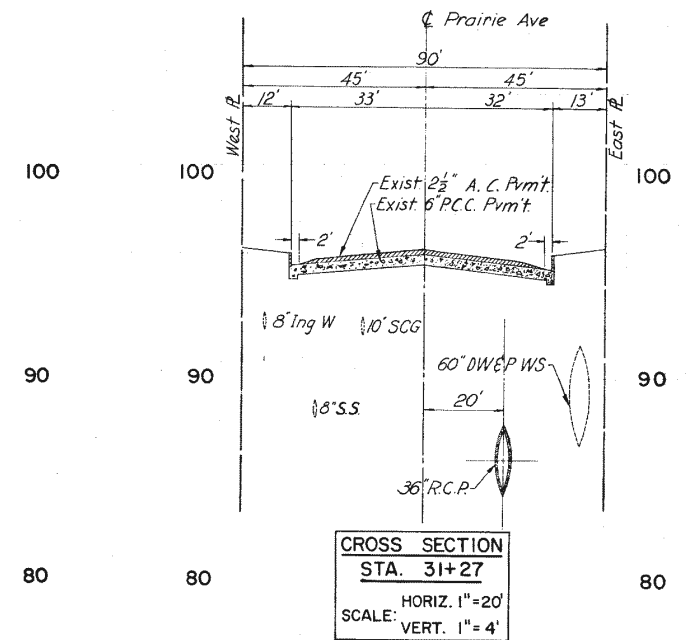


LOCATION MAP

500 0 500 1000 1500  
GRAPHIC SCALE

<b>CITY OF INGLEWOOD</b> PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION SUBMITTED BY: <i>R.K. Lee</i> ASSISTANT CITY ENGINEER R.C.E. 13078 APPROVED BY: <i>William J. Harman</i> 12-1-65 CITY ENGINEER R.C.E. 11237 DATE		1964 STORM DRAIN BOND ISSUE LOS ANGELES COUNTY FLOOD CONTROL DISTRICT <b>PROJECT NO. 4402, UNIT I</b> <b>INGLEWOOD</b> <b>LINE B&amp;C</b> LOCATION MAP, GENERAL NOTES, INDEX TO DRAWINGS, STANDARD DRAWINGS, LEGEND AND ABBREVIATIONS. RECOMMENDED BY: <i>R.K. Lee</i> DIVISION ENGINEER (DESIGN) APPROVED BY: <i>Master J. Wood</i> 12/1/66 ASST. CHIEF DEPUTY ENGINEER CHIEF ENGINEER SCALE JAN. '66 DWG. NO. 364-4402-D2.1 AS SHOWN SHEET 1 OF 4	
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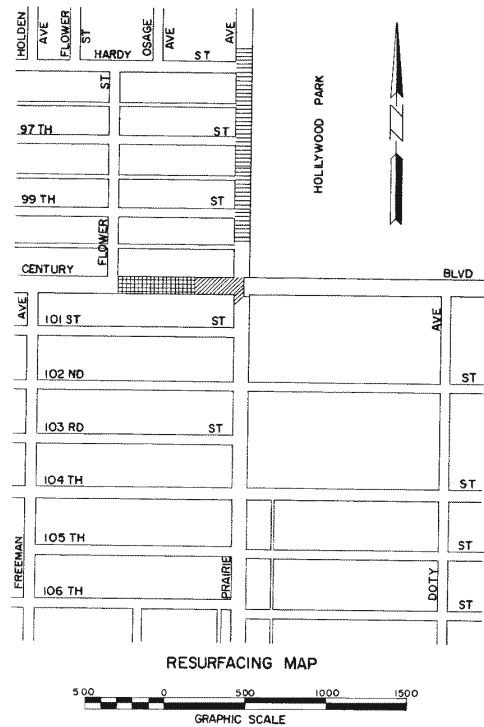
"AS BUILT" DRAWING



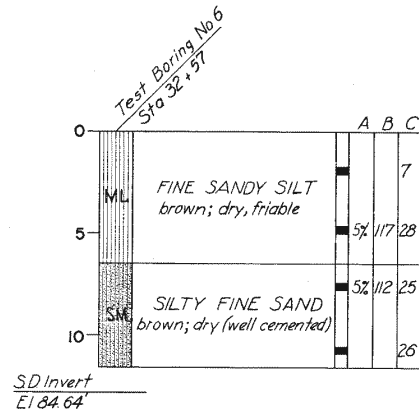
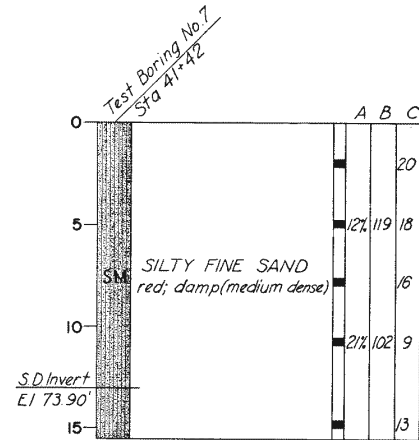
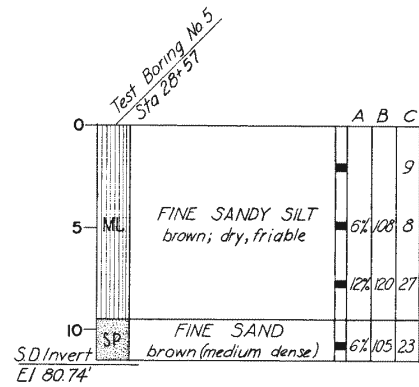
CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION		LOS ANGELES COUNTY FLOOD CONTROL DISTRICT PROJECT NO 4402, UNIT 1 INGLEWOOD LINE C CONCRETE CONDUIT STA. 25+00 TO STA. 34+85 PLAN AND PROFILE	
SUBMITTED BY: <i>R.K. [Signature]</i> ASSISTANT CITY ENGINEER R.C.E. 10378		RECOMMENDED BY: <i>R.B. [Signature]</i> DIVISION ENGINEER (DESIGN) APPROVED BY: <i>Walter [Signature]</i> CITY ENGINEER	
APPROVED BY: <i>Wm. [Signature]</i> CITY ENGINEER R.C.E. 11237 11-15-65 DATE		APPROVAL RECOMMENDED BY: <i>E.W. [Signature]</i> ASST. CHIEF DEPUTY ENGINEER SCALE DATE DWG. NO. 364-4402-022 AS SHOWN JAN. 12 1966 SHEET 2 OF 4	

"AS BUILT" DRAWING





EXISTING SURFACE		PROPOSED RESURFACING (30)	
8" P.C.C. PAVEMENT ON 6" SELECTED BASE MATERIAL		8" P.C.C. PAVEMENT ON 6" SELECTED BASE MATERIAL	
2" A.C. SURFACE ON 6" SELECTED BASE MATERIAL		3" A.C. SURFACE ON 6" SELECTED BASE MATERIAL	
2 1/2" A.C. SURFACE ON 6" PORTLAND CEMENT CONC.		2 1/2" A.C. SURFACE ON 6" PORTLAND CEMENT CONC.	



#### LEGEND AND NOTES:

SCALE: (VERTICAL) 1" = 4'

- A MOISTURE CONTENT IN PERCENTAGE  
 B DRY DENSITY IN LBS PER CUBIC FOOT  
 C STANDARD PENETRATION; NO. OF BLOWS PER FOOT  
 ■ DEPTH AT WHICH UNDISTURBED SAMPLE WAS TAKEN  
 ALL BORINGS WERE COMPLETED 8-26-65 AND 8-27-65.  
 NO GROUND WATER OR CAVING WAS ENCOUNTERED IN ANY BORING.  
 INVERT OF STORM DRAIN SHOWN ON THIS SHEET SUPERSEDES THAT SHOWN IN THE SOIL REPORT.  
 THE SOIL CLASSIFICATIONS SHOWN ARE IN ACCORDANCE WITH THE UNIFIED SOIL CLASSIFICATION SYSTEM.

#### NOTES:

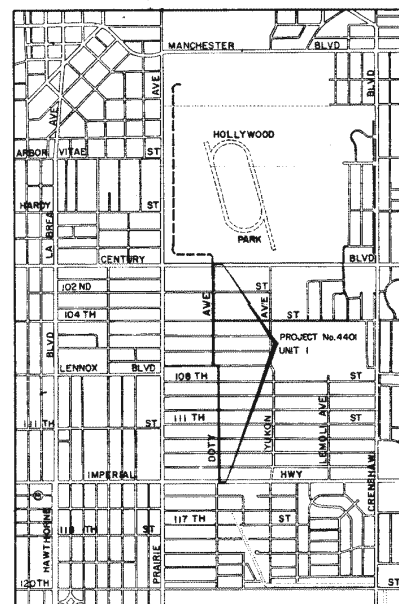
- The change in grade of the connector pipe may occur either over or under an existing utility. The particular utility at which the change occurs is noted on the project drawings. At locations where utility crossings are marked o the connector pipe grade will break over the utility. At locations where utility crossings are marked u the connector pipe grade will break under the utility.
- On those connector pipes where change in grade is not indicated, it is assumed that the connector pipe can be laid on a straight grade from the catch basin to the storm drain without interference with utilities.
- Where connector pipe has a change of grade exceeding .10/ft or differs in diameter from that of existing pipe, use concrete collar per std 2-D 393.
- The Contractor shall make exploratory excavation to determine the exact location and depth of utilities which are marked  $\Delta$  or  $\Delta$ . After the exact location of a utility has been determined, the grade and alignment of the connector pipe will be staked so as to clear the utility.

#### TYPICAL CONNECTOR PIPE PROFILE NO SCALE

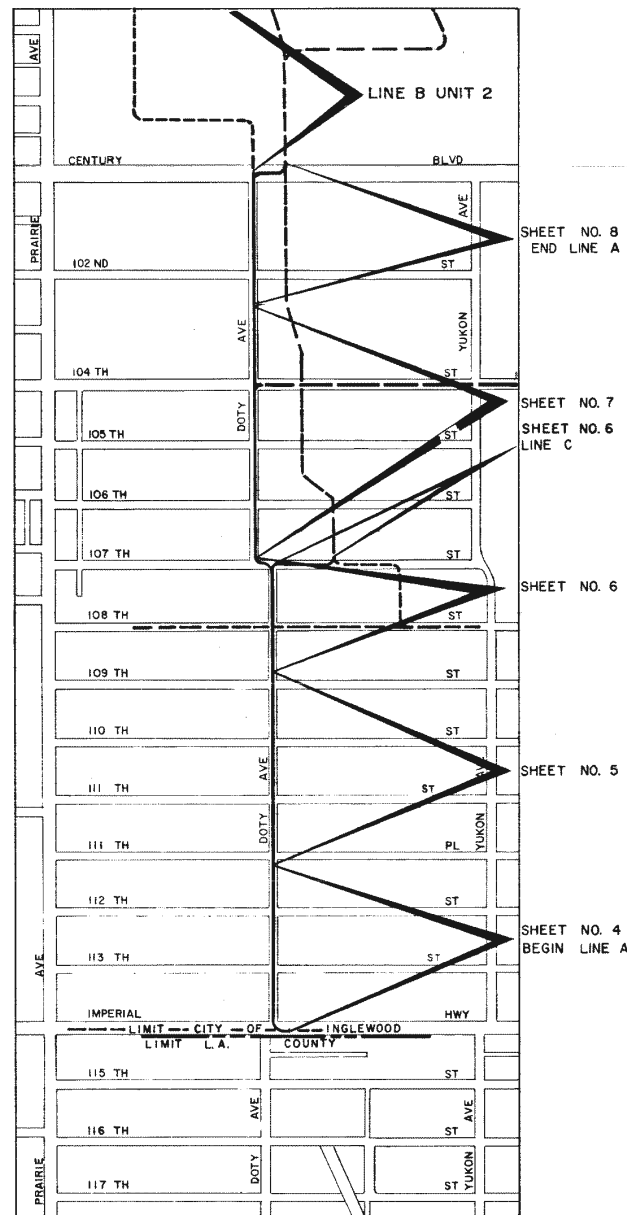
1964 STORM DRAIN BOND ISSUE	
CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION	LOS ANGELES COUNTY FLOOD CONTROL DISTRICT PROJECT NO. 4402, UNIT I INGLEWOOD
LOG OF BORINGS, RESURFACING PLAN AND MISCELLANEOUS DETAILS	
SUBMITTED BY: R. K. Lee ASSISTANT CITY ENGINEER R.C.E. 13078	RECOMMENDED BY: H. B. Hanks DIVISION ENGINEER DESIGN
APPROVED BY: Walter J. Wood CITY ENGINEER R.C.E. 11237	APPROVAL RECOMMENDED BY: R. W. Outland ASST. CHIEF DEPUTY ENGINEER
DATE: 12-2-65	DATE: 12-2-65
SCALE: AS SHOWN	DWG. NO. 364-4402-D2.4
SHEET 4 OF 4	



"AS BUILT" DRAWING



VICINITY MAP  
1000 0 1000 2000 3000 4000  
GRAPHIC SCALE



LOCATION MAP  
500 0 500 1000 1500  
GRAPHIC SCALE

# INDEX TO DRAWINGS

SHEET NO.	TITLE
1.	VICINITY MAP, LOCATION PLAN, INDEX TO DRAWINGS
2.	GENERAL NOTES, STRUCTURAL NOTES
3.	LEGEND & ABBREVIATIONS, STANDARD DRAWINGS, STRUCTURAL NOTES
4.	PLAN & PROFILE CONCRETE CONDUIT LINE A
5.	PLAN & PROFILE CONCRETE CONDUIT LINE A
6.	PLAN & PROFILE CONCRETE CONDUIT LINES A AND C
7.	PLAN & PROFILE CONCRETE CONDUIT LINE A
8.	PLAN & PROFILE CONCRETE CONDUIT LINE A
9.	PLAN & PROFILE COUNTY TRUNK LINE, SEWER LINE A & SEWER SIPHON **
10.	PLAN & PROFILE SANITARY SEWER SIPHON
11.	SINGLE R.C. BOX SCHEDULE & DETAILS
12.	SINGLE R.C. BOX SCHEDULE
13.	RESURFACING PLAN
14.	LOG OF BORINGS

■ "AS BUILT" DWGS.

## LEGEND

Proposed Storm Drain (UNIT I)  
Proposed Storm Drain  
Existing Storm Drain



CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION		LOS ANGELES COUNTY FLOOD CONTROL DISTRICT	
SUBMITTED BY: <i>William A. Maher</i> ASSISTANT CITY ENGINEER RCE 17167		PROJECT NO. 4401 INGLEWOOD LINES A AND C UNIT I VICINITY MAP, LOCATION MAP AND INDEX TO DRAWINGS	
APPROVED BY: <i>W. A. Maher</i> CITY ENGINEER RCE 11237		RECOMMENDED BY: <i>R. J. Milne</i> DIVISION ENGINEER (DESIGN)	
DATE: 11-81-74		DATE: 12-3-74	
SCALE: AS SHOWN		DWG. NO. 364-4401-D.6.1 SHEET 1 OF 14	

"AS BUILT" DRAWING

## GENERAL NOTES

- NUMBERS IN CIRCLES INDICATE ITEM UNDER WHICH PAYMENT WILL BE MADE.
- ELEVATIONS SHOWN ARE IN FEET ABOVE THE U.S.G.S. MEAN SEA LEVEL DATUM.
- STATIONS SHOWN ON DRAWINGS ARE ALONG CENTERLINE OF CONDUIT OR ON A LINE NORMAL TO CENTERLINE OF CONDUIT.
- STATIONS AND INVERT ELEVATIONS OF PIPE INLETS SHOWN ON THE PROFILES ARE AT THE INSIDE FACE OF THE CONDUIT, UNLESS OTHERWISE SHOWN.
- ALL FIELD BOOK REFERENCES ARE TO CITY OF INGLEWOOD FIELD BOOKS, UNLESS OTHERWISE NOTED.
- LOCATIONS SHOWN ON THE PLANS FOR EXISTING SANITARY SEWER HOUSE CONNECTIONS ARE APPROXIMATE ONLY.
- PIPE CONNECTIONS TO STORM DRAIN SHALL CONFORM TO STANDARD DRAWING 2-D191 & 2-D193 UNLESS OTHERWISE SHOWN.
- TIES FOR CATCH BASINS AS SHOWN ON THE DRAWINGS ARE FROM CURB RETURN TO CENTER LINE OF CATCH BASINS, UNLESS OTHERWISE SHOWN.
- LOCATIONS OF CATCH BASIN CONNECTOR PIPE JUNCTIONS WITH CATCH BASINS AS SHOWN ON THE DRAWINGS ARE SCHEMATIC. IT IS INTENDED THAT SUCH JUNCTIONS BE LOCATED AT THE DOWNSTREAM ENDS OF THE CATCH BASINS, UNLESS A DETAIL OF THE CONNECTION IS SHOWN OR A NOTE SPECIFICALLY INDICATES OTHERWISE. IN ALL CASES THE EXACT LOCATIONS WILL BE DETERMINED IN THE FIELD BY THE ENGINEER TO MEET FIELD CONDITIONS.
- MONOLITHIC CATCH BASIN CONNECTIONS SHALL BE CONSTRUCTED, WHERE APPLICABLE, PER STANDARD DRAWING 2-D224.
- "V<sub>1</sub>" IS THE DEPTH OF INLET OF CATCH BASINS IN SERIES MEASURED FROM TOP OF CURB TO INVERT OF CONNECTOR PIPE. "V<sub>2</sub>" IS THE SAME AS "V" ON THE VARIOUS CATCH BASIN STANDARD DRAWINGS.
- ALL EXISTING SANITARY SEWERS SHOWN ON THE DRAWINGS ARE CITY OF INGLEWOOD SEWERS, UNLESS OTHERWISE NOTED.
- EXISTING UTILITIES SHALL BE MAINTAINED IN PLACE BY THE CONTRACTOR, UNLESS OTHERWISE NOTED.
- DELETED.
- UTILITIES DESIGNATED BY THE SYMBOL "\*" WILL BE ABANDONED IN PLACE AND THE OWNER WILL INSTALL A NEW SECTION OF THE AFFECTED UTILITY AT A LOCATION IN CLOSE PROXIMITY TO, BUT WHICH DOES NOT PHYSICALLY INTERFERE WITH, THE PROPOSED STORM DRAIN CONDUIT AND APPURTENANT STRUCTURES.
- WHERE UTILITIES ARE INDICATED ON THE DRAWINGS TO BE SUPPORTED, SAID SUPPORTS SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D173.1, .2 OR .3, UNLESS OTHERWISE INDICATED.

## GENERAL NOTES

- SANITARY SEWER HOUSE CONNECTION RECONSTRUCTION AND RECONNECTION SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D250, UNLESS OTHERWISE SHOWN.
- SANITARY SEWERS AND HOUSE CONNECTIONS CROSSING OVER THE STORM DRAIN TRENCH SHALL BE SUPPORTED IN ACCORDANCE WITH STANDARD DRAWING 2-D173.1 TO .3 AND ENCASED PER GENERAL NOTE 1 ON STANDARD DRAWING 2-D173.1.
- WHEN INDICATED ON THE DRAWINGS, SANITARY SEWERS AND HOUSE CONNECTIONS SHALL BE ENCASED OR BLANKETED IN ACCORDANCE WITH STANDARD DRAWING 2-D251.
- ALL OPENINGS RESULTING FROM THE CUTTING OR PARTIAL REMOVAL OF EXISTING CULVERTS, PIPES OR SIMILAR STRUCTURES SHALL BE SEALED WITH 8 INCHES OF BRICK AND MORTAR OR 6 INCHES OF CONCRETE, UNLESS OTHERWISE SHOWN.
- ALL RESURFACING, CURBS, GUTTERS, SIDEWALKS, DRIVEWAYS AND OTHER EXISTING IMPROVEMENTS TO BE RECONSTRUCTED SHALL BE CONSTRUCTED AT THE SAME ELEVATION AND LOCATION AS THE EXISTING IMPROVEMENTS, UNLESS OTHERWISE NOTED.
- REFER TO SHEET 13 FOR TYPICAL CATCH BASIN CONNECTOR PIPE PROFILE.
- STREET RESURFACING PLANS ARE SHOWN ON SHEET 13.
- SOIL TEST BORINGS FOR THIS PROJECT WERE MADE IN AUGUST AND SEPTEMBER, 1972
- PAY LINES FOR EXCAVATION FOR REINFORCED CONCRETE BOX CONDUIT ARE SHOWN ON SHEET II OF THE DRAWINGS.
- DESIGN OF THE PIPE SHOWN HEREON IS BASED ON THE ASSUMPTION THE PIPE WILL BE INSTALLED IN ACCORDANCE WITH CASE III BEDDING AS SHOWN ON STANDARD DRAWING 2-D177 UNLESS OTHERWISE SHOWN. "W" VALUES SHALL BE AS SPECIFIED ON STANDARD DWG. 2-D177 FOR CASE III BEDDING, NOTES 3(a), 3(b) AND 3(c). IF THE "W" VALUE AT THE TOP OF THE PIPE IS EXCEEDED, THE BEDDING SHALL BE MODIFIED, AND/OR PIPE OF ADDITIONAL STRENGTH SHALL BE PROVIDED. THE PROPOSED MODIFICATION SHALL BE APPROVED BY THE DISTRICT.
- CONCRETE BACKFILL SHALL BE PROVIDED AROUND PIPE 21" IN DIAMETER OR LESS WHERE THE COVER IS EQUAL TO OR LESS THAN 2'-0", AROUND PIPE GREATER THAN 21 INCHES IN DIAMETER BUT LESS THAN 39 INCHES WHERE THE COVER IS LESS THAN 1'-3", AND FOR PIPE 39" OR GREATER WHERE THE COVER IS LESS THAN 1'-0". THE CONCRETE BACKFILL SHALL BE AS SPECIFIED ON STANDARD DRAWING 2-D177, NOTE 3.
- CURB FACE (C.F) SHOWN ON THE GENERAL PLAN PERTAINS TO THE CURB FACE AT THE CATCH BASIN OPENING UNLESS OTHERWISE NOTED. FOR LOCAL DEPRESSION NO. 2, THE CURB FACE SHALL BE THE EXISTING PLUS 4", UNLESS OTHERWISE SPECIFIED.
- ASBESTOS CEMENT PIPE MAY BE USED IN LIEU OF REINFORCED CONCRETE PIPE 42 INCHES OR LESS IN DIAMETER.
- THE REQUIRED D-LOAD FOR THE ASBESTOS CEMENT PIPE SHALL BE 1.5 TIMES THAT SPECIFIED ON THE PLANS FOR REINFORCED CONCRETE PIPE.
- UTILITIES DESIGNATED BY THE SYMBOL \* WILL BE REMOVED BY THE OWNER AND THE OWNER WILL REINSTALL A NEW SECTION OF THE AFFECTED UTILITY AT A LOCATION IN CLOSE PROXIMITY TO, BUT WHICH DOES NOT PHYSICALLY INTERFERE WITH, THE PROPOSED STORM DRAIN CONDUIT AND APPURTENANT STRUCTURES.

## STRUCTURAL NOTES

- DIMENSIONS FROM FACE OF CONCRETE TO STEEL ARE TO CENTER OF BAR AND SHALL BE 2" UNLESS OTHERWISE SHOWN.
- CONCRETE DIMENSIONS SHALL BE MEASURED HORIZONTALLY OR VERTICALLY ON THE PROFILE, AND PARALLEL TO OR AT RIGHT ANGLES (OR RADIALY) TO CENTERLINE OF CONDUIT ON THE PLAN EXCEPT AS OTHERWISE SHOWN.
- ALL BAR BENDS AND HOOKS SHALL CONFORM TO THE 1963 AMERICAN CONCRETE INSTITUTE'S "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE" SECTION 801.
- PLACING OF REINFORCEMENT SHALL CONFORM TO THE 1963 AMERICAN CONCRETE INSTITUTE'S "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE" SECTION 803.
- TRANSVERSE CONSTRUCTION JOINTS SHALL NOT BE PLACED WITHIN 30 INCHES OF MANHOLE OR JUNCTION STRUCTURE OPENINGS.
- TRANSVERSE CONSTRUCTION JOINTS IN WALLS AND SLABS SHALL BE IN THE SAME PLANE. NO STAGGERING OF JOINTS WILL BE PERMITTED. TRANSVERSE CONSTRUCTION JOINTS SHALL BE NORMAL OR RADIAL TO THE CENTER LINE OF CONSTRUCTION.
- THE TRANSVERSE REINFORCING STEEL SHALL TERMINATE 1-1/2 INCHES FROM THE CONCRETE SURFACE UNLESS OTHERWISE SHOWN ON THE STRUCTUAL DETAILS.
- EXPOSED EDGES OF CONCRETE MEMBERS SHALL BE ROUNDED OR BEVELED.
- NO SPLICES IN TRANSVERSE STEEL REINFORCEMENT WILL BE PERMITTED OTHER THAN SHOWN ON THE DRAWING WITHOUT APPROVAL OF THE ENGINEER. NO MORE THAN 2 SPLICES WILL BE PERMITTED IN ANY LONGITUDINAL BAR BETWEEN TRANSVERSE JOINTS. SPLICES SHALL BE STAGGERED.
- LONGITUDINAL STEEL SHALL BE LAPPED 20 BAR DIAMETERS AT SPLICES. TRANSVERSE STEEL SHALL BE LAPPED 30 BAR DIAMETERS AT SPLICES.
- LONGITUDINAL STEEL SHALL BE CONTINUOUS AND EXTEND THROUGH ALL CONSTRUCTION JOINTS.
- UNLESS OTHERWISE SHOWN ON THE DRAWINGS, TRANSVERSE JOINT KEYWAYS (IN BOTH SLABS AND WALLS), AS DETAILED FOR LONGITUDINAL KEYWAYS AT THE BASE OF THE WALLS, SHALL BE PLACED AT THE END OF EACH POUR, BUT THE SPACING THEREOF SHALL NOT EXCEED 50 FEET OR BE LESS THAN 10 FEET. SPACING MAY BE DECREASED TO AVOID PROXIMITY TO INLETS. ALL CONSTRUCTION JOINTS IN BOTTOM SLAB, TOP SLAB, AND SIDE WALLS SHALL BE IN THE SAME PLANE. NO STAGGERING OF JOINTS WILL BE PERMITTED.
- THE VERTICAL STEEL IN THE INTERIOR FACE OF EXTERIOR WALLS MAY BE SPLICED AT THE CONSTRUCTION JOINT AT THE BASE OF THE WALL. THE SPLICE SHALL BE 20 BAR DIAMETERS IN LENGTH.



1964 STORM DRAIN BOND ISSUE

REVISIONS			
MARK	DATE	DESCRIPTION	

CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION		LOS ANGELES COUNTY FLOOD CONTROL DISTRICT	
SUBMITTED BY: <i>William J. Maher</i> ASSISTANT CITY ENGINEER R.C.E. 17167		PROJECT NO. 4401 INGLEWOOD LINES A AND C UNIT I GENERAL NOTES & STRUCTURAL NOTES	
APPROVED BY: <i>W. J. Maher</i> CITY ENGINEER R.C.E. 11237 DATE 1-3-74		RECOMMENDED BY: <i>W. J. Maher</i> DIVISION ENGINEER (DESIGN)	
SCALE DATE AS SHOWN Sept, 74		DWG. NO. 364-4401-D6.2 SHEET 2 OF 14	

"AS BUILT" DRAWING



LEGEND AND ABBREVIATIONS

RIGHT OF WAY (OR EASEMENT)	
PROPERTY LINE	
CURB	
GUTTER	
SIDE INLET CATCH BASIN	
EXISTING DRAINAGE STRUCTURES	
GRATING TYPE CATCH BASIN	
DRIVEWAY	
LIMIT OF CONCRETE SURFACE	
WALK	
TRAFFIC SIGNAL	
DEAD MAN	
POWER, TELEPHONE OR GUY POLE	
FIRE HYDRANT	
ELECTROLIER	
WATER & GAS METER	
BENCH MARK	
TEST BORING	
TREE	
TREES TO BE REPLACED BY CONTRACTOR	
UNDER EXISTING UTILITY	
OVER EXISTING UTILITY	
TRAFFIC SIGNAL CONDUIT	T.S.C.
TRANSITION STRUCTURE	T.S.
MANHOLE	M.H.
LOCAL DEPRESSION	L.D.
REINFORCED CONCRETE PIPE	R.C.P.
TEST BORING	T.B.
JUNCTION STRUCTURE	J.S.
CATCH BASIN	C.B.
SANITARY SEWER	S.S.
TEMPORARY BENCH MARKS	T.B.M.
SOUTHERN CALIFORNIA GAS CO.	SCG
L.A. DEPT. OF WATER & POWER WATER SYST.	D.W.&P.W.S.
SOUTHERN CALIFORNIA WATER CO.	SCW
INGLEWOOD CITY WATER DEPT.	I.W.D.
SOUTHERN CALIFORNIA EDISON CO.	S.C.E.
PACIFIC TELEPHONE & TELEGRAPH CO.	P.T.&T.
RICHFIELD OIL CO. GAS LINE	R.G.L.
HOLLYWOOD TURF CLUB WATER	H.T.C.W.
UNIFIED SCHOOL DISTRICT WATER	U.S.D.W.
BURRIED CABLE	BUR. CA.
CRUSHED AGGREGATE BASE	C.A.B.
LIGHT STANDARD	L.S.

LOS ANGELES COUNTY FLOOD CONTROL DISTRICT  
STANDARD DRAWINGS

DRAWING NO.	TITLE
2-D 88	LOCAL DEPRESSION NO. 2
2-D 96	STANDARD DROP STEP
2-D 104	MANHOLE NO. 3
2-D 107	CONCRETE RINGS, REDUCER AND PIPE FOR MANHOLE SHAFT
2-D 156	MANHOLE FRAME AND COVER FOR CATCH BASINS
2-D 157	CATCH BASIN REINFORCEMENT FOR ROUND MANHOLES
2-D 160	CATCH BASIN NO. 1
2-D 162	CATCH BASIN NO. 2
2-D 171	STANDARD A-615 REINFORCING BARS
2-D 172	CATCH BASIN REINFORCEMENT
2-D 173.1 TO .3	PIPE SUPPORTS ACROSS TRENCHES
2-D 175	REMOVABLE PROTECTION BAR FOR CATCH BASINS
2-D 177	PIPE BEDDING IN TRENCHES
2-D 184	MANHOLE NO. 2
2-D 189	JUNCTION STRUCTURE NO. 1
2-D 191	JUNCTION STRUCTURE NO. 3
2-D 193	JUNCTION STRUCTURE NO. 4
2-D 224	CONNECTION TO CATCH BASIN FOR PIPES 12" THROUGH 72"
2-D 232	DETAIL OF CATCH BASIN OPENING
2-D 235	TRANSITION STRUCTURE NO. 1
2-D 239	TRANSITION STRUCTURE NO. 2
2-D 250	REMODELING OF SANITARY SEWER HOUSE CONNECTIONS
2-D 251	PROTECTION FOR MAIN LINE AND HOUSE CONNECTION SEWERS
2-D 264	ADJUSTABLE PROTECTION BAR STIRRUP
2-D 393	CONCRETE COLLAR FOR PIPES 12" THROUGH 66"
2-D 466	CRITERIA FOR THE DESIGN OF SHORING FOR EXCAVATIONS
2-D 400	SAMPLE SHEET FOR USE AS A GUIDE IN PREPARING CALCULATIONS FOR SHORING OF EXCAVATIONS
2-D 413	UNIFIED SOIL CLASSIFICATION SYSTEM
2-D 465	ADDITIONAL REINFORCEMENT FOR JACKED R.C. BOX
2-D 431	"D" LOAD TABLE FOR DESIGN OF ASBESTOS CEMENT PIPE
2-D 461	MODIFICATIONS FOR SIDE OPENING CATCH BASINS
2-D 472	STANDARD 24 INCH MANHOLE FRAME AND COVER
2-D 476	PORTABLE SECURITY FENCE FOR OPEN TRENCHES

LOS ANGELES COUNTY ENGINEER  
STANDARD DRAWINGS

DRAWING NO.	TITLE
S-3	BRICK MANHOLE
S-17	STANDARD MANHOLE STEP
S-21	BEDDING FOR SEWER PIPE
S-23	CRADLING AND ENCASEMENT
S-27	CHIMNEY PIPE AND BASE
S-33	ALLOWABLE TRENCH WIDTH
S-35	LOCKING MANHOLE FRAME AND COVER
S-36	NON-REINFORCED PRECAST CONCRETE MANHOLE

LOS ANGELES COUNTY ROAD DEPARTMENT  
STANDARD DRAWINGS

M57-39R	PARTIAL CONCRETE REPLACEMENT FOR CROSS GUTTER AND SPANDRELS
32-01	TYPICAL SIDEWALK DETAILS

LOS ANGELES COUNTY SANITATION DISTRICT  
STANDARD DRAWINGS

DRAWING NO.	TITLE
S-a-201	STANDARD MANHOLE, TYPE "A"
S-a-204	STANDARD MANHOLE, TYPE "D"
S-a-207	STANDARD 24" MANHOLE FRAME & COVER
S-a-209	STANDARD MANHOLE STEP
S-a-217	CONCRETE PIPE SUPPORT
S-a-220	STANDARD PULL RING
S-a-222	TEMPORARY SEWER SUPPORT
S-a-227	STANDARD CONCRETE BEAM FOR HOUSE CONNECTIONS

CITY OF INGLEWOOD  
STANDARD DRAWINGS

G-1	STANDARD CURB & GUTTER AND STANDARD CROSS GUTTER
G-2	STANDARD ALLEY INTERSECTION
G-4	STANDARD DRIVEWAY APPROACH

21. THE CONTRACTOR SHALL USE JACKING HEADS OR LOAD SPREADING BEAMS OF SUCH DESIGN AND SIZE AS TO SPREAD THE JACKING FORCE UNIFORMLY OVER THE ENTIRE INVERT SECTION.
22. IF THE LOAD SPREADING DEVICE OR JACKING HEAD SELECTED DOES NOT PERMIT THE REQUIRED 20 BAR DIAMETER EXTENSION OF THE NORMAL LONGITUDINAL STEEL, CONTINUITY MAY BE MAINTAINED BY DOWELING FROM THE ADJACENT SECTION.
23. THE LEADING EDGE OF CONDUIT SHALL BE EQUIPPED WITH A JACKING HEAD SECURELY ANCHORED THERE. THE LENGTH AND DETAILS OF THE JACKING HEAD SHALL BE SUBJECT TO THE APPROVAL OF THE ENGINEER.
24. THE USE OF GUIDE RAILS, SLABS, CRADLES, ETC. WILL BE SUBJECT TO WRITTEN APPROVAL BY THE ENGINEER.

STRUCTURAL NOTES CONT'D.

14. UNLESS OTHERWISE SHOWN ON THE DETAILS, IN CURVED SECTIONS TRANSVERSE BARS SHALL BE PLACED RADIALLY. STRAIGHT TRANSVERSE BARS IN TOP AND BOTTOM SLABS SHALL BE SPACED AS SHOWN ON THE TYPICAL SECTIONS; SPACING SHALL BE AT THE CENTERLINE OF CONSTRUCTION. STRAIGHT BARS AND L-BARS IN WALLS SHALL BE SPACED AS SHOWN ON THE TYPICAL SECTIONS, WITH THE SPACING MEASURED BETWEEN THE VERTICAL LEGS OF BARS.
15. AT THE BEGINNING AND ENDING OF ALL POURS, A CURTAIN OF REINFORCEMENT COMPOSED OF B, C, C<sub>2</sub>, D, F, G, AND H BARS SHALL BE PLACED THREE INCHES FROM THE TRANSVERSE CONSTRUCTION JOINT.
16. IN ALL SECTIONS LAP C AND C<sub>2</sub> BARS, THE VERTICAL LENGTH OF C AND C<sub>2</sub> BARS HAS BEEN CALCULATED FOR A FOUR-INCH STARTER WALL. IF THE HEIGHT OF STARTER IS VARIED, THE VERTICAL LENGTH OF THE C AND C<sub>2</sub> BARS SHALL BE VARIED CORRESPONDINGLY SO AS TO MAINTAIN A 30 DIAMETER LAP BETWEEN THE TWO BARS. THE LAPS SHALL BE BASED ON THE SMALLER BAR.
17. IF WALL THICKNESS IS SIX INCHES, PLACE REINFORCEMENT AT THE CENTERLINE OF THE WALL.
18. CONCRETE QUANTITIES ARE BASED ON A SIX BY SIX INCH FILLET AND STEEL QUANTITIES DO NOT INCLUDE ANY OPTIONAL SPLICES.
19. ALL LONGITUDINAL BARS SHALL BE NO. 4 BARS. SPACING SHALL BE 18 INCHES UNLESS OTHERWISE SHOWN. BARS IN TOP OR BOTTOM SLAB SHALL BE SPACED SYMMETRICAL ABOUT THE CENTER LINE. BARS IN WALLS SHALL BE SPACED SYMMETRICAL ABOUT MID HEIGHT OF THE WALLS.
20. CONCRETE BREAKOUT NOTES:
1. FOR CONCRETE REMOVAL, WHERE REINFORCEMENT IS TO BE RETAINED THROUGH THE JOINT, MAKE A SAWCUT ONE AND ONE-HALF INCHES DEEP ON THE EXPOSED FACES OF THE CONCRETE AT THE REMOVAL LIMITS. CUT A GROOVE IN THE CONCRETE ADJACENT TO THE SAWCUT, ON THE SIDE TO BE REMOVED TO THE DEPTH OF THE SAWCUT, WITH A CHIPPING HAMMER. EXISTING REINFORCEMENT SHALL BE RESTORED AND RETAINED OR CUT AND LAPPED 30 BAR DIAMETERS WITH NEW REINFORCEMENT.
2. CARE SHALL BE EXERCISED IN SAWING AT THE REMOVAL LIMITS SO AS NOT TO CUT THE REINFORCEMENT IN THE STRUCTURE TO REMAIN. AFTER MAKING SAW CUTS THE CONCRETE SHALL BE REMOVED WITH HAND OPERATED EQUIPMENT. USE OF EXPLOSIVES, WRECKING BALLS, STOMPERS OR OTHER EQUIPMENT, WHICH WOULD CAUSE DAMAGE TO THE EXISTING FACILITY REMAINING IN PLACE, WILL NOT BE PERMITTED. THE ENGINEER SHALL BE THE SOLE JUDGE OF THE USAGE OF ANY EQUIPMENT FOR THE CONCRETE REMOVAL OPERATION.

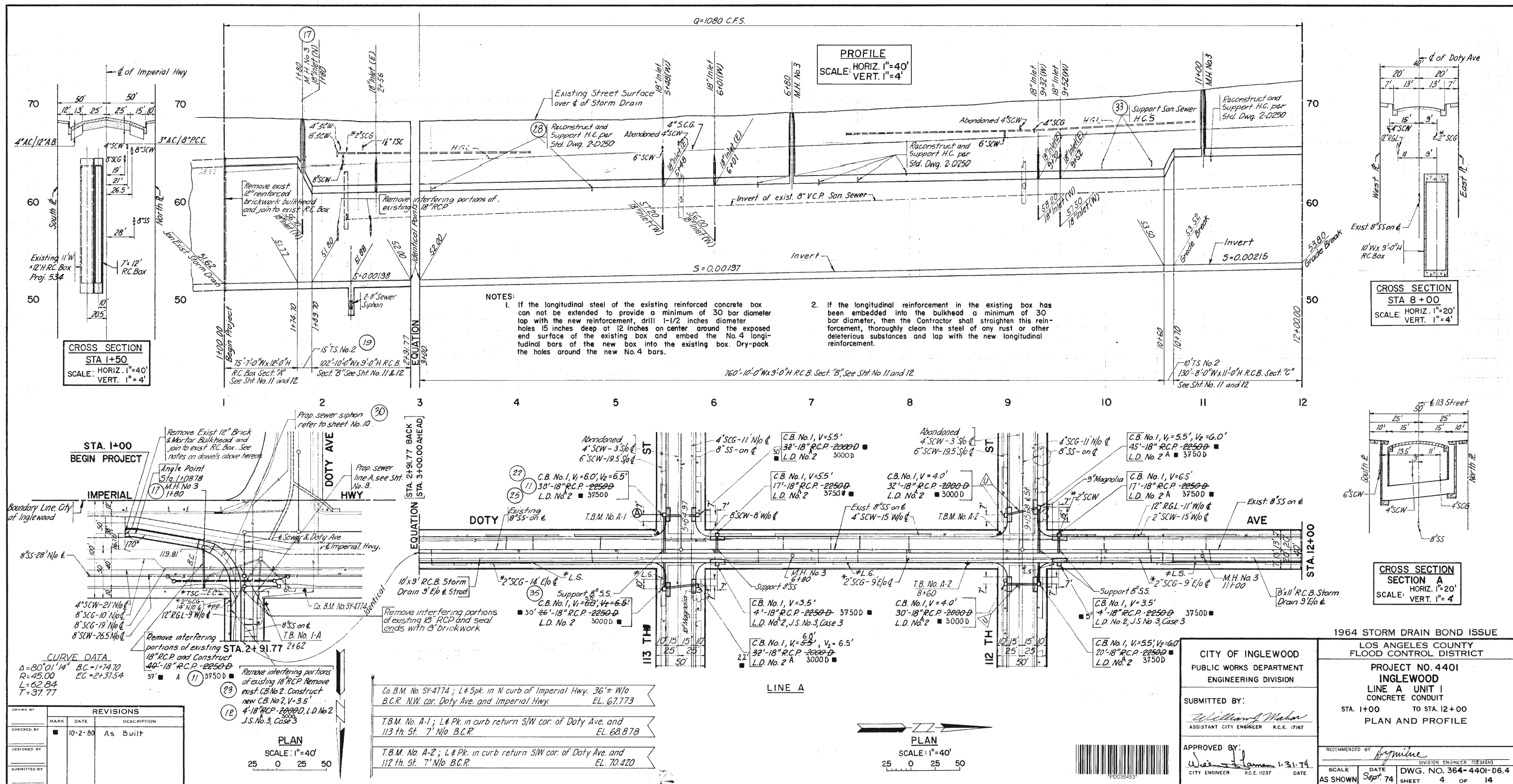


1964 STORM DRAIN BOND ISSUE

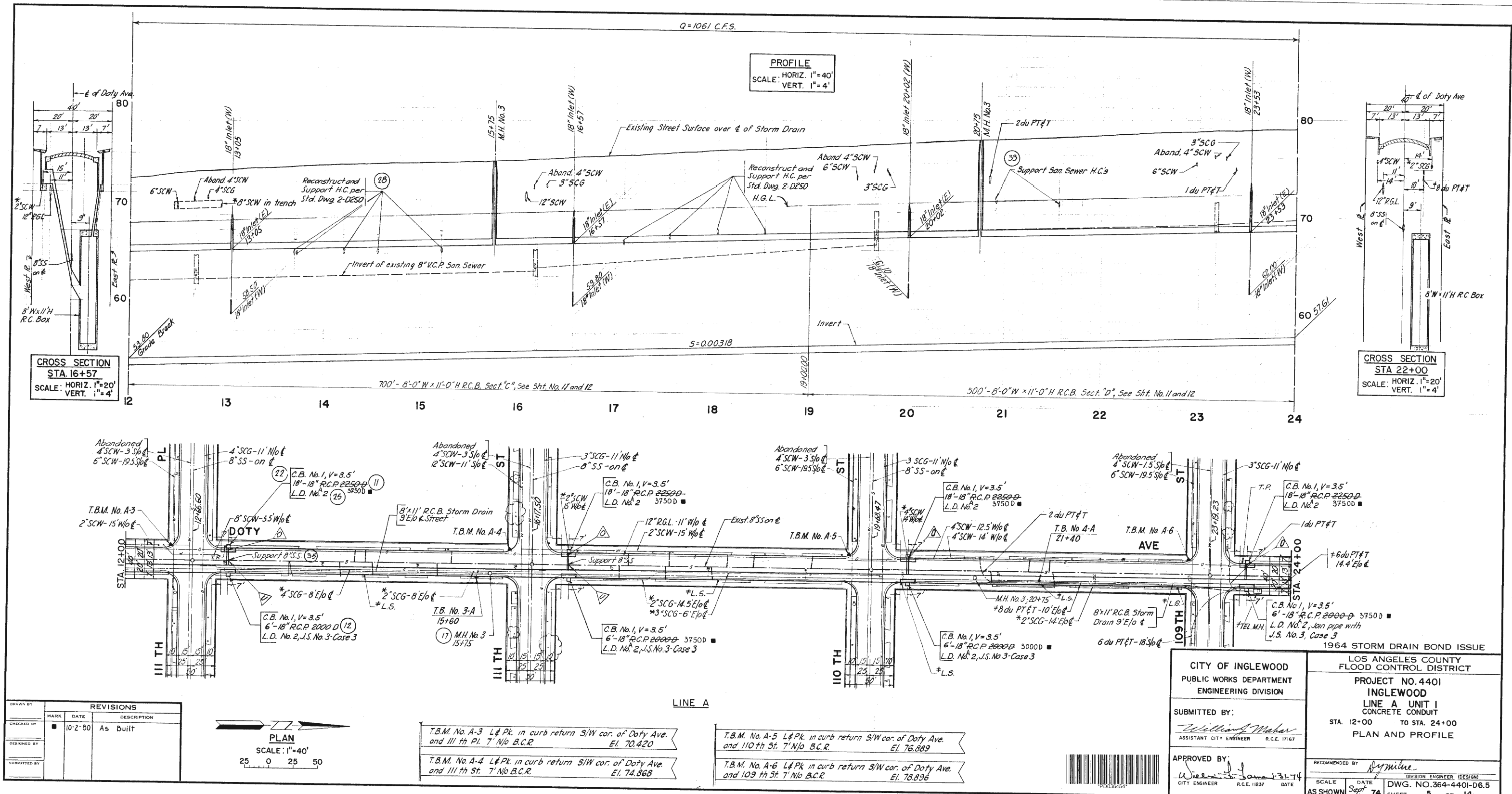
CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION	LOS ANGELES COUNTY FLOOD CONTROL DISTRICT
SUBMITTED BY: <i>William A. Maher</i> ASSISTANT CITY ENGINEER R.C.E. 17167	PROJECT NO. 4401 INGLEWOOD LINES A, AND C UNIT I LEGEND AND ABBREVIATION, STANDARD DRAWINGS, AND STRUCTURAL NOTES
APPROVED BY: <i>William A. Maher</i> CITY ENGINEER R.C.E. 11237 DATE 1-31-74	RECOMMENDED BY: <i>[Signature]</i> DIVISION ENGINEER (DESIGN) SCALE DATE DWG. NO. 364-4401-D63 AS SHOWN 3-1-74 SHEET 3 OF 14

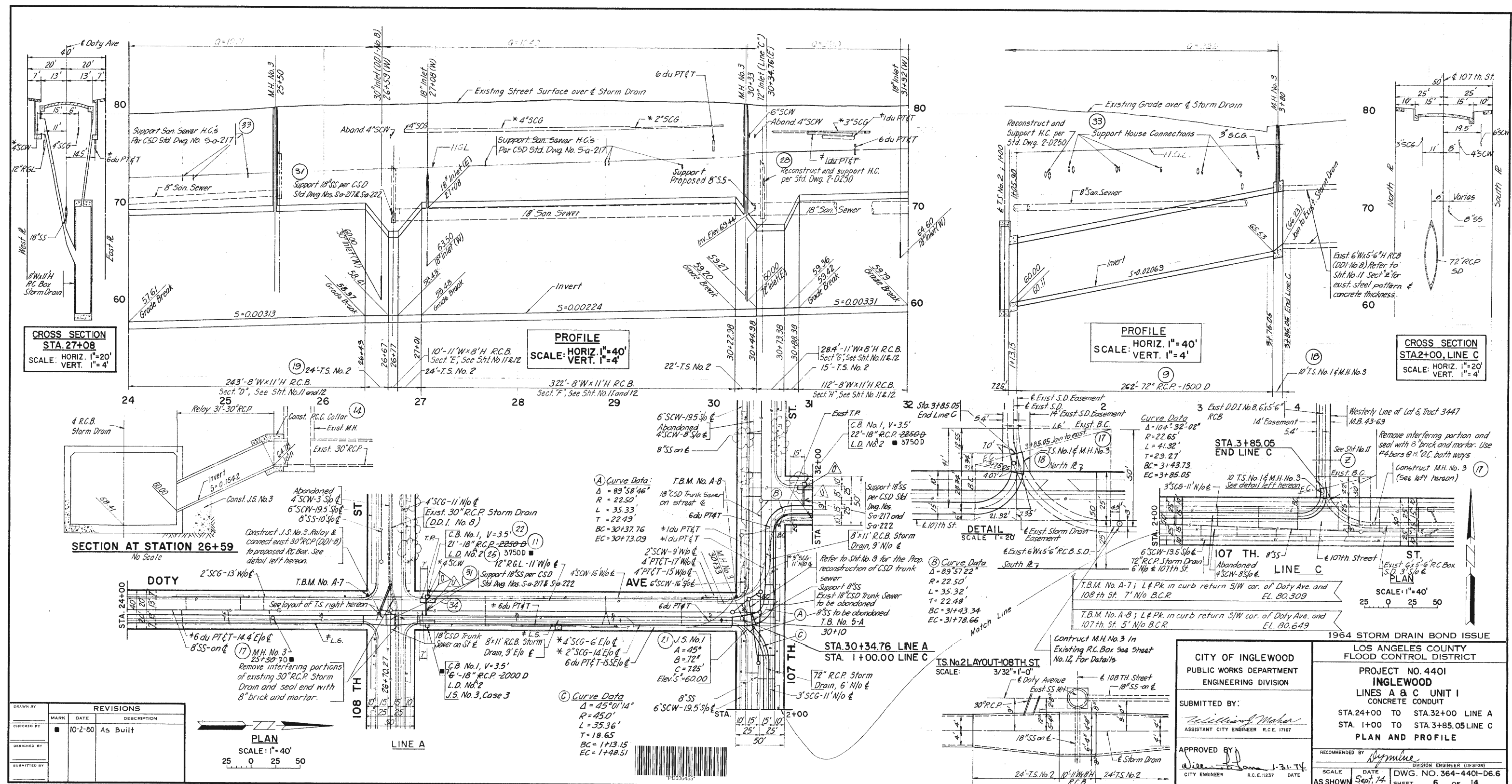
"AS BUILT" DRAWING

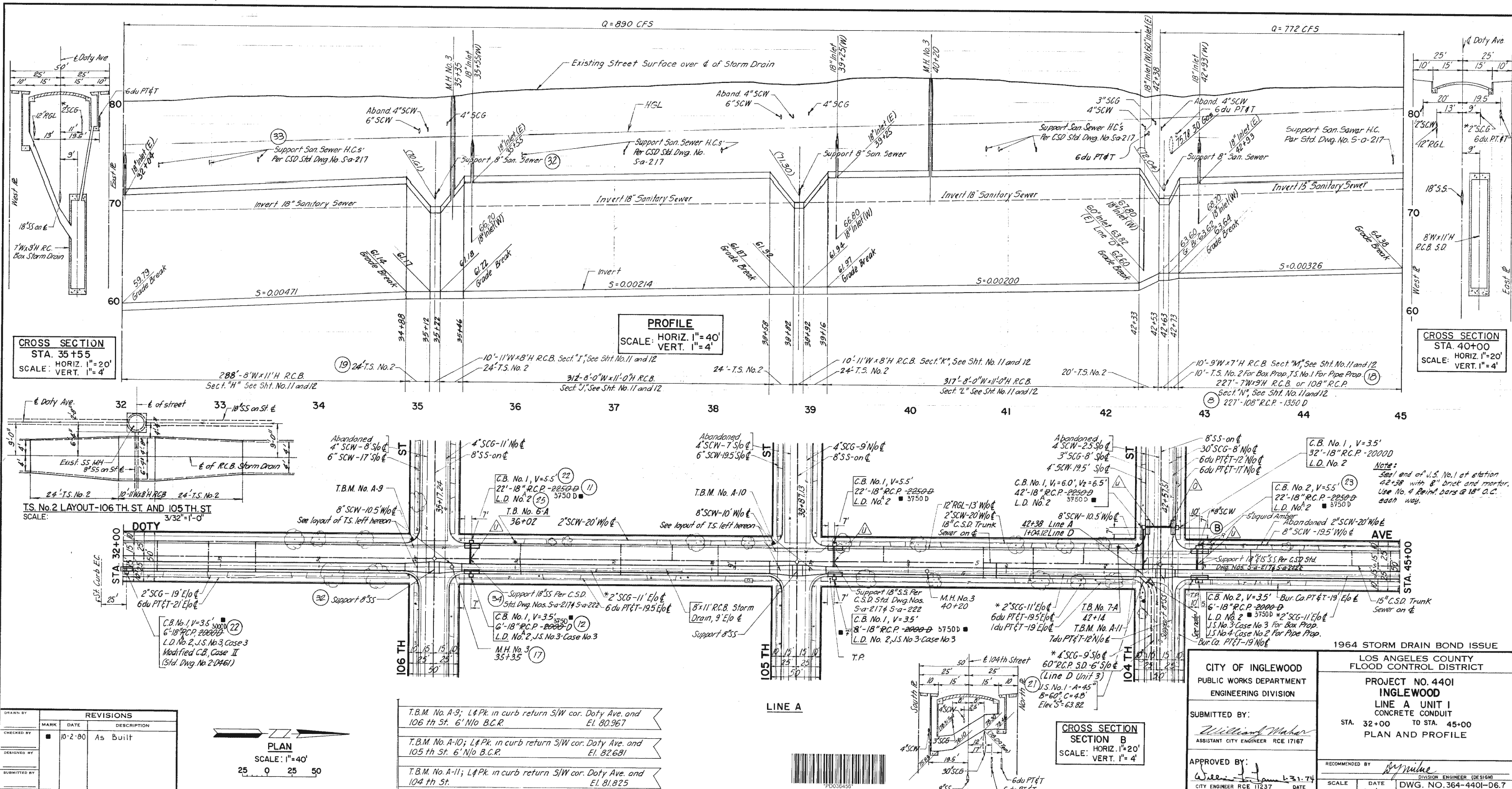
REVISIONS			
DRAWN BY	MARK	DATE	DESCRIPTION
CHECKED BY			
DESIGNED BY			
SUBMITTED BY			



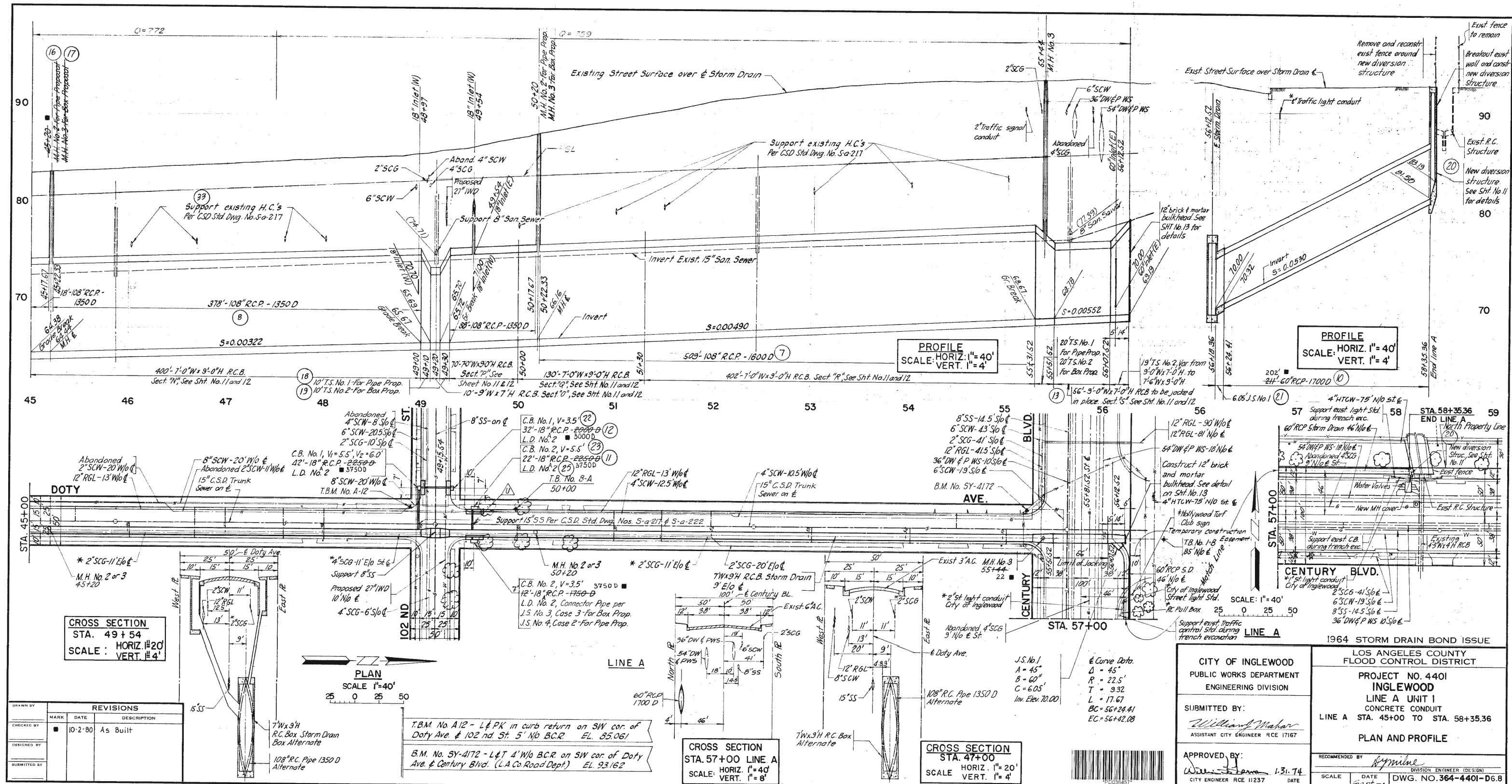








"AS BUILT" DRAWING



**CROSS SECTION**  
STA. 49+54  
SCALE: HORIZ. 1"=20'  
VERT. 1"=4'

**PLAN**  
SCALE: 1"=40'

**CROSS SECTION**  
STA. 57+00 LINE A  
SCALE: HORIZ. 1"=20'  
VERT. 1"=4'

**CROSS SECTION**  
STA. 47+00  
SCALE: HORIZ. 1"=20'  
VERT. 1"=4'

REVISIONS			
MARK	DATE	DESCRIPTION	
1	10-2-80	As Built	

**CITY OF INGLEWOOD**  
PUBLIC WORKS DEPARTMENT  
ENGINEERING DIVISION

SUBMITTED BY:  
*William Maher*  
ASSISTANT CITY ENGINEER RCE 17167

APPROVED BY:  
*William Maher* 1.31.74  
CITY ENGINEER RCE 11237

1964 STORM DRAIN BOND ISSUE  
LOS ANGELES COUNTY  
FLOOD CONTROL DISTRICT

PROJECT NO. 4401  
**INGLEWOOD**  
LINE A UNIT 1  
CONCRETE CONDUIT  
LINE A STA. 45+00 TO STA. 58+35.36

**PLAN AND PROFILE**

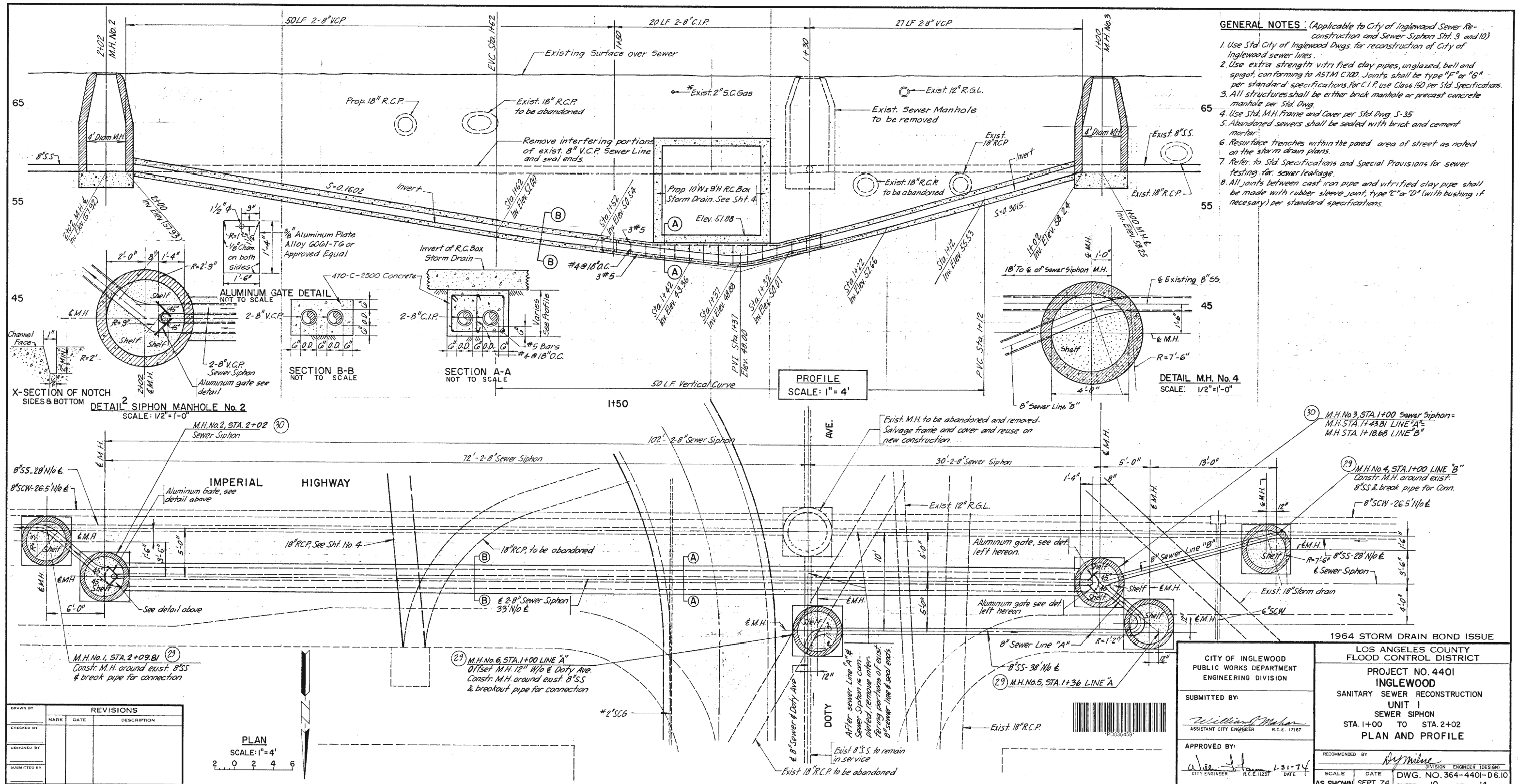
RECOMMENDED BY: *By mine*  
DIVISION ENGINEER (DESIGN)

SCALE: AS SHOWN  
DATE: Sept 74  
DWG. NO. 364-4401-06.8  
SHEET 8 OF 14

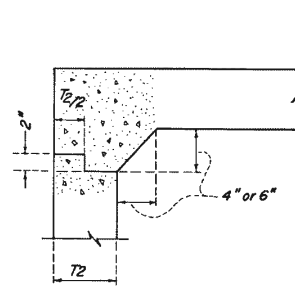
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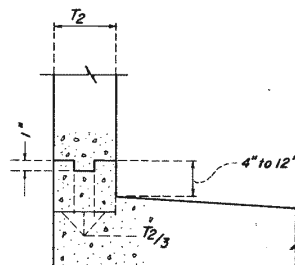




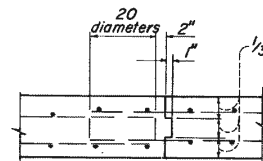
"AS BUILT" DRAWING



TOP OF WALL



BASE OF WALL



TRANSVERSE JOINT

CONSTRUCTION JOINT DETAILS  
NO SCALE

DESIGN DATA:

LIVE LOAD:

H20-S16-44 unless otherwise noted

DEAD LOAD:

Earth load per Marston's formula:  $W=120$  PCF

$K_u = K_u' = 0.150$

$B_d$  = Outside width of box plus 3 feet

Side earth  $W = 40$  PSF per foot of depth

Internal water pressure: 62.4 p.s.f. per foot of depth

Weight of Concrete: 150 p.c.f.

ALLOWABLE STRESSES:

$f_c' = 4000$  p.s.i. at 28 days

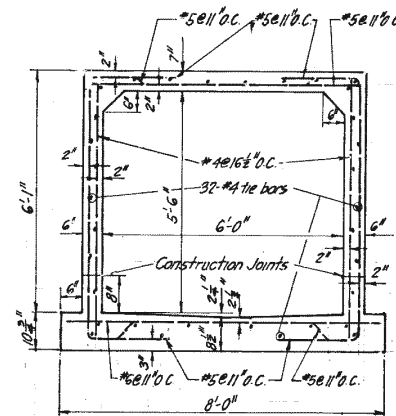
$f_c = 1800$  p.s.i.

$f_s = 24,000$  p.s.i.

$n = 8$

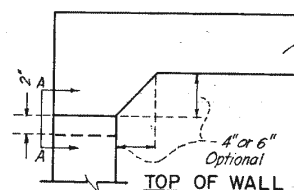
shear and bond stresses per A.C.I. 318-63

TYPICAL R.C. BOX SECTION  
NO SCALE

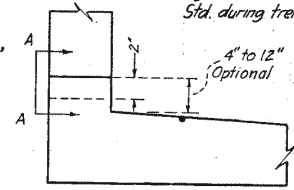


SECTION Z (Refer to Sheet No. 6)  
SCALE:  $1/2" = 1'-0"$

CONSTRUCTION JOINT DETAILS  
FOR BOXES JACKED IN PLACE

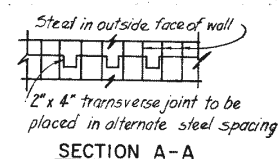


TOP OF WALL

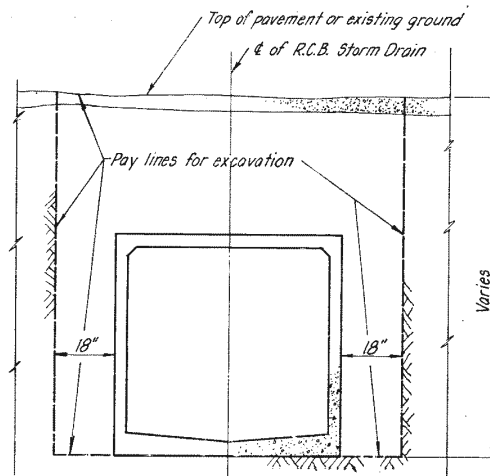


BASE OF WALL

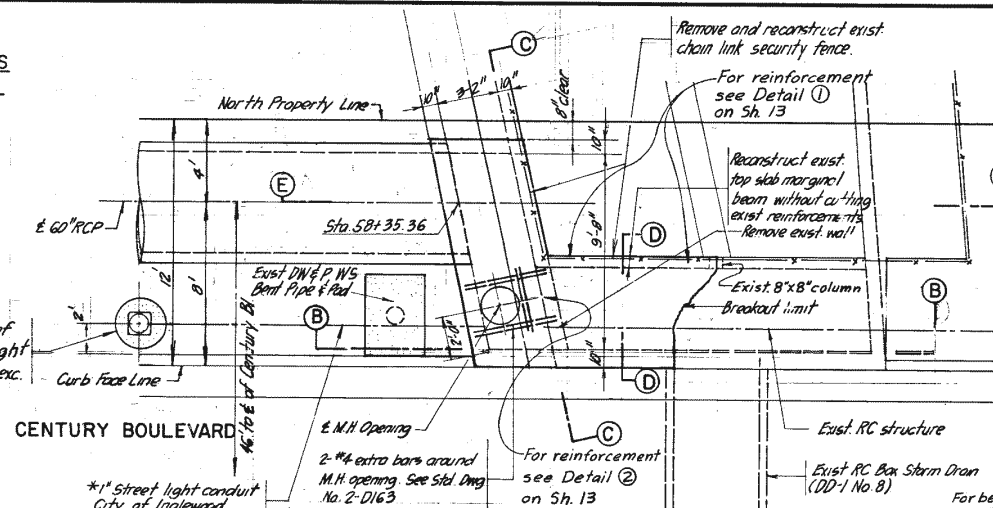
Refer to Std. Dwg. No. 2-D465 for additional steel details



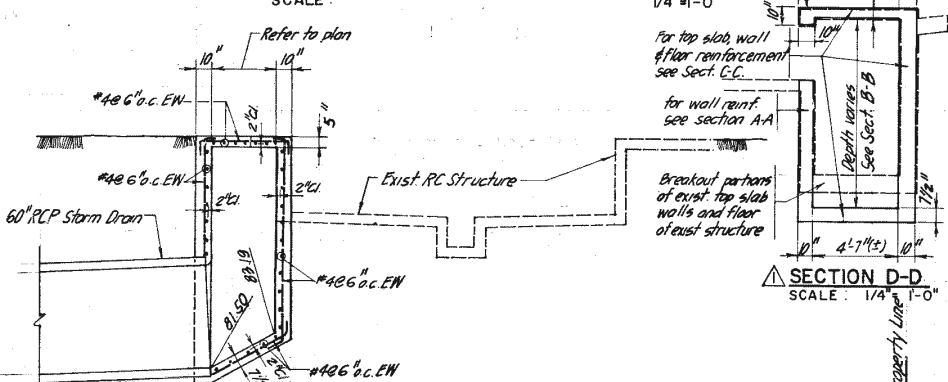
SECTION A-A



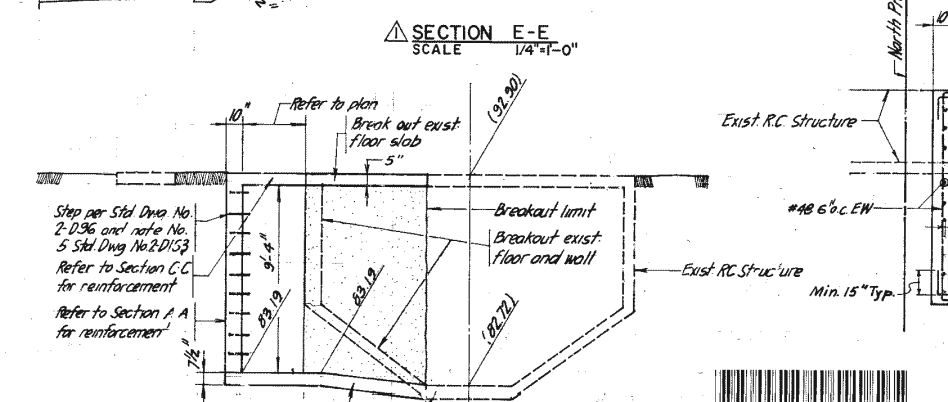
TYPICAL SECTION SHOWING PAY LINES  
FOR EXCAVATION OF R.C.B.  
NO SCALE



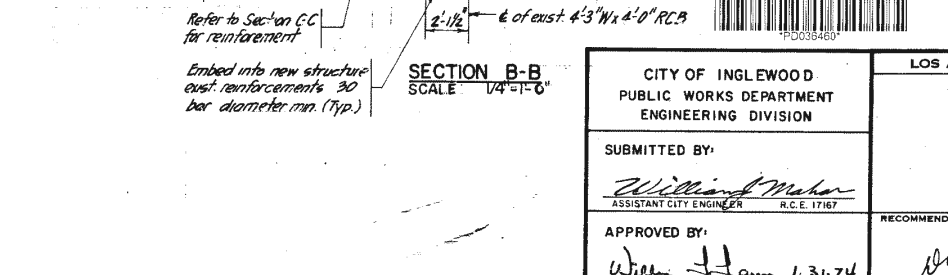
PLAN-PROPOSED DIVERSION STRUCTURE  
SCALE:  $1/4" = 1'-0"$



SECTION D-D  
SCALE:  $1/4" = 1'-0"$



SECTION E-E  
SCALE:  $1/4" = 1'-0"$



SECTION B-B  
SCALE:  $1/4" = 1'-0"$

REINFORCED CONCRETE  
BOX LOCATION SCHEDULE

LINE A		
BOX SECTION	FROM	TO
A	1+00	1+74.70
B	1+89.70	2+91.77
B	3+00	10+60
C	10+70	19+00
D	19+00	26+43
E	26+67	26+77
F	27+01	30+22.98
G	30+44.98	30+73.38
H	30+88.38	34+88
I	35+12	35+22
J	35+46	38+58
K	38+82	38+92
L	39+16	42+33
M	42+53	42+63
N	42+73	49+00
O	49+10	49+20
P	49+30	50+00
Q	50+00	51+30
R	51+30	55+31.52
S	55+51.52	56+07.52

SECTION C-C  
SCALE:  $1/4" = 1'-0"$

1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY FLOOD CONTROL DISTRICT

CITY OF INGLEWOOD  
PUBLIC WORKS DEPARTMENT  
ENGINEERING DIVISION

SUBMITTED BY:

William Maher  
ASSISTANT CITY ENGINEER R.C.E. 17167

APPROVED BY:

William Maher  
CITY ENGINEER R.C.E. 11237 DATE 1.31.74

RECOMMENDED BY:

William Maher  
DIVISION ENGINEER (DESIGN)

PROJECT NO. 4401  
INGLEWOOD  
SINGLE R.C. BOX UNIT I  
SCHEDULE & DETAILS

DATE 1.31.74 SCALE AS SHOWN

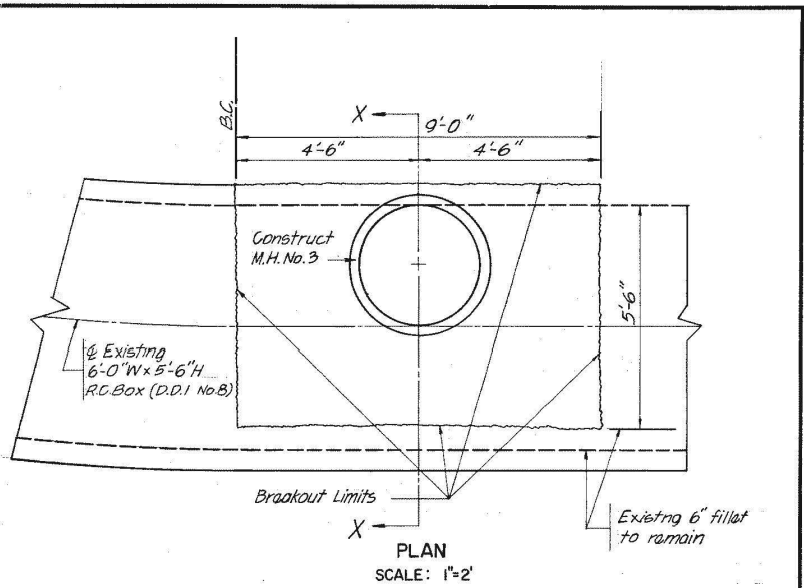
NO. 364-4401-D6.11

SHEET 11 OF 14

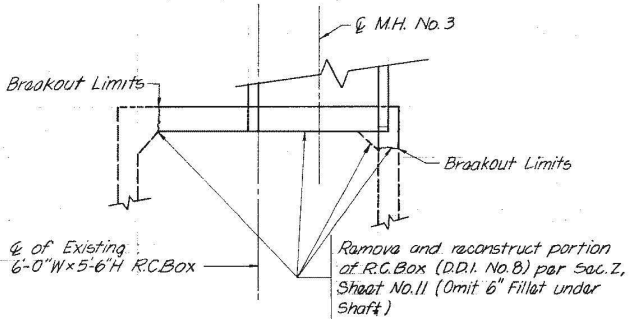
"AS BUILT" DRAWING



BOX SECTION		A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y
Design Cover (ft.)		4.2'	7.8'	8.8'	10.1'	13.0'	10.1'	12.3'	9.1'	11.0'	9.2'	12.0'	9.5'	10.5'	9.7'	11.8'	10.9'	12.9'	15.1'	16.7'	14.3'	13.0'	11.1'	8.9'	9.1'	9.7'
W	Width	7'-0"	10'-0"	8'-0"	8'-0"	11'-0"	8'-0"	11'-0"	8'-0"	11'-0"	8'-0"	11'-0"	8'-0"	9'-0"	7'-0"	9'-0"	7'-0"	7'-0"	7'-0"	9'-0"	7'-6"	7'-6"	7'-6"	7'-6"	7'-6"	7'-6"
H	Height	12'-0"	9'-0"	11'-0"	11'-0"	8'-0"	11'-0"	8'-0"	11'-0"	8'-0"	11'-0"	8'-0"	11'-0"	7'-0"	9'-0"	7'-0"	9'-0"	9'-0"	9'-0"	7'-0"	9'-0"	9'-0"	9'-0"	9'-0"	9'-0"	9'-0"
T <sub>1</sub>	Top Slab Thickness	6.50"	9.00"	8.25"	8.00"	12.50"	8.00"	12.00"	8.25"	11.00"	8.50"	11.75"	8.50"	9.00"	7.75"	9.75"	7.75"	8.50"	9.25"	12.00"	9.50"	9.00"	8.25"	7.75"	8.00"	8.25"
T <sub>2</sub>	Side Wall Thickness	3.00"	8.00"	8.00"	8.00"	8.75"	8.00"	8.50"	8.00"	8.25"	8.00"	8.50"	8.00"	8.00"	8.00"	8.00"	8.00"	8.00"	8.00"	8.75"	8.00"	8.00"	8.00"	8.00"	8.00"	8.00"
T <sub>3</sub>	Bottom Slab Thickness	7.00"	10.00"	9.25"	9.25"	13.50"	9.25"	13.00"	9.25"	12.00"	9.50"	12.75"	9.75"	10.25"	8.75"	10.75"	8.75"	9.50"	10.25"	13.00"	10.50"	10.00"	9.25"	8.75"	8.75"	9.25"
B	Bar No. & Spacing	#6@17"	#9@16"	#8@18"	#6@11"	#8@10"	#6@11"	#8@10"	#8@18"	#7@8"	#8@18"	#7@8"	#8@18"	#8@15"	#7@15"	#7@10"	#7@17"	#8@19"	#9@20"	#9@13"	#9@20"	#7@13"	#8@19"	#6@11"	#8@19"	#8@17"
Bars	Length, h	8'-1"	11'-1"	9'-1"	9'-1"	12'-25"	9'-1"	12'-2"	9'-1"	12'-15"	9'-1"	12'-2"	9'-1"	10'-1"	8'-1"	10'-1"	8'-1"	8'-1"	8'-1"	10'-25"	8'-7"	8'-7"	8'-7"	8'-7"	8'-7"	8'-7"
B	Bar No. & Spacing	#5@17"	#5@16"	#5@18"	#4@11"	#5@10"	#4@11"	#5@10"	#5@18"	#4@8"	#5@18"	#4@8"	#5@18"	#5@15"	#4@15"	#4@10"	#5@17"	#5@19"	#4@20"	#4@13"	#5@20"	#4@13"	#5@19"	#4@11"	#5@19"	#4@17"
Bars	Length, h	5'-0.5"	5'-11.5"	5'-1"	5'-2"	7'-1.5"	5'-2"	6'-10.5"	5'-2"	6'-9"	5'-2"	7'-1"	5'-2.5"	5'-9"	4'-5"	5'-7"	4'-8.5"	4'-7.5"	4'-0.5"	5'-5"	4'-10.5"	4'-11"	4'-10.5"	4'-11"	4'-10.5"	4'-5.5"
C	Bar No. & Spacing	#4@11"	#4@12"	#4@12"	#4@12"	#4@13"	#4@12"	#4@12"	#4@11"	#4@11"	#4@12"	#4@12"	#4@11"	#4@11"	#4@14"	#4@14"	#4@14"	#4@14"	#4@14"	#4@13"	#4@14"	#4@14"	#4@14"	#4@13"	#4@13"	#4@14"
	Horiz. Length, h	3'-5.5"	4'-2.5"	3'-8.5"	3'-8.5"	4'-6.5"	3'-8.5"	4'-6"	3'-8.5"	4'-6"	3'-8.5"	4'-6"	3'-8.5"	3'-11.5"	3'-5.5"	3'-11.5"	3'-5.5"	3'-5.5"	3'-5.5"	4'-0.5"	3'-7"	3'-7"	3'-7"	3'-7"	3'-7"	3'-7.0"
	Vert. Length, v	11'-11.5"	9'-2"	11'-1.5"	11'-1"	8'-5.5"	11'-1"	8'-5"	11'-1.5"	8'-4"	11'-1.5"	8'-5"	11'-1.5"	7'-2"	9'-1"	7'-3"	9'-1"	9'-1.5"	9'-2.5"	7'-5"	9'-2.5"	9'-2"	9'-1.5"	9'-1"	9'-1.0"	9'-1.5"
C <sub>1</sub>	Bar No. & Spacing	#5@11"	#5@12"	#6@12"	#6@12"	#5@13"	#6@12"	#5@12"	#5@11"	#5@11"	#6@12"	#5@12"	#5@11"	#4@11"	#5@14"	#5@14"	#5@14"	#5@14"	#5@14"	#4@13"	#5@14"	#5@14"	#5@14"	#5@13"	#5@13"	#5@14"
	Horiz. Length, h	2'-2.5"	1'-10"	1'-10"	1'-9"	2'-0.5"	1'-9"	1'-11.5"	1'-9"	1'-10"	1'-10"	1'-11"	1'-9.5"	1'-6.5"	1'-6.5"	1'-8"	1'-6.5"	1'-7"	1'-7.5"	1'-9"	1'-8"	1'-8"	1'-7"	1'-6.5"	1'-6.5"	1'-7.0"
	Vert. Length, v	1'-7"	3'-5"	2'-1"	2'-0.5"	2'-11.5"	2'-0.5"	2'-11.5"	2'-0"	3'-1"	2'-1"	3'-0"	2'-0.5"	2'-6.5"	1'-9.5"	2'-11"	1'-9.5"	2'-11"	1'-10"	1'-10.5"	2'-2"	1'-11.5"	1'-11.5"	1'-11"	1'-10.5"	1'-10.5"
C <sub>2</sub>	Bar No. & Spacing	#5@11"	#5@12"	#4@12"	#4@12"	#4@13"	#4@12"	#4@12"	#4@11"	#4@11"	#4@12"	#4@12"	#4@11"	#4@11"	#4@14"	#4@14"	#4@14"	#4@14"	#4@14"	#4@13"	#4@14"	#4@14"	#4@14"	#4@13"	#4@13"	#4@14"
	Horiz. Length, h	3'-9"	4'-3.5"	3'-8.5"	3'-8.5"	4'-6.5"	3'-8.5"	4'-6"	3'-8.5"	4'-6"	3'-8.5"	4'-6"	3'-8.5"	3'-11.5"	3'-5.5"	3'-11.5"	3'-5.5"	3'-5.5"	3'-5.5"	4'-0.5"	3'-7"	3'-7"	3'-7"	3'-7"	3'-7"	3'-7.0"
	Vert. Length, v	2'-0"	2'-3"	2'-2.5"	2'-2.5"	2'-6.5"	2'-2.5"	2'-6"	2'-2.5"	2'-5"	2'-2.5"	2'-6"	2'-3"	2'-3.5"	2'-2"	2'-4"	2'-2"	2'-2.5"	2'-3.5"	2'-6"	2'-3.5"	2'-3"	2'-2.5"	2'-2"	2'-2.0"	2'-2.5"
C <sub>3</sub>	Bar No. & Spacing	#5@11"	#4@12"	#6@12"	#6@12"	#4@13"	#6@12"	#4@12"	#6@11"	#4@11"	#5@12"	#4@12"	#5@11"	#4@11"	#5@14"	#4@14"	#5@14"	#5@14"	#5@14"	#4@13"	#5@14"	#5@14"	#5@14"	#5@13"	#5@13"	#5@14"
	Horiz. Length, h	1'-8.5"	1'-6"	2'-1"	2'-1"	1'-11"	2'-1"	1'-10"	1'-10.5"	1'-8.5"	2'-0.5"	1'-10"	1'-11"	1'-6"	1'-7.5"	1'-7.5"	1'-7.5"	1'-8"	1'-8.5"	1'-8"	1'-9"	1'-8.5"	1'-8"	1'-7.5"	1'-7.5"	1'-8"
	Vert. Length, v	1'-3"	1'-11.5"	2'-0"	2'-0.5"	2'-6.5"	2'-0.5"	2'-7.5"	2'-0"	2'-9.5"	2'-0.5"	2'-9"	2'-0"	2'-4.5"	1'-9.5"	5'-7.5"	1'-9.5"	1'-10.5"	1'-11"	1'-10.5"	1'-10.5"	1'-11"	1'-10.5"	1'-10"	1'-10"	1'-10.5"
D	Bar No. & Spacing	#5@9"	#4@18"	#4@9"	#4@9"	#4@18"	#4@9"	#4@18"	#4@9"	#4@18"	#4@9"	#4@18"	#4@9"	#4@18"	#4@17"	#4@18"	#4@17"	#4@17"	#4@18"	#4@18"	#4@18"	#4@18"	#4@17"	#4@17"	#4@17"	#4@17"
Bars	Length, v	12'-10.5"	10'-4"	12'-2.5"	12'-2.5"	9'-11"	12'-2.5"	9'-10"	12'-2.5"	9'-8"	12'-3"	9'-9.5"	12'-3"	8'-4"	10'-1.5"	8'-5.5"	10'-1.5"	10'-3"	10'-4.5"	8'-10"	10'-5"	10'-4"	10'-2.5"	10'-1.5"	10'-1.5"	10'-2.5"
F	Bar No. & Spacing	#7@17"	#8@11"	#9@19"	#9@19"	#9@11"	#9@19"	#9@11"	#8@14"	#9@12"	#8@14"	#8@9"	#8@14"	#9@16"	#7@13"	#9@15"	#7@13"	#9@20"	#9@18"	#9@12"	#9@16"	#8@14"	#7@12"	#9@20"	#9@20"	#9@20"
Bars	Length, h	8'-1"	11'-1"	9'-1"	9'-1"	12'-2.5"	9'-1"	12'-2"	9'-1"	12'-1.5"	9'-1"	12'-2"	9'-1"	10'-1"	8'-1"	10'-1"	8'-1"	8'-1"	8'-1"	10'-2.5"	8'-7"	8'-7"	8'-7"	8'-7"	8'-7"	8'-7"
F <sub>1</sub>	Bar No. & Spacing	#5@17"	#4@11"	#5@19"	#5@19"	#5@11"	#5@19"	#5@11"	#4@14"	#5@12"	#4@14"	#4@9"	#4@14"	#5@16"	#4@13"	#5@15"	#4@13"	#5@20"	#4@18"	#4@12"	#4@16"	#4@14"	#4@12"	#5@20"	#5@20"	#5@20"
Bars	Length, h	4'-11"	6'-0.5"	5'-3.5"	5'-3"	7'-1"	5'-3"	6'-9.5"	5'-0"	7'-1.5"	4'-11.5"	7'-1"	5'-0.5"	5'-11"	4'-9"	6'-0"	4'-8.5"	4'-9"	4'-6"	5'-9.5"	4'-5.5"	4'-11"	5'-1.5"	4'-11.5"	5'-0"	5'-1.5"
G	Bar No. & Spacing	#4@11"	#4@12"	#4@12"	#4@12"	#4@13"	#4@12"	#4@12"	#4@11"	#4@11"	#4@12"	#4@12"	#4@11"	#4@11"	#4@14"	#4@14"	#4@14"	#4@14"	#4@14"	#4@13"	#4@14"	#4@14"	#4@14"	#4@13"	#4@13"	#4@14"
Bars	Length, h	3'-6"	5'-0"	4'-0"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	4'-6"	3'-6"	4'-6"	3'-6"	3'-6"	3'-6"	4'-6"	3'-9"	3'-9"	3'-9"	3'-9"	3'-9"	3'-9"
H	Bar No. & Spacing	#5@11"		#4@12"	#4@12"	#4@13"	#4@12"	#4@12"	#4@11"	#4@11"	#4@12"	#4@12"	#4@11"	#4@11"	#4@14"	#4@14"	#4@14"	#4@14"	#4@14"	#4@13"	#4@13"	#4@14"	#4@14"	#4@13"	#4@13"	#4@14"
Bars	Length, h	3'-6"		4'-0"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	5'-6"	4'-0"	4'-6"	3'-6"	4'-6"	3'-6"	3'-6"	3'-6"	4'-6"	3'-9"	3'-9"	3'-9"	3'-9"	3'-9"	3'-9"
		NUMBER OF LONGITUDINAL REINFORCEMENT # 4 BARS																				NO. OF LONG. REINF. # 4 BARS				
Top Slab (Includes Distrib.)		13	17	14	14	19	14	19	14	19	14	19	14	16	13	16	13	13	13	16	14	14	14	14	14	14
Bottom Slab		13	16	14	14	19	14	19	14	19	14	19	14	16	13	16	13	13	13	16	14	14	14	14	14	14
Side Walls		32	24	28	28	20	28	20	28	20	28	20	28	16	24	16	24	24	24	16	24	24	24	24	24	24
TOTAL		58	57	56	56	58	56	58	56	58	56	58	56	48	50	48	50	50	50	48	52	52	52	52	52	52
		QUANTITIES																				QUANTITIES				
Concrete Cu. Yds./Lin. Ft.		0.96	1.13	1.07	1.06	1.46	1.06	1.40	1.07	1.31	1.08	1.38	1.09	0.98	0.89	1.02	0.89	0.93	0.97	1.21	1.01	0.98	0.94	0.92	0.92	0.94
Steel Lbs. / Lin. Ft.		159.5	167.0	158.5	157.2	195.1	157.2	197.7	159.6	194.0	159.6	191.6	156.2	139.3	113.4	142.6	112.9	116.3	118.6	150.2	127.0	124.0	120.9	122.8	123.0	121.2
		LINE A																				LINE B				



DETAILS OF REMOVAL AND RECONSTRUCTION OF  
A PORTION OF D.D.I. No. 8 IN 107<sup>th</sup> STREET  
(24) (REFER TO SHEET No. 6)



SECTION X-X  
SCALE: 1"=2'

NOTE: Refer to Sheet 3 for Concrete Breakout Notes



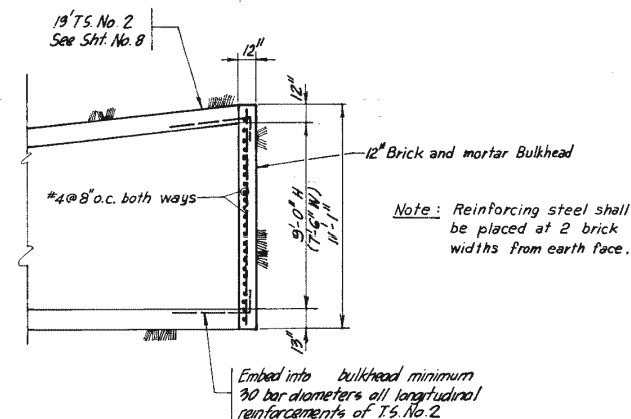
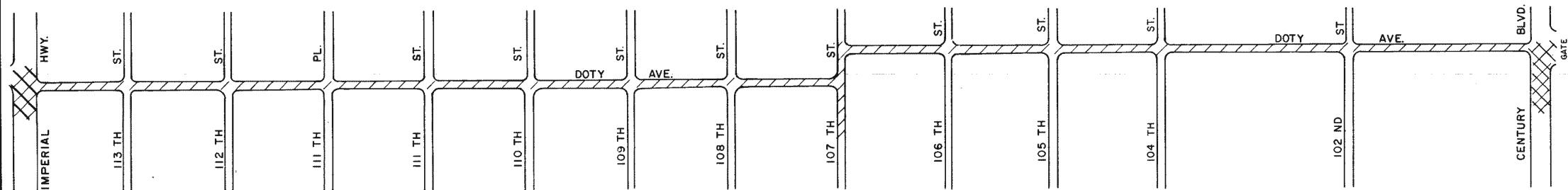
1964 STORM DRAIN BOND ISSUE

REVISIONS	
MARK	DESCRIPTION

CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION		LOS ANGELES COUNTY FLOOD CONTROL DISTRICT	
SUBMITTED BY:  Assistant City Engineer R.C.E. 17167		PROJECT NO. 4401 INGLEWOOD LINE A UNIT I  SINGLE R.C. BOX SCHEDULE	
APPROVED BY:  City Engineer R.C.E. 11237 DATE 1-31-74		RECOMMENDED BY:  Division Engineer (Design)	
SCALE AS SHOWN		DATE SEPT 74	
DWG. NO. 364-4401-06.12		SHEET 12 OF 14	

"AS BUILT" DRAWING

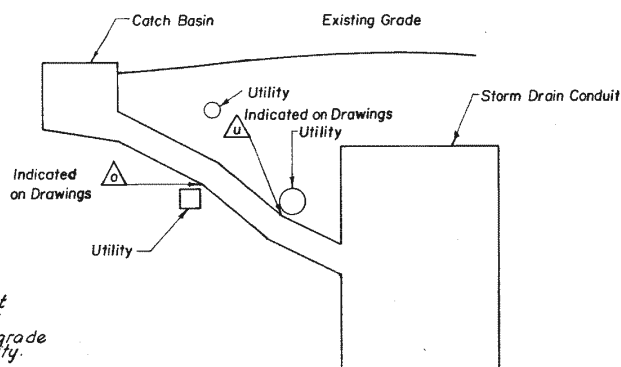




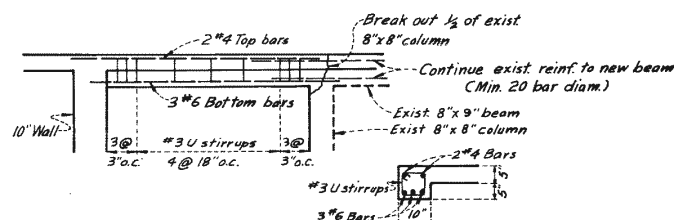
**BULKHEAD DETAIL (Refer to sheet No. 8)**  
SCALE: 1/4" = 1'-0"

**NOTES:**

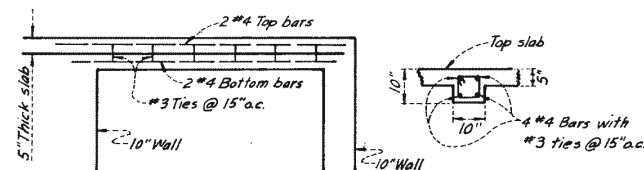
1. The change in grade of the connector pipe may occur either over or under an existing utility. The utilities at which the grade change occur are shown on the project drawings. At locations where utility crossings are marked  $\Delta$  the connector pipe will break over the utility. At locations where the utility crossings are marked  $\Delta$  the connector pipe will break under the utility.
2. On those connector pipes where change of grade is not indicated, it is assumed that the connector pipe can be laid on a straight grade from the catch basin to the storm drain without interference with utilities.
3. Where connector pipe has a change of grade exceeding 1/10'FT or differs in diameter from that of existing pipe, use concrete collar per standard DWG 2-D393.
4. The Contractor shall make exploratory excavation to determine the exact location and depth of utilities except sanitary sewers which are marked  $\Delta$  or  $\Delta$ . After the exact location of a utility has been determined, the grade and alignment of the connector pipe will be stated so as to clear the utility.



**TYPICAL CONNECTOR PIPE PROFILE**  
NO SCALE



**DETAIL 1**  
NOT TO SCALE

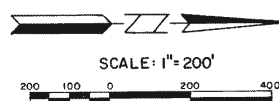


**DETAIL 2**  
NOT TO SCALE

**Pavement Reconstruction Legend**

Existing Section	Reconstruction Section
3" A.C. over 6" A.B.	4" A.C. over 6" C.A.B.
2" A.C. over 4" Base	3" A.C. over 4" C.A.B.
6" A.C. over 8" A.B.	6" A.C. over 8" C.A.B.
5" A.C. over 12" A.B.	6" A.C. over 12" C.A.B.

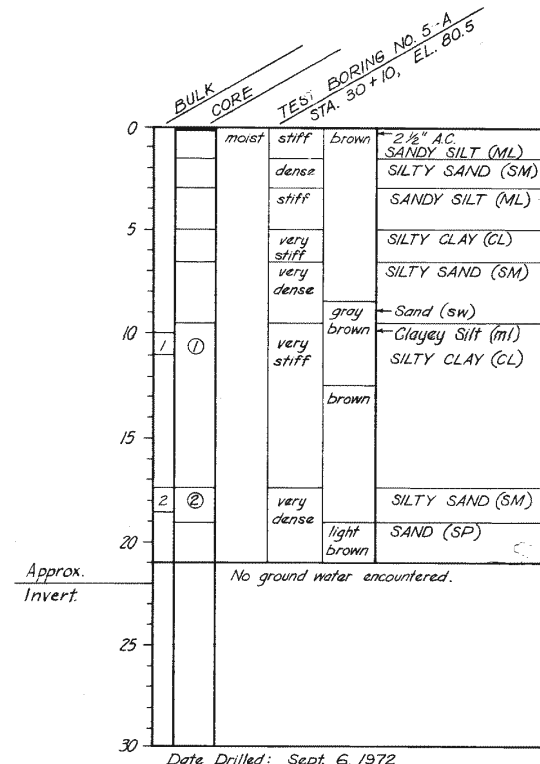
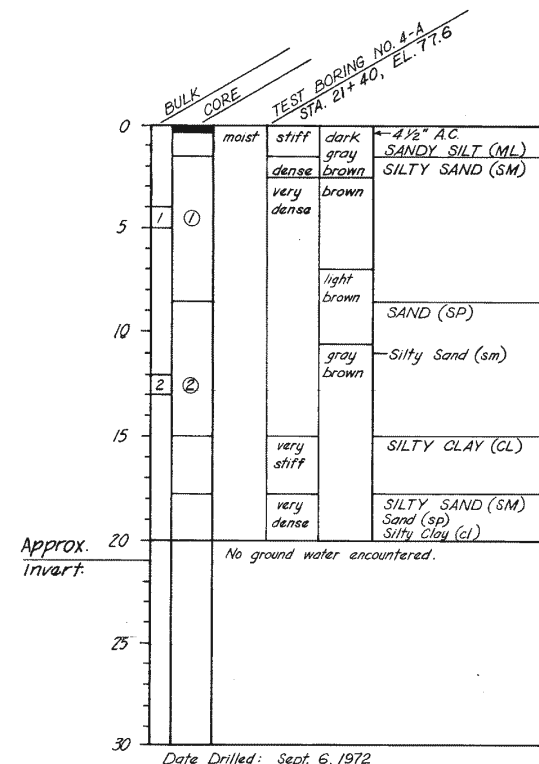
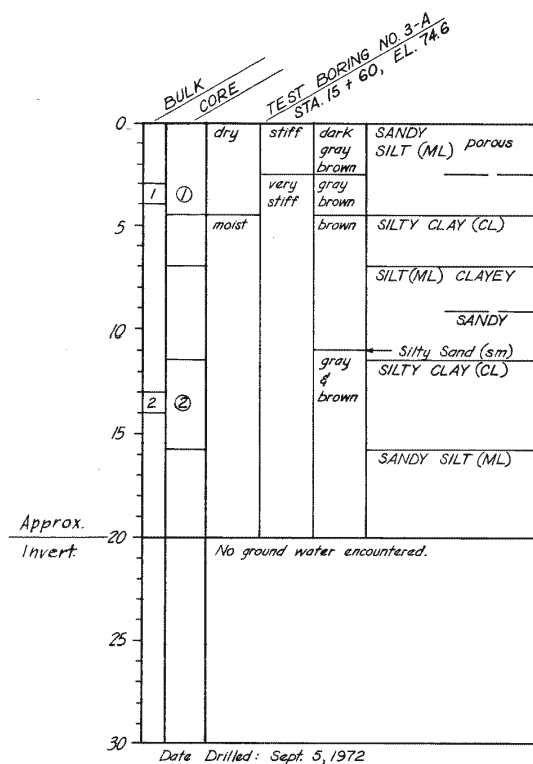
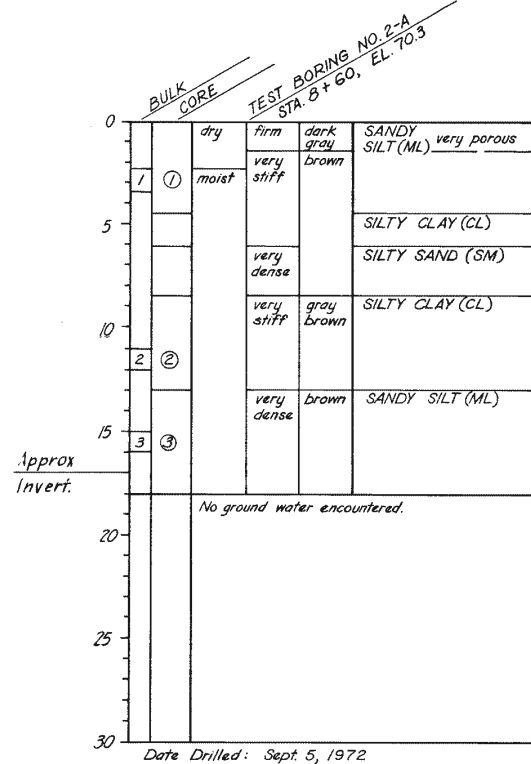
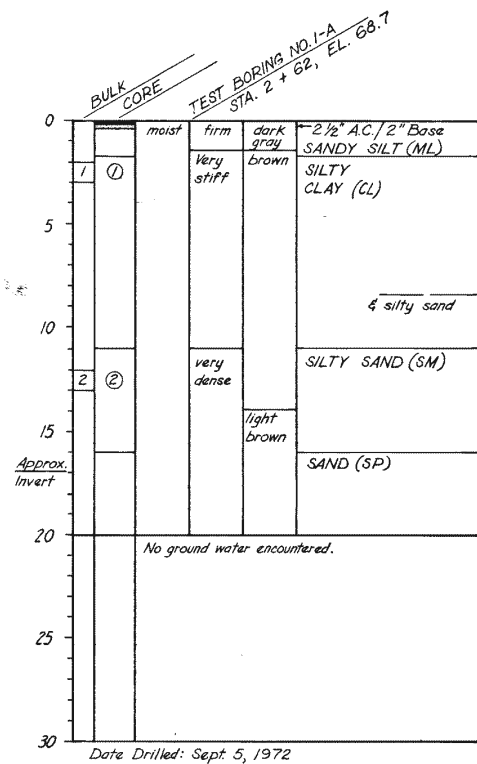
REVISIONS
NO. DATE DESCRIPTION
1 12-9-74 Addition of Details



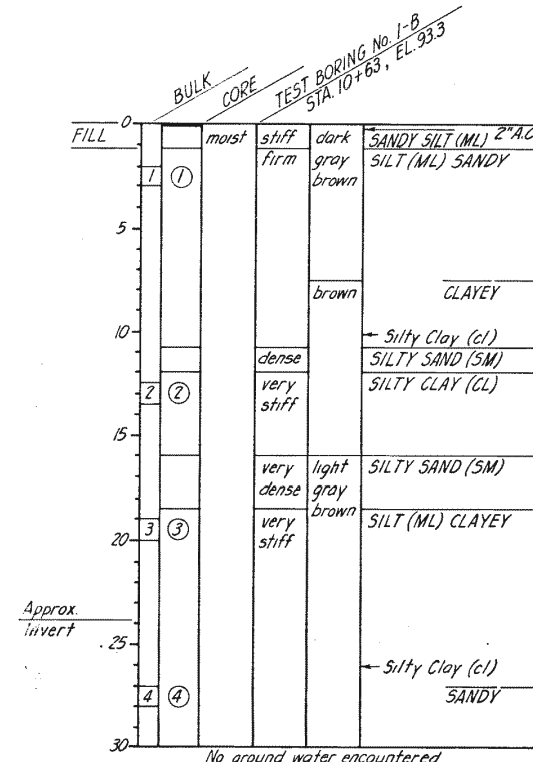
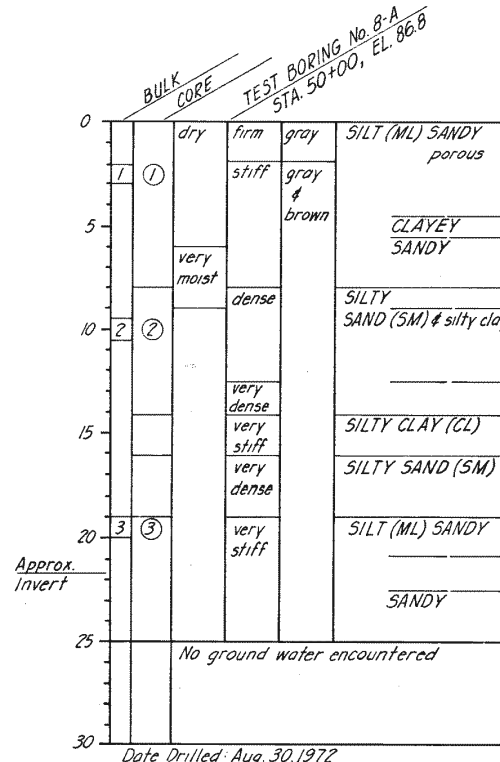
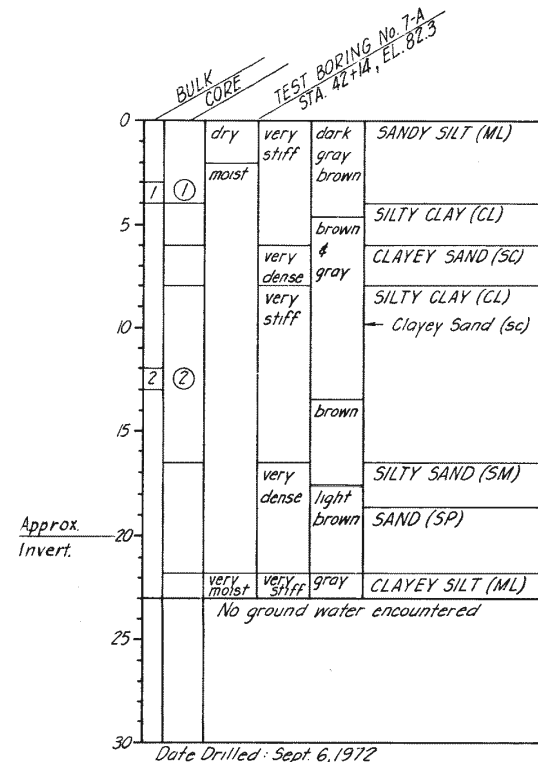
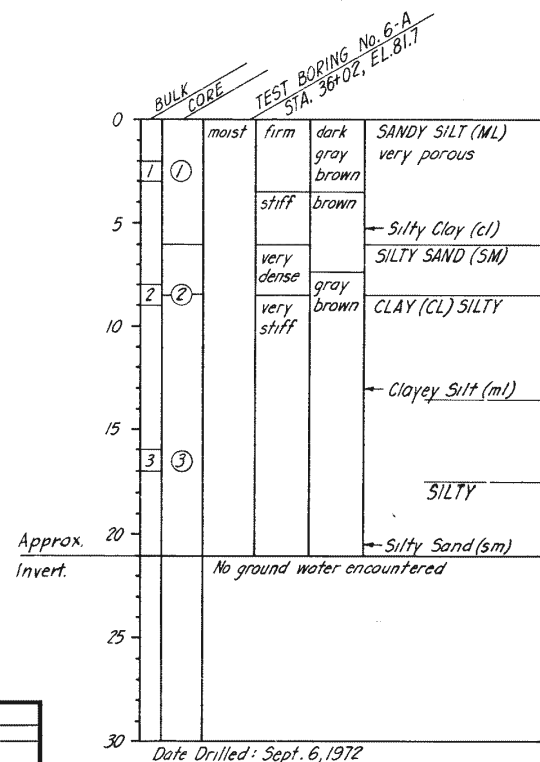
1964 STORM DRAIN BOND ISSUE

CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION		LOS ANGELES COUNTY FLOOD CONTROL DISTRICT	
SUBMITTED BY: <i>William M. Mohr</i> ASSISTANT CITY ENGINEER R.C.E. 17161		PROJECT NO. 4401 INGLEWOOD RESURFACING PLAN UNIT 1	
APPROVED BY: <i>W. H. Hama</i> CITY ENGINEER R.C.E. 11237 DATE 1-31-74		RECOMMENDED BY: <i>W. H. Hama</i> DIVISION ENGINEER (DESIGN)	DATE SEPT 74 SCALE AS SHOWN NO. 364-4401-D6 13 SHEET 13 OF 14

"AS BUILT" DRAWING



- NOTES:
1. Soil classification was made in accordance with the Unified Soil Classification System shown on Std. Dwg. No. 2-D413.
  2. Borings were drilled with an 18" diameter Truck-Mounted Rotary Bucket Auger.
  3. Approximate invert elevations shown above Supersedes Soils Report.



CITY OF INGLEWOOD  
PUBLIC WORKS DEPARTMENT  
ENGINEERING DIVISION

SUBMITTED BY:  
*William Maher*  
ASSISTANT CITY ENGINEER R.C.E. 17167

APPROVED BY:  
*John J. ...*  
CITY ENGINEER R.C.E. 11237 DATE 1-31-74



1964 STORM DRAIN BOND ISSUE

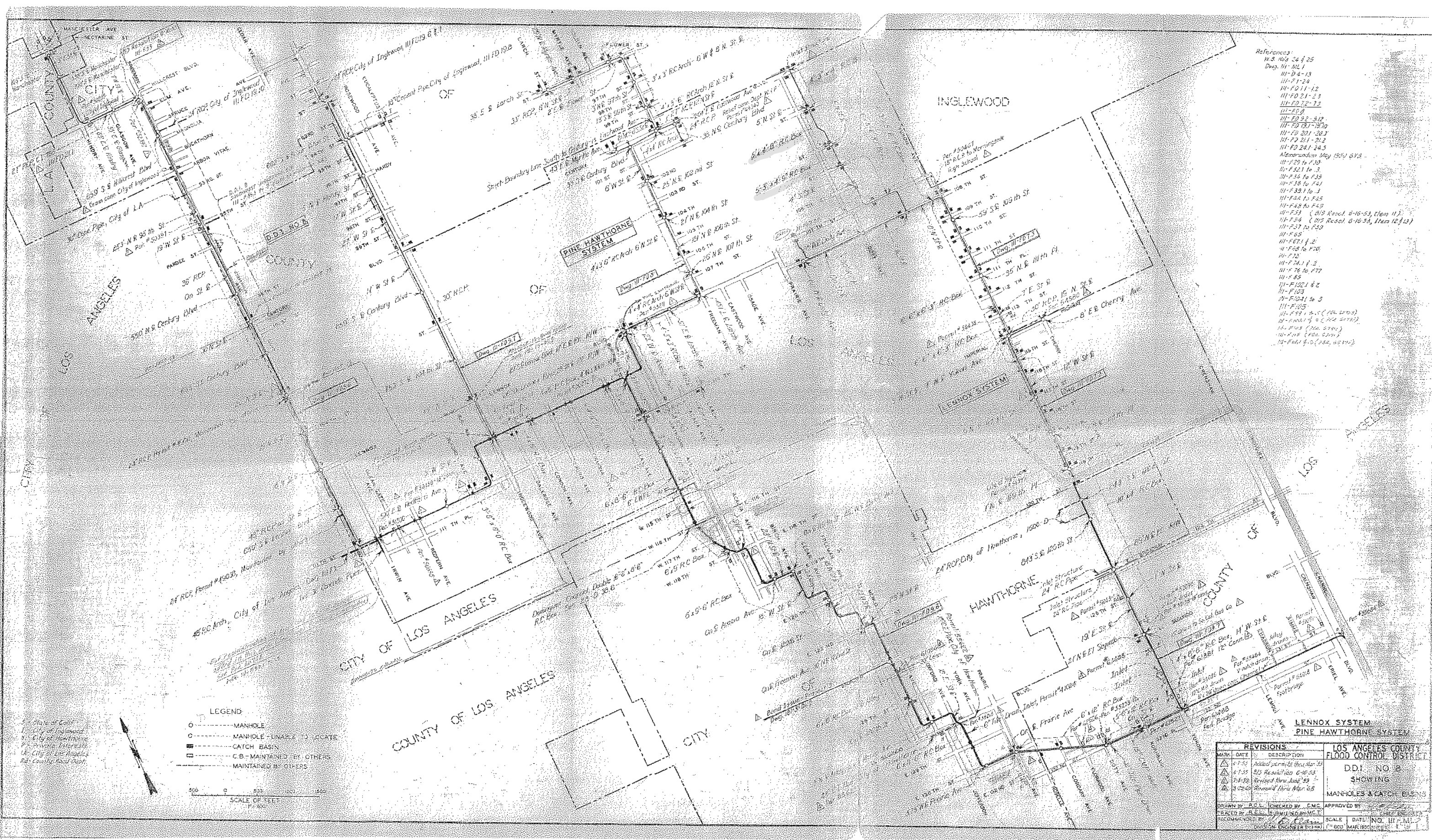
LOS ANGELES COUNTY FLOOD CONTROL DISTRICT

PROJECT NO. 4401  
INGLEWOOD  
LINE A UNIT I  
LOG OF BORINGS

RECOMMENDED BY: *Almyline* DATE SEPT 74 SCALE AS SHOWN  
DIVISION ENGINEER (DESIGN) NO. 364-4401-D614

SHEET 4 OF 14

AS BUILT DRAWING

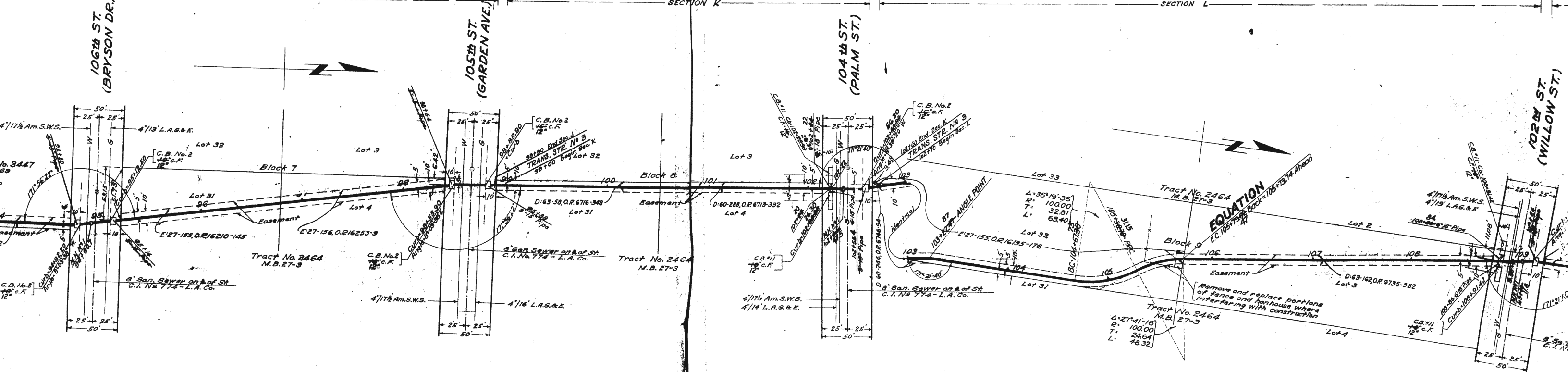
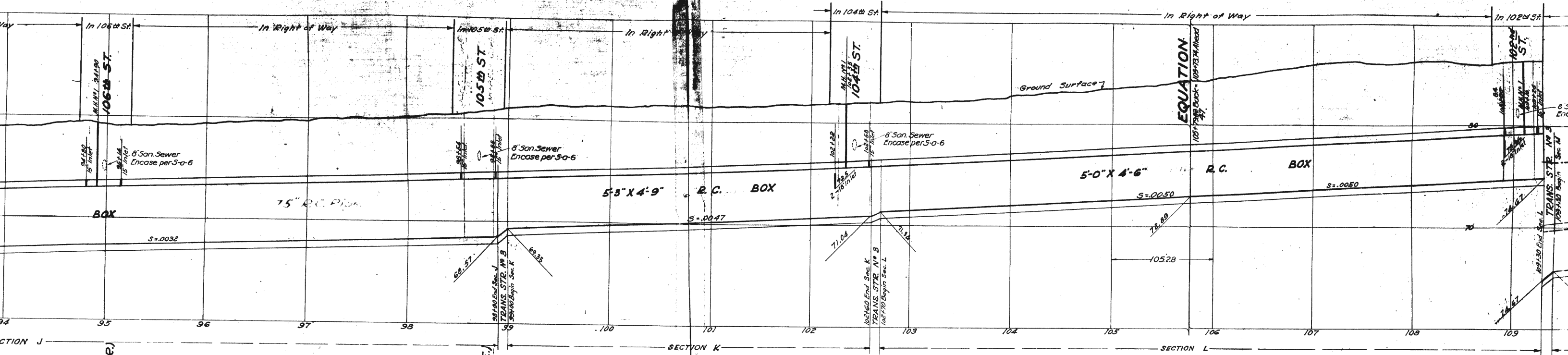


- References:
- W.S. No. 24 & 25
  - Map No. 1
  - Map No. 2
  - Map No. 3
  - Map No. 4
  - Map No. 5
  - Map No. 6
  - Map No. 7
  - Map No. 8
  - Map No. 9
  - Map No. 10
  - Map No. 11
  - Map No. 12
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  - Map No. 94
  - Map No. 95
  - Map No. 96
  - Map No. 97
  - Map No. 98
  - Map No. 99
  - Map No. 100

REVISIONS			LOS ANGELES COUNTY FLOOD CONTROL DISTRICT
MARK	DATE	DESCRIPTION	
△	4-1-52	Added permits thru Mar 52	D.D. NO. 8 SHOWING MANHOLES & CATCH BASINS
△	4-1-52	Added permits thru Mar 52	
△	4-1-52	Added permits thru Mar 52	
△	4-1-52	Added permits thru Mar 52	
DRAWN BY: R.C.L. CHECKED BY: C.M.C. APPROVED BY: [Signature]			SCALE: 1" = 100' DATE: NO. 111, M.L. 1
RECOMMENDED BY: [Signature] DIVISION ENGINEER			





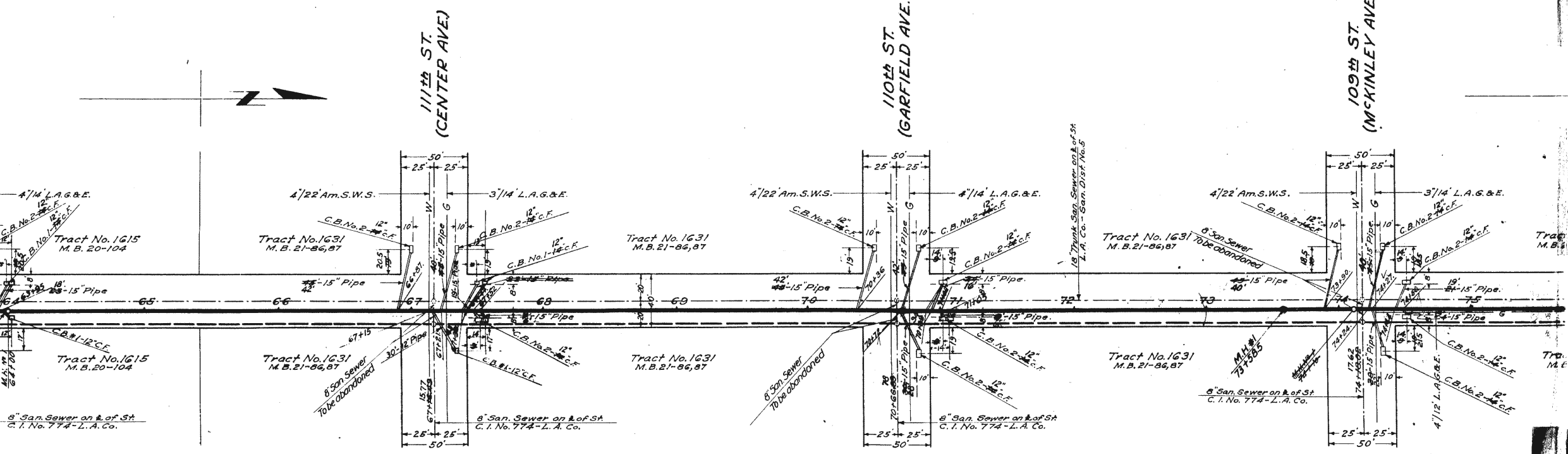
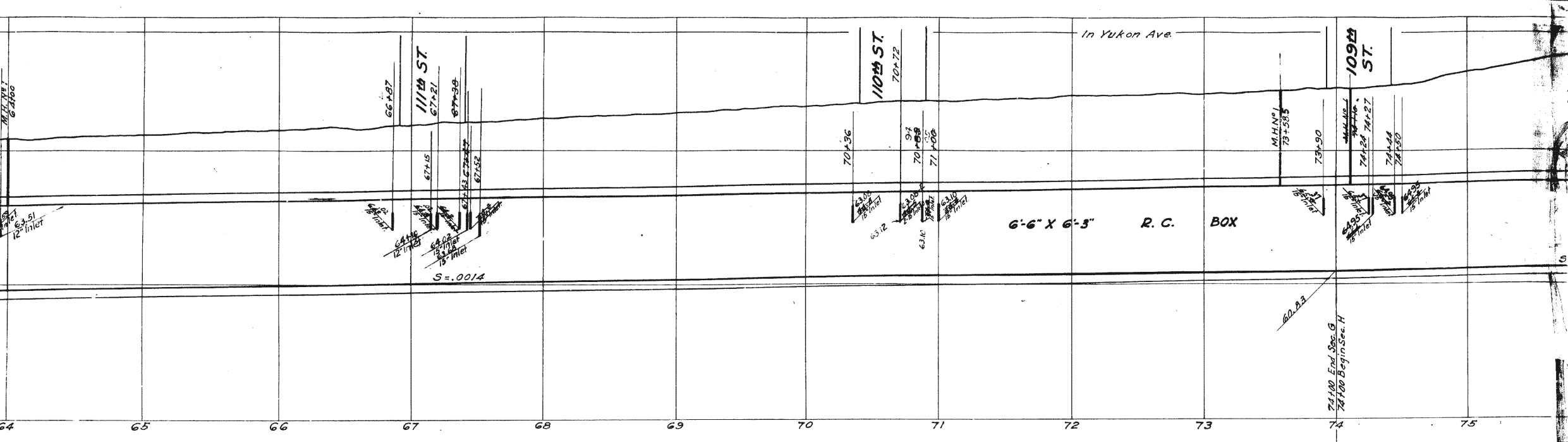


Note:  
Elevations for top of curb at catch basins  
to be determined in field, making top of curb  
4' higher than crown of street.

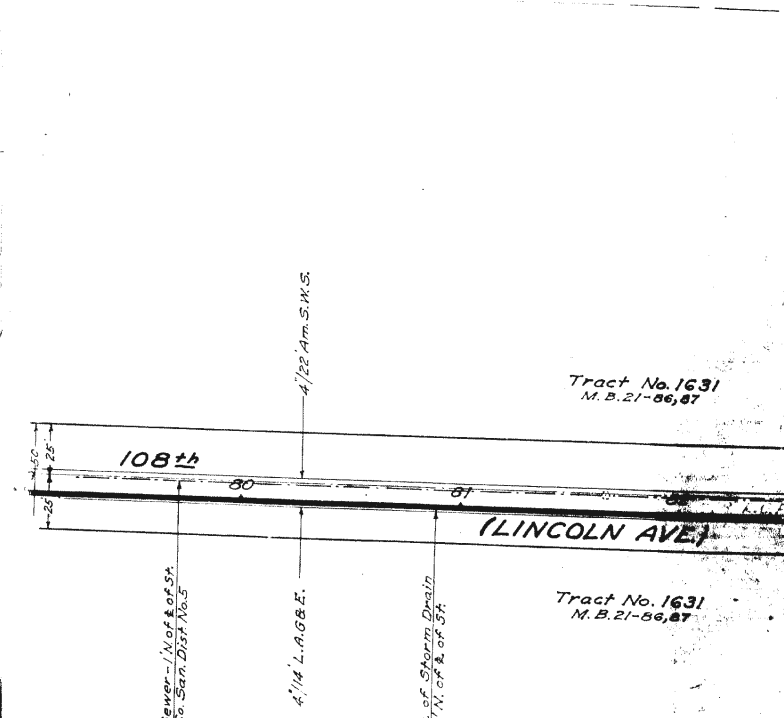
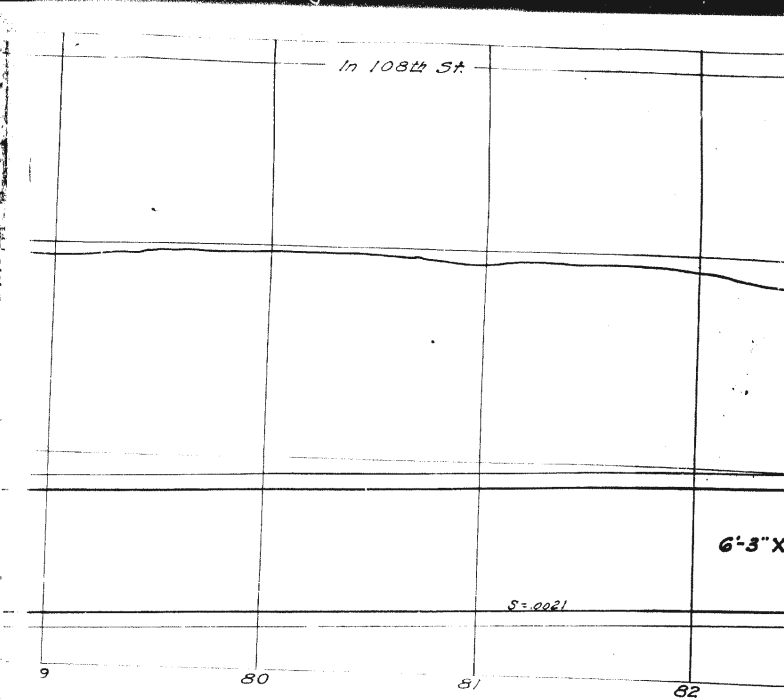
Note:  
Elevations for top of curb to  
in field, making top of curb  
4' higher than crown of st.

YUKON AVENUE





Note:  
Elevations for top of curb at catch basins  
to be determined in field, making top of curb  
4" higher than crown of street.



LINE

YUKON

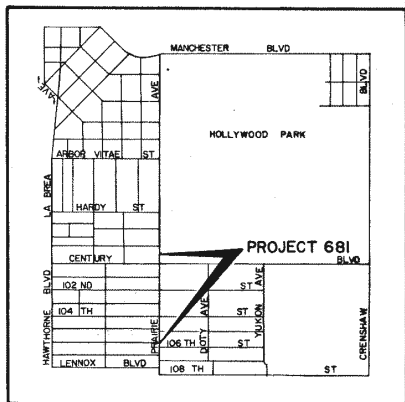
AVE





# LEGEND & ABBREVIATIONS

PROPERTY LINE	
CURB	
GUTTER	
SIDE INLET CATCH BASIN	
EXISTING DRAINAGE STRUCTURES	
GRATING TYPE CATCH BASIN	
DRIVEWAY	
LIMIT OF CONCRETE SURFACE	
WALK	
TRAFFIC SIGNAL	
DEAD MAN	
POWER, TELEPHONE OR GUY POLE	
FIRE HYDRANT	
ELECTROLIER	
WATER & GAS METER	
BENCH MARK	
TEST BORING	
TREE	
TREES TO BE REPLACED BY CONTRACTOR	
UNDER EXISTING UTILITY	
OVER EXISTING UTILITY	
TRAFFIC SIGNAL CONDUIT	T.S.C.
TRANSITION STRUCTURE	T.S.
MANHOLE	M.H.
LOCAL DEPRESSION	L.D.
REINFORCED CONCRETE PIPE	R.C.P.
TEST BORING	T.B.
JUNCTION STRUCTURE	J.S.
CATCH BASIN	C.B.
SANITARY SEWER	S.S.
TEMPORARY BENCH MARKS	T.B.M.
SOUTHERN CALIFORNIA GAS CO.	S.C.G.
L.A. DEPT. OF WATER & POWER WATER SYST. DW&PWS	
SOUTHERN CALIFORNIA WATER CO.	S.C.W.
INGLEWOOD CITY WATER DEPT.	ING.W.
SOUTHERN CALIFORNIA EDISON CO.	S.C.E.
PACIFIC TELEPHONE & TELEGRAPH CO.	P.T.&T.



VICINITY MAP  
GRAPHIC SCALE

# LOS ANGELES COUNTY FLOOD CONTROL DISTRICT

## STANDARD DRAWINGS

DRAWING NO.	TITLE
2-D88	LOCAL DEPRESSION NO. 2
2-D96	STANDARD DROP STEP
2-D107	CONCRETE RINGS, REDUCER AND PIPE
2-D193	JUNCTION STRUCTURE NO. 4
2-D156	MANHOLE FRAME AND COVER FOR CATCH BASINS
2-D160	CATCH BASIN NO. 1 (W=3'6")
2-D162	CATCH BASIN NO. 2 (W=7')
2-D163	CATCH BASIN NO. 3 (W=10'; 14'; 21'; 28'; ETC.)
2-D172	CATCH BASIN REINFORCEMENT
2-D173.1 TO .3	PIPE SUPPORTS ACROSS TRENCHES
2-D175	REMOVABLE PROTECTION BAR FOR CATCH BASINS
2-D177	PIPE BEDDING IN TRENCHES
2-D181	STANDARD NON-ROCKING MANHOLE FRAME AND COVER
2-D184	MANHOLE NO. 2 (PIPES, 36" OR LARGER)
2-D188	TRANSITION STRUCTURE NO. 3 (PIPE TO PIPE)
2-D213.1 & .2	"D" LOAD TABLE FOR DESIGN OF REINFORCED CONCRETE PIPE
2-D171	STANDARD A-305 REINFORCING BARS
2-D232	DETAIL OF CATCH BASIN OPENING
2-D250	REMODELING OF SANITARY SEWER HOUSE CONNECTIONS
2-D251	PROTECTION FOR MAIN LINE AND HOUSE CONNECTION SEWERS
2-D109	CATCH BASIN NO. 6
2-D224	CONNECTION TO CATCH BASIN FOR PIPES 12" THROUGH 72"
2-D227	FRAME AND GRATING FOR CATCH BASINS
2-D249.1 & .2	CATCH BASIN NO. 8
2-D264	ADJUSTABLE PROTECTION BAR STIRRUP
2-D393	CONCRETE COLLAR FOR PIPES 12" THROUGH 66"
2-D413	UNIFIED SOIL CLASSIFICATION SYSTEM
2-D399	CRITERIA FOR THE DESIGN OF SHORING FOR EXCAVATIONS
2-D400	SAMPLE SHEET FOR USE AS A GUIDE IN PREPARING CALCULATIONS FOR SHORING OF EXCAVATIONS
2-D113	MANHOLE NO. 4
2-D112	JUNCTION STRUCTURE NO. 2
2-D161	DETAIL OF ANGLE AND ANCHOR FOR CATCH BASINS.

# LOS ANGELES COUNTY ROAD DEPARTMENT

## STANDARD DRAWINGS

DRAWING NO.	TITLE
M57-39R	PARTIAL CONCRETE REPLACEMENT FOR CROSS GUTTERS AND SPANDRELS.
M57-45R	SPECIFICATIONS FOR REPAIRS OF CUTS IN CONCRETE PAVEMENT.

28. CONSTRUCT LOCAL DEPRESSION PER STANDARD DRAWING 2-D109 AND AS MODIFIED ON THE DRAWINGS FOR CATCH BASIN NO. 6.

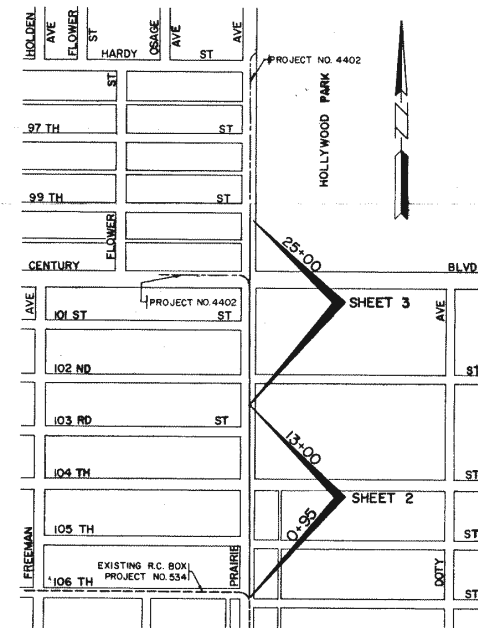
■ "AS BUILT DWGS."

# GENERAL NOTES

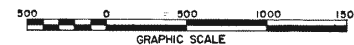
- NUMBERS IN CIRCLES INDICATE ITEMS UNDER WHICH PAYMENT WILL BE MADE.
- ELEVATIONS SHOWN ARE IN FEET ABOVE THE U.S.G.S. MEAN SEA LEVEL DATUM.
- STATIONS SHOWN ON DRAWINGS ARE ALONG CENTER LINE OF CONDUIT OR ON A LINE NORMAL TO CENTER LINE OF CONDUIT.
- STATIONS AND INVERT ELEVATIONS OF PIPE INLETS SHOWN ON THE PROFILES ARE AT THE INSIDE FACE OF THE CONDUIT, UNLESS OTHERWISE SHOWN.
- ALL FIELD BOOK REFERENCES ARE TO CITY OF INGLEWOOD FIELD BOOKS, UNLESS OTHERWISE NOTED.
- ALL PIPE IN OPEN TRENCH SHALL BE BEDDED ACCORDING TO STANDARD DRAWING 2-D177, CASE III, UNLESS OTHERWISE SHOWN OR MODIFIED IN THE SPECIFICATIONS.
- PIPE CONNECTIONS TO STORM DRAIN SHALL CONFORM TO STANDARD DRAWING 2-D193, UNLESS OTHERWISE SHOWN.
- TIES FOR CATCH BASINS AS SHOWN ON THE DRAWINGS ARE FROM CURB RETURN TO CENTER LINE OF CATCH BASIN, UNLESS OTHERWISE SHOWN.
- LOCATIONS OF CATCH BASIN CONNECTOR PIPE JUNCTIONS WITH CATCH BASINS AS SHOWN ON THE DRAWINGS ARE SCHEMATIC. IT IS INTENDED THAT SUCH JUNCTIONS BE LOCATED AT THE DOWNSTREAM ENDS OF THE CATCH BASINS, UNLESS OTHERWISE SHOWN. IN ALL CASES THE EXACT LOCATIONS WILL BE DETERMINED IN THE FIELD BY THE ENGINEER TO MEET FIELD CONDITIONS.
- MONOLITHIC CATCH BASIN CONNECTIONS SHALL BE CONSTRUCTED, WHERE APPLICABLE, PER STANDARD DRAWING 2-D224.
- "V" IS THE DEPTH OF INLET OF CATCH BASINS IN SERIES MEASURED FROM TOP OF CURB TO INVERT OF CONNECTOR PIPE.
- ALL EXISTING SANITARY SEWERS SHOWN ON THE DRAWINGS ARE CITY OF INGLEWOOD SEWERS.
- EXISTING UTILITIES SHALL BE MAINTAINED IN PLACE BY THE CONTRACTOR, UNLESS OTHERWISE NOTED.
- WHERE UTILITIES ARE INDICATED ON THE DRAWINGS TO BE SUPPORTED, SAID SUPPORTS SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D173.1, .2 OR .3, UNLESS OTHERWISE INDICATED.
- LOCATIONS SHOWN ON THE PLANS FOR EXISTING SANITARY SEWER HOUSE CONNECTIONS ARE APPROXIMATE ONLY.
- SANITARY SEWER HOUSE CONNECTION RECONSTRUCTION AND RECONNECTION SHALL BE IN ACCORDANCE WITH STANDARD DRAWING 2-D250, UNLESS OTHERWISE SHOWN.
- SANITARY SEWERS AND HOUSE CONNECTIONS CROSSING OVER THE STORM DRAIN TRENCH SHALL BE SUPPORTED IN ACCORDANCE WITH STANDARD DRAWINGS 2-D173.1 TO .3 AND ENCASED PER GENERAL NOTE 1 ON STANDARD DRAWING 2-D173.1.
- WHEN INDICATED ON THE DRAWINGS, SANITARY SEWERS AND HOUSE CONNECTIONS SHALL BE ENCASED OR BLANKETED IN ACCORDANCE WITH STANDARD DRAWING 2-D251.
- ALL RESURFACING, CURBS, GUTTERS, SIDEWALKS, DRIVEWAYS AND OTHER EXISTING IMPROVEMENTS TO BE RECONSTRUCTED SHALL BE CONSTRUCTED AT THE SAME ELEVATION AND LOCATION AS THE EXISTING IMPROVEMENTS, UNLESS OTHERWISE NOTED.
- SOIL TEST BORINGS FOR THIS PROJECT WERE MADE 8-26-65.
- UTILITIES DESIGNATED BY THE SYMBOL \* WILL BE ABANDONED IN PLACE AND THE OWNER WILL INSTALL A NEW SECTION OF THE AFFECTED UTILITY AT A LOCATION IN CLOSE PROXIMITY TO, BUT WHICH DOES NOT PHYSICALLY INTERFERE WITH, THE PROPOSED STORM DRAIN CONDUIT AND APPURTENANT STRUCTURES.
- THE DEPTH AT THE UPSTREAM END OF CATCH BASINS 10 FEET OR MORE IN LENGTH SHALL BE CURB FACE PLUS 12 INCHES UNLESS OTHERWISE SHOWN.
- REFER TO SHEET 4 FOR TYPICAL CATCH BASIN CONNECTOR PIPE PROFILE.
- ALL OPENINGS RESULTING FROM THE CUTTING OR PARTIAL REMOVAL OF EXISTING PIPES, CULVERTS, OR SIMILAR STRUCTURES SHALL BE SEALED WITH 8 INCHES OF BRICK AND MORTAR OR 6 INCHES OF CONCRETE.
- THE OPENINGS AND TOP SLABS OF ALL SIDE INLET CATCH BASINS AND CATCH BASIN NO. 6 SHALL BE MODIFIED TO MEET THE REQUIREMENTS ON STANDARD DRAWING 2-D232 EXCEPT AS NOTED.
- WHERE REQUIRED BY STANDARD DRAWING 2-D213.1, CONCRETE BACKFILL SHALL BE USED AROUND CONNECTOR PIPES 36 INCHES OR LESS IN DIAMETER. CONCRETE BACKFILL FOR MAIN LINE PIPE SHALL BE USED ONLY WHEN DIRECTED BY THE ENGINEER.
- THE OPENING OF ALL SIDE INLET CATCH BASINS AND CATCH BASIN NO. 6 THAT HAVE MODIFIED LOCAL DEPRESSIONS TO BE CURB FACE PLUS 1" IN LIEU OF 9".

# INDEX TO DRAWINGS

SHEET NO.	TITLE
1.	LOCATION MAP, GENERAL NOTES, INDEX TO DRAWINGS, STANDARD DRAWINGS, ABBREVIATIONS AND LEGEND.
2.	PLAN, PROFILE AND SECTION STA 0+95 TO STA 13+00
3.	PLAN, PROFILE AND SECTION STA 13+00 TO STA 25+00
4.	LOG OF BORINGS & RESURFACING PLAN



LOCATION MAP

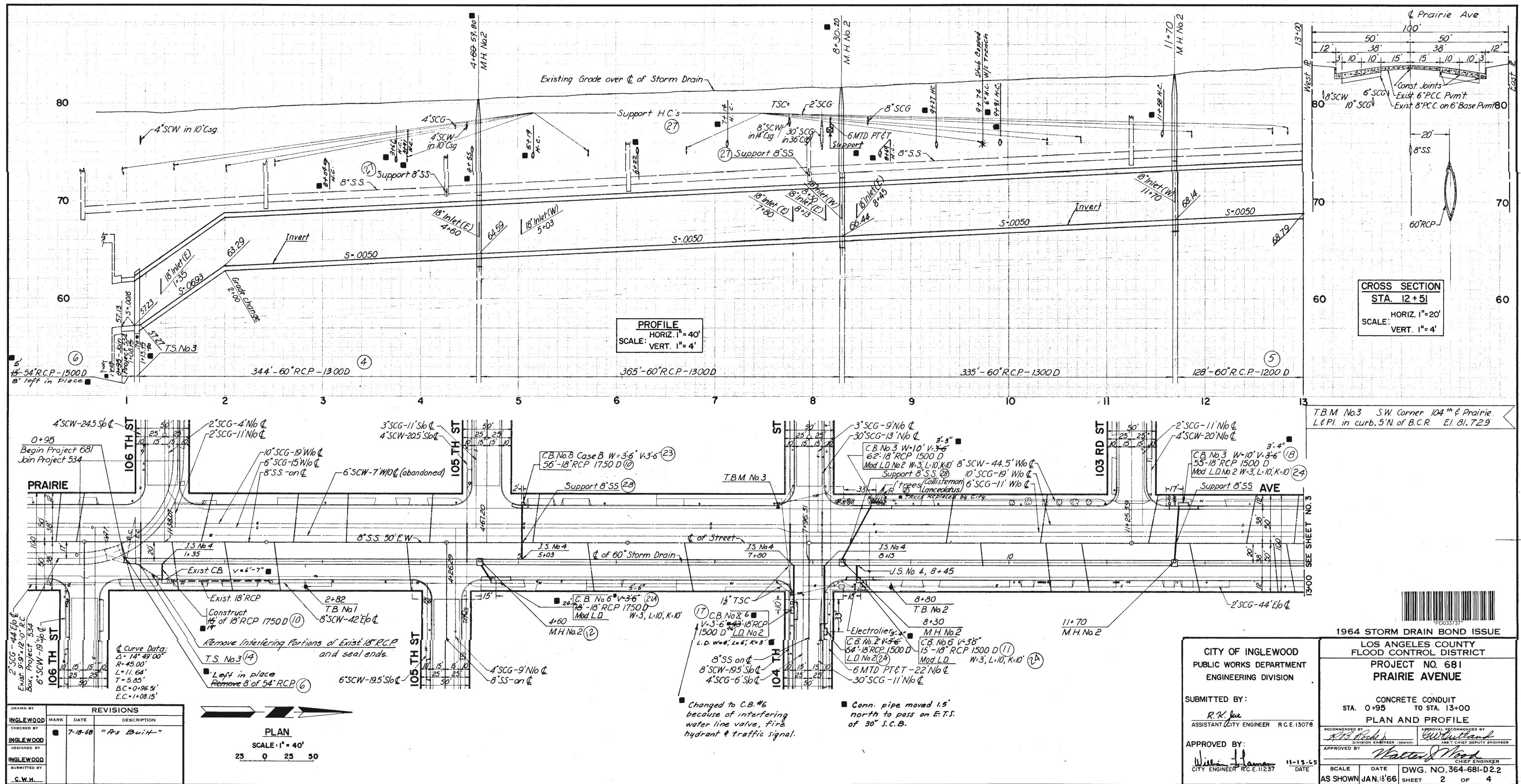


NOTE CHANGE OF PROJECT LIMITS  
Due to bond issue financing requirements, the upstream limit of Project 681, has been changed to Station 14+98. See DWG. NO. 364-681-D2.3. The downstream limit of Project 4402 Unit I, Line C, has been extended to meet the new upstream limit of Project 681, see DWG. NO. 364-4402-D2.2.

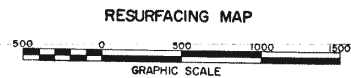
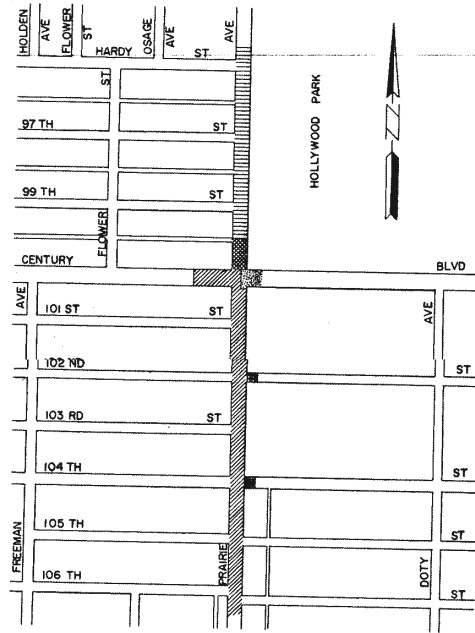
1964 STORM DRAIN BOND ISSUE

<p>CITY OF INGLEWOOD PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION</p>		<p>LOS ANGELES COUNTY FLOOD CONTROL DISTRICT PROJECT NO. 681 PRAIRIE AVENUE</p>	
<p>SUBMITTED BY: R.R. [Signature] ASSISTANT CITY ENGINEER R.C.E. 13078</p>		<p>RECOMMENDED BY: R.R. [Signature] DIVISION ENGINEER (DESIGN)</p>	
<p>APPROVED BY: Walter [Signature] CITY ENGINEER R.C.E. 11237</p>		<p>APPROVAL RECOMMENDED BY: [Signature] ASST. CHIEF DEPUTY ENGINEER</p>	
SCALE	DATE	DWG. NO.	SHEET
AS SHOWN	JAN. 1966	NO. 364-681-D2.1	1 OF 4

"AS BUILT" DRAWING

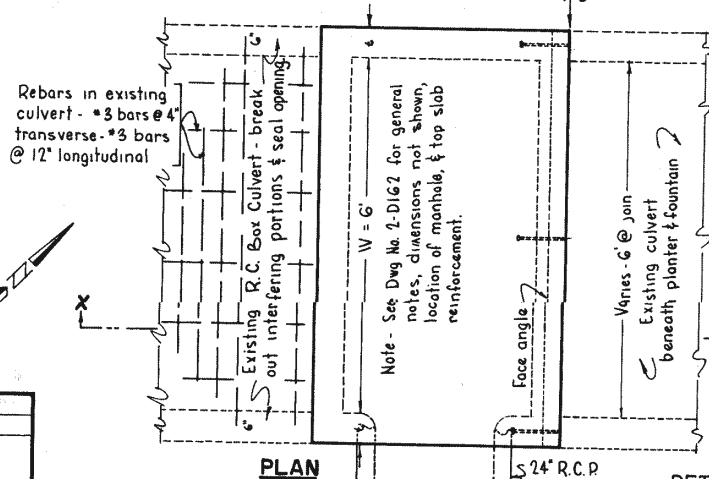






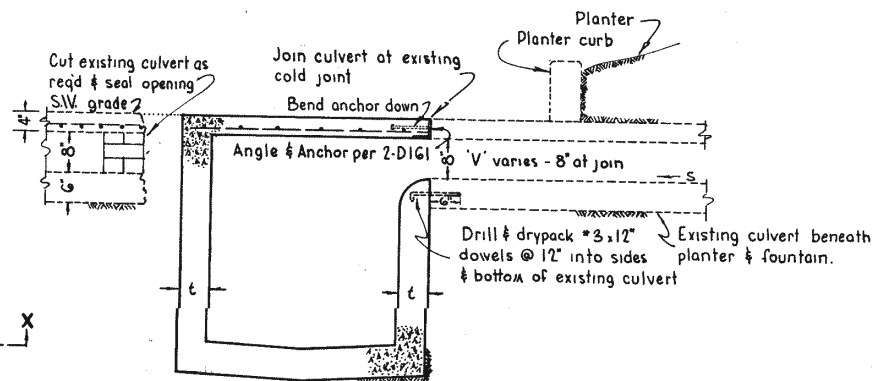
EXISTING SURFACE	PROPOSED RESURFACING
8" P.C.C. PAVEMENT ON 6" SELECTED BASE MATERIAL	8" P.C.C. PAVEMENT ON 6" SELECTED BASE MATERIAL
2 1/2" A.C. SURFACE ON 6" PORTLAND CEMENT CONC.	2 1/2" A.C. SURFACE ON 6" PORTLAND CEMENT CONC.
3" A.C. SURFACE ON 12" SELECTED BASE MATERIAL	4" A.C. SURFACE ON 12" SELECTED BASE MATERIAL
6" PORTLAND CEMENT CONCRETE	6" PORTLAND CEMENT CONCRETE

Rebars in existing culvert - 3 bars @ 4' transverse - 3 bars @ 12' longitudinal

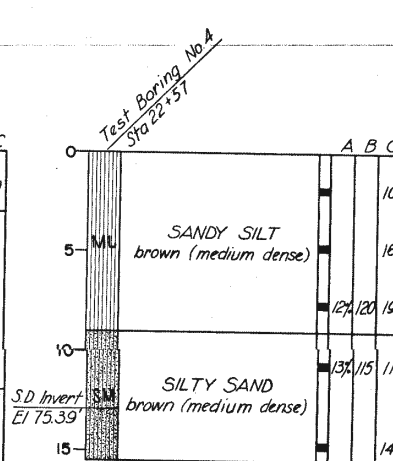
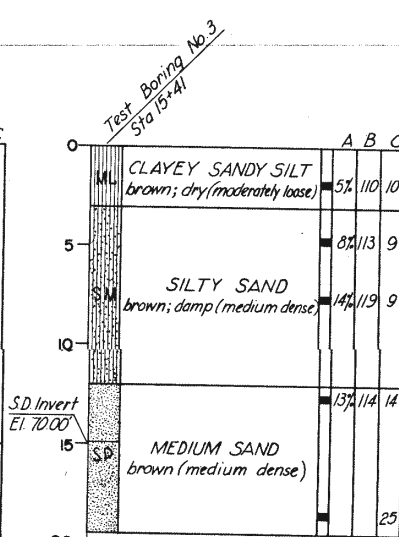
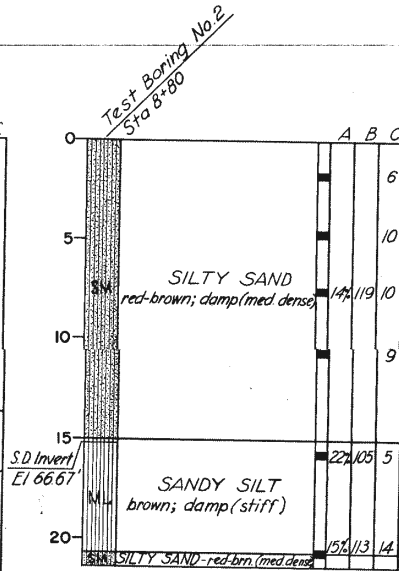
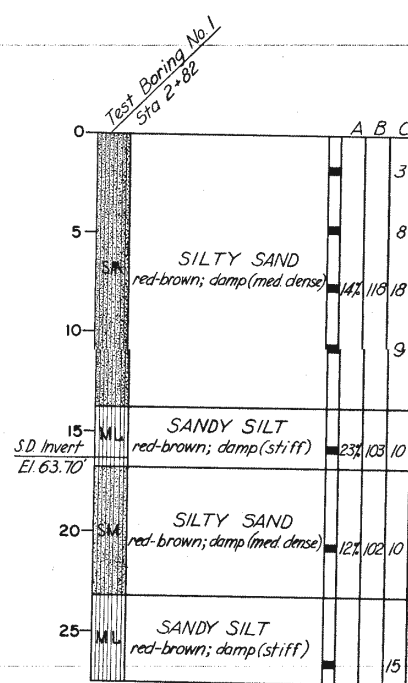


PLAN

DETAIL OF CATCH BASIN NO. 2 (MODIFIED) AT STA. 21+78(EAST) Scale 3/4"=1'



SECTION X-X

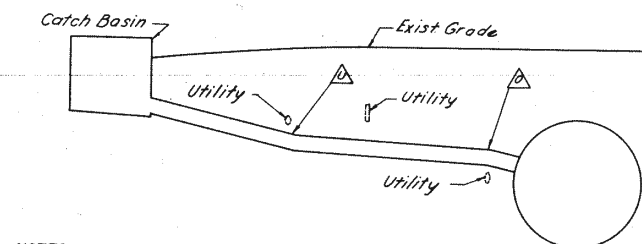


# LEGEND AND NOTES:

SCALE: (VERTICAL) 1"=4'

- A MOISTURE CONTENT IN PERCENTAGE
- B DRY DENSITY IN LBS PER CUBIC FOOT
- C STANDARD PENETRATION; NO. OF BLOWS PER FOOT
- DEPTH AT WHICH UNDISTURBED SAMPLE WAS TAKEN
- ALL BORINGS WERE COMPLETED 8-26-65.
- NO GROUND WATER OR CAVING WAS ENCOUNTERED IN ANY BORING.
- INVERT OF STORM DRAIN SHOWN ON THIS SHEET SUPERSEDES THAT SHOWN IN THE SOIL REPORT.
- THE SOIL CLASSIFICATIONS SHOWN ARE IN ACCORDANCE WITH THE UNIFIED SOIL CLASSIFICATION SYSTEM.

TYPICAL CONNECTOR PIPE PROFILE NO SCALE



# NOTES:

- The change in grade of the connector pipe may occur either over or under an existing utility. The particular utility at which the change occurs is noted on the project drawings. At locations where utility crossings are marked with a triangle, the connector pipe grade will break over the utility. At locations where utility crossings are marked with a circle, the connector pipe grade will break under the utility.
- On those connector pipes where change in grade is not indicated, it is assumed that the connector pipe can be laid on a straight grade from the catch basin to the storm drain without interference with utilities.
- Where connector pipe has a change of grade exceeding .10'/ft or differs in diameter from that of existing pipe, use concrete collar per std 2-D393.
- The contractor shall make exploratory excavations to determine the exact location and depth of utilities, which are marked 'A' or 'B'. After the exact location of a utility has been determined, the grade and alignment of the connector pipe will be staked so as to clear the utility.



1964 STORM DRAIN BOND ISSUE

CITY OF INGLEWOOD  
PUBLIC WORKS DEPARTMENT  
ENGINEERING DIVISION

SUBMITTED BY:

R. K. Lee  
ASSISTANT CITY ENGINEER R.C.E. 13078

APPROVED BY:

W. J. H. H. H.  
CITY ENGINEER R.C.E. 11237

LOS ANGELES COUNTY  
FLOOD CONTROL DISTRICT  
PROJECT NO. 681  
PRAIRIE AVENUE

LOG OF BORINGS, RESURFACING PLAN AND  
MISCELLANEOUS DETAILS

RECOMMENDED BY: [Signature]  
DIVISION ENGINEER (DESIGN)

APPROVED BY: [Signature]  
CHIEF ENGINEER

SCALE: DATE: DWG. NO. 364-681-D2.4  
AS SHOWN JAN. 12 '66 SHEET 4 OF 4

"AS BUILT" DRAWING