

**PRELIMINARY**  
**HYDROLOGY REPORT**  
**FOR**  
**SANDPIPER VILLA**  
**Oceanside, CA**

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1. Vicinity Map

### Exhibits

- Exhibit A – Existing-Condition Hydrology Map
- Exhibit B – Proposed-Condition Hydrology Map

## SECTION 1.0

### PROJECT DESCRIPTION

#### **1.1 Site Description**

The site is comprised of 2.01 acres of arable land, and contains remnants of an existing single-family residence, and outbuildings. There are multiple concrete slabs along the easterly portion of the site, and a paved driveway off Dixie Street to the concrete slab area. The topography gently slopes from the northeast to the southwest with approximately 9 feet of relief across the site. Elevations range from 160 Mean Sea Level (MSL) in the northeastern corner of the site; to 151 MSL at the southwest parcel boundary. The site is moderately vegetated with a mix of mature trees; low growing shrubs and grasses.

#### **1.2 Existing Condition Drainage**

The site is a tributary to the Loma Alta Creek, Loma Alta Slough, and the Pacific Ocean Shoreline at the Loma Alta Slough.

The site drainage patterns are characterized as sheet flow and tend from northeast to southwest. The flows concentrate at the existing curb located at northwest parcel boundary. The flows form a confluence with offsite runoff and travel by street/gutter flow to an existing curb inlet located north of the site on Dixie Street.

The drainage basin and runoff patterns are delineated on the “Pre-Development Condition Drainage Exhibit” and the results of the Rational Method Hydrology calculations are located in Section 3.0 – Summary and Conclusion.

#### **1.3 Proposed Project Improvements**

The proposed SANDPIPER VILLA development will consist of site development and construction of (4) Multi-Unit Residential Buildings for Senior Assisted Living Care. The onsite surface improvements are private, and include curb and gutter, solid unit paver drive aisle, and guest parking areas, concrete pedestrian walkways, private storm drainage systems to serve the Stormwater Treatment Control BMPs, and underground Detention/HMP facilities. Public underground utilities will include, sanitary sewer, storm drain systems, water mains and dry utilities. There is a single entry/exit driveway to the project from Dixie Street, and an offsite employee parking facility located at the NE corner of the adjacent Friendly Church of God in Christ Oceanside. The surface improvement to the offsite parking will include asphalt paving, concrete valley gutter, pedestrian sidewalk, and private storm drain catch basin and pipe system that also connects to the onsite Detention/HMP facilities.

## **1.4 Proposed Condition Drainage**

The surface runoff from the offsite employee parking area will sheet flow to a PCC Valley Gutter that will carry the runoff to a curb opening catch basin at the SE corner of the Employee Parking lot. The flow will discharge to, and be carried by a private storm drain system that confluence with onsite storm water runoff from the onsite drainage basin areas. The offsite, and onsite flows discharge to (4) individual storm water treatment control BMPs facilities, manufactured by BioClean Environmental Services, Inc. The treatment facilities operate as a Modular Wetlands System and utilizes horizontal flow-through-filtration as it replicates the natural processes to remove a variety of pollutants from stormwater runoff. including fine TSS, bacteria, oils and grease, heavy metals and harmful nutrients like nitrate and phosphorus. While most systems utilize a single treatment method, the MWS incorporates screening, hydrodynamic separation, sorptive media filtration into a single completely modular system. The treated runoff is then piped to a downstream Hydromodification Management Practice Facility (HMP).

The HMP facility will consist of a 42" HDPE underground detention/storage pipe with a controlled outlet structure at the downstream end of the pipe. The outlet of the HMP structure has a double chamber with a built-in weir. The weir has multiple low flow orifice openings that release the runoff at a rate equal to or less than the existing (0.1) (Q2) and (Q10). The Peak unmitigated Q100 runoff will be attenuated to the existing condition runoff rate with added detention storage provide by the HMP storage pipe. An overflow weir will be sized to allow only a release rate of 3.38 cfs, equal to the existing project Q100 peak flow rate. The detention design, details, exhibits, volume and orifice sizing calculations are provided in the "Technical Memorandum: Determination for Pre- and Post- Developed 100-year Peak Flow" for Sandpiper Villa, prepared by: "Tory R.Walker Engineering", Revision dated: September 13, 2019, and is included in Section 4, Appendix A8 of this hydrology report.

The HMP outlet structure connects to a proposed 18" RCP storm drain system in Dixie Street, and carries the runoff westerly to an existing 36" RCP. The existing 36" RCP crosses Dixie Street, and connects to an existing catch basin box on the south side of the Street.

This Preliminary Hydrology Report has been prepared using methods described in the San Diego County Hydrology Manual (2003 edition). Supporting charts are included in the appendix of the report. A node-to-node computer analysis is used for the rational method calculations. Ultimate development runoff coefficients are used throughout the study.

The following reference documents were used in the preparation of this study:

- City of Oceanside ("Engineering Design and Processing Manual"), latest edition.
- Hydrology Manual, County of San Diego, 2003 ("County Design Manual").

## SECTION 2.0

### HYDROLOGY CALCULATIONS

The hydrological analysis utilized to calculate the storm runoff for the 100-year storm event was the Rational Method ( $Q = C * I * A$ ). Using a computer program based on the San Diego County Flood Control Division 2003, 1981 Hydrology Manual © copyright 1982-2003 Advanced Engineering Software (AES) ver. 1.5A, release date: 1/1/03, determines each component of the Rational Method equation, in which:

Q = Runoff (cfs),

C = Runoff coefficient,

I<sub>A</sub> = Rainfall intensity (inches/hour),

A = Area (acres),

T<sub>C</sub> = Time of Concentration (initial, overland, street gutter, or pipe).

#### **2.1 Determination of Runoff Coefficient**

The runoff coefficient (C) is based on the soil group of the drainage basin. This project lies in Soil Group D, as determined by referencing the soil survey maps.

Runoff coefficients are also dependent on the proposed land use density of each basin. Coefficients for this project were based from the County of San Diego Hydrology Manual, 2003 edition. The runoff coefficient used in the calculation for the onsite developed areas is based on a Residential Density of 10.9 DU/A or less. (See Appendix A-2).

#### **2.2 Determination of Intensity**

Rainfall intensity (I) is a function of the six-hour precipitation measure and the time of concentration for the drainage basin, as defined by the County of San Diego Hydrology Manual (Appendix A-3, A-4, A-5).

### **2.3     Determination of Areas**

The area (A) of each drainage basin was determined from the Drainage Area Map. The onsite drainage basins have been based on the ultimate anticipated land use. See the Hydrology Map Exhibit 'B' for the Onsite Drainage Basins.

### **2.4     Determination of Initial Time of Concentration**

The initial  $T_c$  is the overland time required for runoff to travel from the farthest edge of a drainage basin to the street gutter and or storm drain collection system. The  $T_c$  is determined using the 2003 County of San Diego Hydrology Manual.

### **2.5     Flood Routing Method**

The Modified Rational Method was utilized to calculate peak storm water flows and route the calculated flows through the proposed drainage system.

When two flows confluence at a junction point, the smaller of the flows has been decreased by using the Modified Rational Method. This procedure accounts for the differing times of concentration for the flows upstream of the confluence point. The smaller Q is reduced by either the ratio of the intensities or the ratio of the times of concentration.

### **2.6     Hydrology Calculations**

The Rational Method Hydrology calculations for the current project Pre, and Post 2, 10 and 100-year conditions, are contained in Appendix A-6 and A-7. Each sub-basin is identified with its corresponding area, time of concentration and total flow.

## SECTION 3.0

### SUMMARY/CONCLUSIONS

#### Summary of existing/proposed basin comparisons:

The following tables present the Pre and un-mitigated Post development runoff, for the entire project tributary watershed. The discharge rates are shown for comparison purposes:

TABLE 3.1

Pre-Development Rational Method Hydrology Calculations – Entire Watershed – Node A1-A16						
Storm Frequency	$P_6$ (adjusted)	$C_{Avg}$	$I$ (in/hr)	AREA (ac.)	$T_c$	Peak Flowrate $Q$ (cfs)
2-Year	1.20	0.46	1.81	2.01	11.87	1.57
10-Year	1.70	0.46	2.66	2.01	11.25	2.31
100-Year	2.70	0.46	4.35	2.01	10.70	3.78

TABLE 3.2

Post-Development Rational Method Hydrology Calculations – Entire Watershed – Node A1-A26						
Storm Frequency	$P_6$ (adjusted )	$C_{Avg}$	$I$ (in/hr)	AREA (ac. )	$T_c$	Peak Flowrate $Q$ (cfs)
2-Year	1.20	0.76	2.63	2.01	6.63	4.05
10-Year	1.70	0.76	3.76	2.01	6.56	5.69
100-Year	2.70	0.76	6.17	2.01	6.24	9.28

Net increased Q100 runoff of 5.50 cfs.

#### Conclusion:

Tables 3.1 through 3.2 illustrate that the un-mitigated post-condition  $Q_{100}$  is increased when compared to the pre-development condition  $Q_{100}$ . This project is a Priority Development Project, as determined by the (HMP) Applicability Matrix within the approved SWMP. Hydro-modification Management Plan Requirements per the Regional Water Quality Control Board is required to mitigate the post condition  $Q_2$ -  $Q_{10}$  flows to no greater than 10% of the existing storm events. The design, details, exhibits, and calculations are shown in the “Technical Memorandum: SWMM Modeling for Hydromodification Compliance of: Sandpiper Villa” prepared by: “Tory R. Walker Engineering per Revision dated: September 13, 2019, and is included within the approved SWMP Section 27, Attachments.

In addition the City of Oceanside Engineering Department has determined the existing downstream drainage facilities are currently at maximum capacity, and are conditioning this project to provide onsite detention to limit the post runoff rate, equal to the existing condition flow rate. The onsite HMP facility will be designed to provide additional storage volume to attenuate the Q100 release rate to a Peak Q100 development runoff rate of 3.38 cfs (0.40 cfs less than pre-development runoff rate of 3.78 cfs). The detention design, details, exhibits, volume and calculations are provided in the “Technical Memorandum: Determination for Pre- and Post- Developed 100-year Peak Flow” for Sandpiper Villa, prepared by: “Tory R. Walker Engineering”, Revision dated: September 13, 2019 in Section 4, Appendix A8 of this hydrology report.



**SECTION 4.0**  
**LIST OF APPENDICES**

Appendix

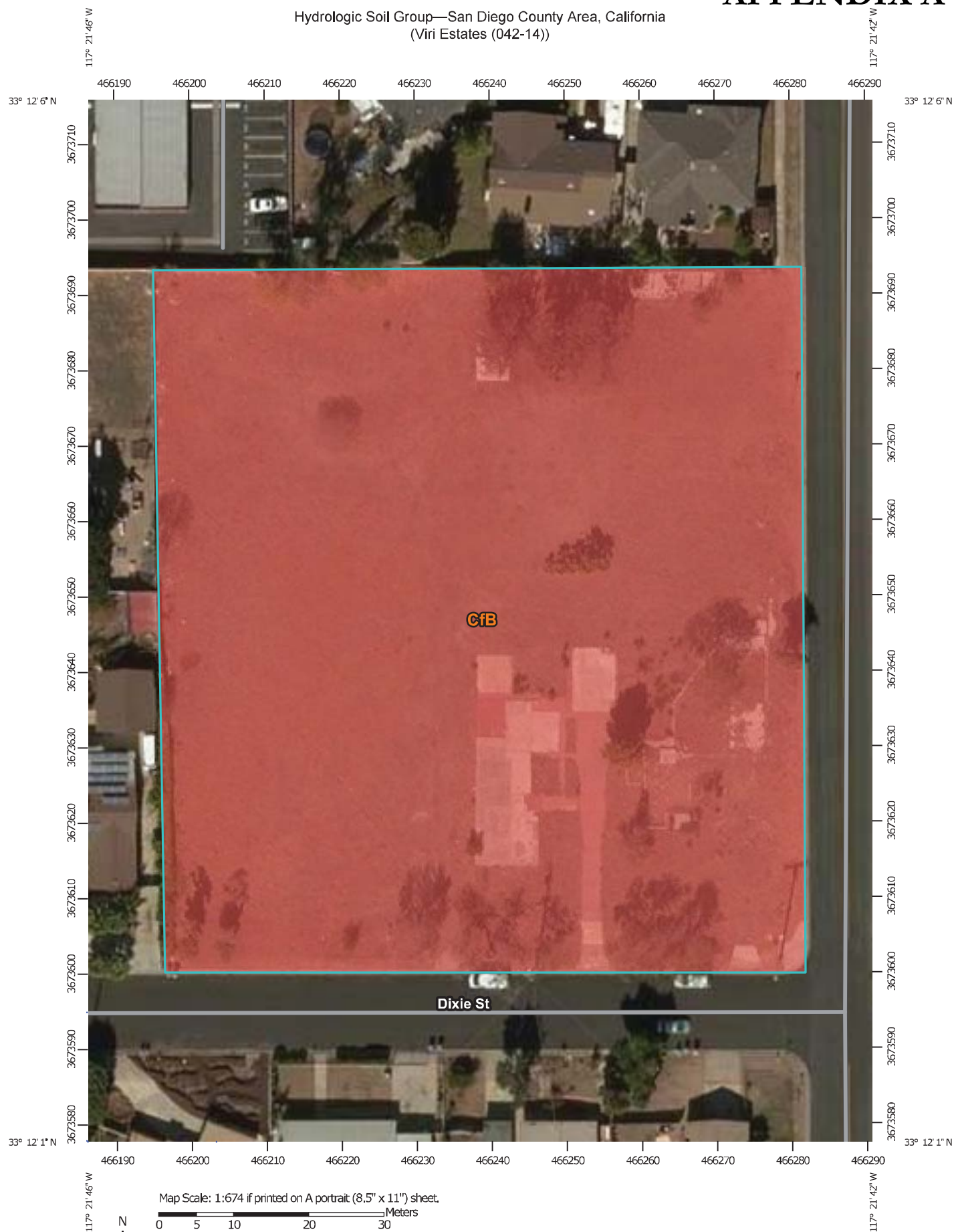
A. HYDROLOGY

- A-1 Hydrologic Soil Groups Map – San Diego County Soils Interpretation Study
- A-2 Runoff Coefficients for Urban Areas
- A-3 Intensity-Duration Design Chart (2-year)  
2-Year, 6-Hour Precipitation Isopluvials  
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- A-4 Intensity-Duration Design Chart (10-year)  
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- A-6 Hydrology Calculations – Existing Onsite Conditions – 2, 10 & 100 Year
- A-7 Hydrology Calculations – Proposed Onsite Conditions – 2, 10 & 100 Year
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Engineering”, Revision dated: September 13, 2019.

**A-1**

**HYDROLOGIC SOIL GROUP MAP**

## Hydrologic Soil Group—San Diego County Area, California (Viri Estates (042-14))



MAP LEGEND

**Area of Interest (AOI)**

Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**

A  
A/D  
B  
B/D  
C  
C/D  
D  
Not rated or not available

**Soil Rating Lines**

A  
A/D  
B  
B/D  
C  
C/D  
D  
Not rated or not available

**Soil Rating Points**

A  
A/D  
B  
B/D

**Water Features**

Streams and Canals

**Transportation**

Rails  
Interstate Highways  
US Routes  
Major Roads  
Local Roads

**Background**

Aerial Photography

C  
C/D  
D  
Not rated or not available

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Diego County Area, California  
Survey Area Data: Version 8, Sep 17, 2014

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Nov 3, 2014—Nov 22, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — San Diego County Area, California (CA638)				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
CfB	Chesterton fine sandy loam, 2 to 5 percent slopes	D	2.0	100.0%
<b>Totals for Area of Interest</b>			<b>2.0</b>	<b>100.0%</b>

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

**A-2**

**RUNOFF COEFFICIENTS FOR  
URBAN AREAS**

**Table 3-1  
RUNOFF COEFFICIENTS FOR URBAN AREAS**

Land Use		Runoff Coefficient "C"				
NRCS Elements	County Elements	% IMPER.	Soil Type			
			A	B	C	D
Undisturbed Natural Terrain (Natural)	Permanent Open Space	0*	0.20	0.25	0.30	0.35
Low Density Residential (LDR)	Residential, 1.0 DU/A or less	10	0.27	0.32	0.36	0.41
Low Density Residential (LDR)	Residential, 2.0 DU/A or less	20	0.34	0.38	0.42	0.46
Low Density Residential (LDR)	Residential, 2.9 DU/A or less	25	0.38	0.41	0.45	0.49
Medium Density Residential (MDR)	Residential, 4.3 DU/A or less	30	0.41	0.45	0.48	0.52
Medium Density Residential (MDR)	Residential, 7.3 DU/A or less	40	0.48	0.51	0.54	0.57
Medium Density Residential (MDR)	Residential, 10.9 DU/A or less	45	0.52	0.54	0.57	0.60
Medium Density Residential (MDR)	Residential, 14.5 DU/A or less	50	0.55	0.58	0.60	0.63
High Density Residential (HDR)	Residential, 24.0 DU/A or less	65	0.66	0.67	0.69	0.71
High Density Residential (HDR)	Residential, 43.0 DU/A or less	80	0.76	0.77	0.78	0.79
Commercial/Industrial (N. Com)	Neighborhood Commercial	80	0.76	0.77	0.78	0.79
Commercial/Industrial (G. Com)	General Commercial	85	0.80	0.80	0.81	0.82
Commercial/Industrial (O.P. Com)	Office Professional/Commercial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (Limited I.)	Limited Industrial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (General I.)	General Industrial	95	0.87	0.87	0.87	0.87

\*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, Cp, for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

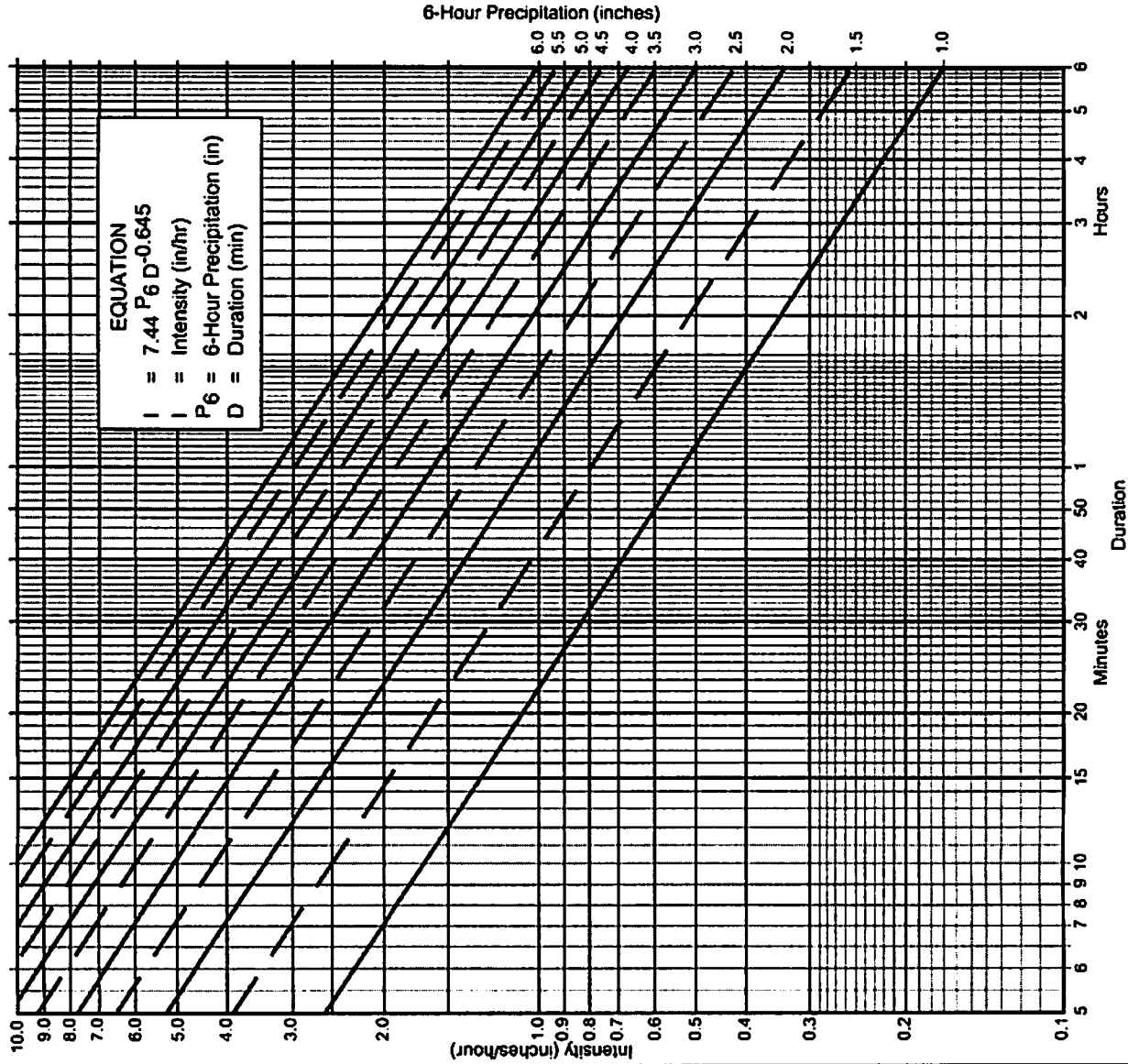
DU/A = dwelling units per acre

NRCS = National Resources Conservation Service

**A-3**

**INTENSITY - DURATION DESIGN CHARTS  
(2-YEAR)**





#### Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

#### Application Form:

- (a) Selected frequency \_\_\_\_\_ year
- (b)  $P_6 =$  \_\_\_\_\_ in.,  $P_{24} =$  \_\_\_\_\_,  $\frac{P_6}{P_{24}} =$  \_\_\_\_\_ %<sup>(2)</sup>
- (c) Adjusted  $P_6^{(2)} =$  \_\_\_\_\_ in.
- (d)  $t_x =$  \_\_\_\_\_ min.
- (e)  $I =$  \_\_\_\_\_ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

$P_6$	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
Duration	1	1	1	1	1	1	1	1	1	1	1
5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49	15.81
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.60	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.29	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.39	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

Intensity-Duration Design Chart - Template

FIGURE

3-1

# County of San Diego Hydrology Manual



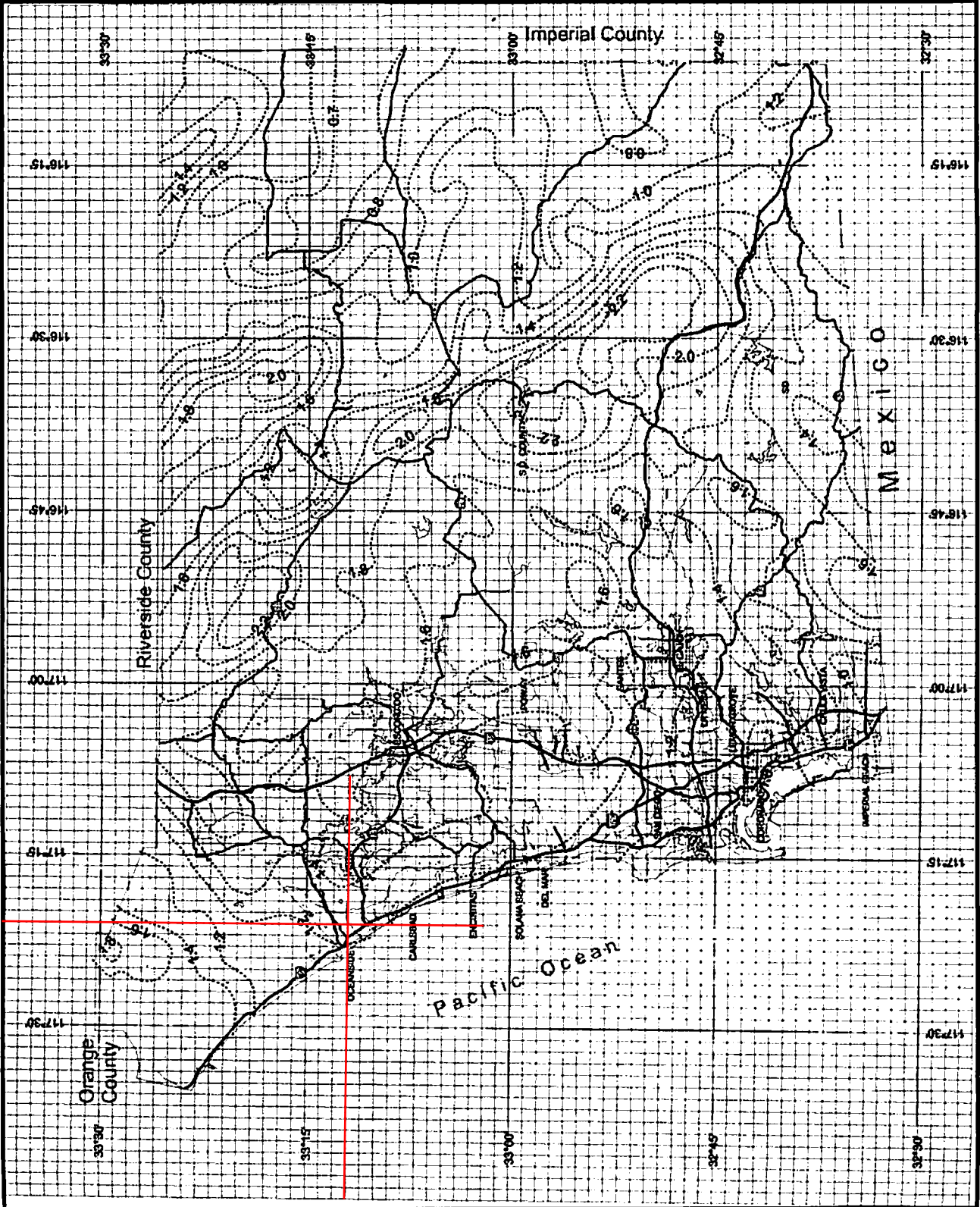
## Rainfall Isoplethals

2 Year Rainfall Event - 6 Hours

.....  
Isopleth (inches)



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# County of San Diego Hydrology Manual



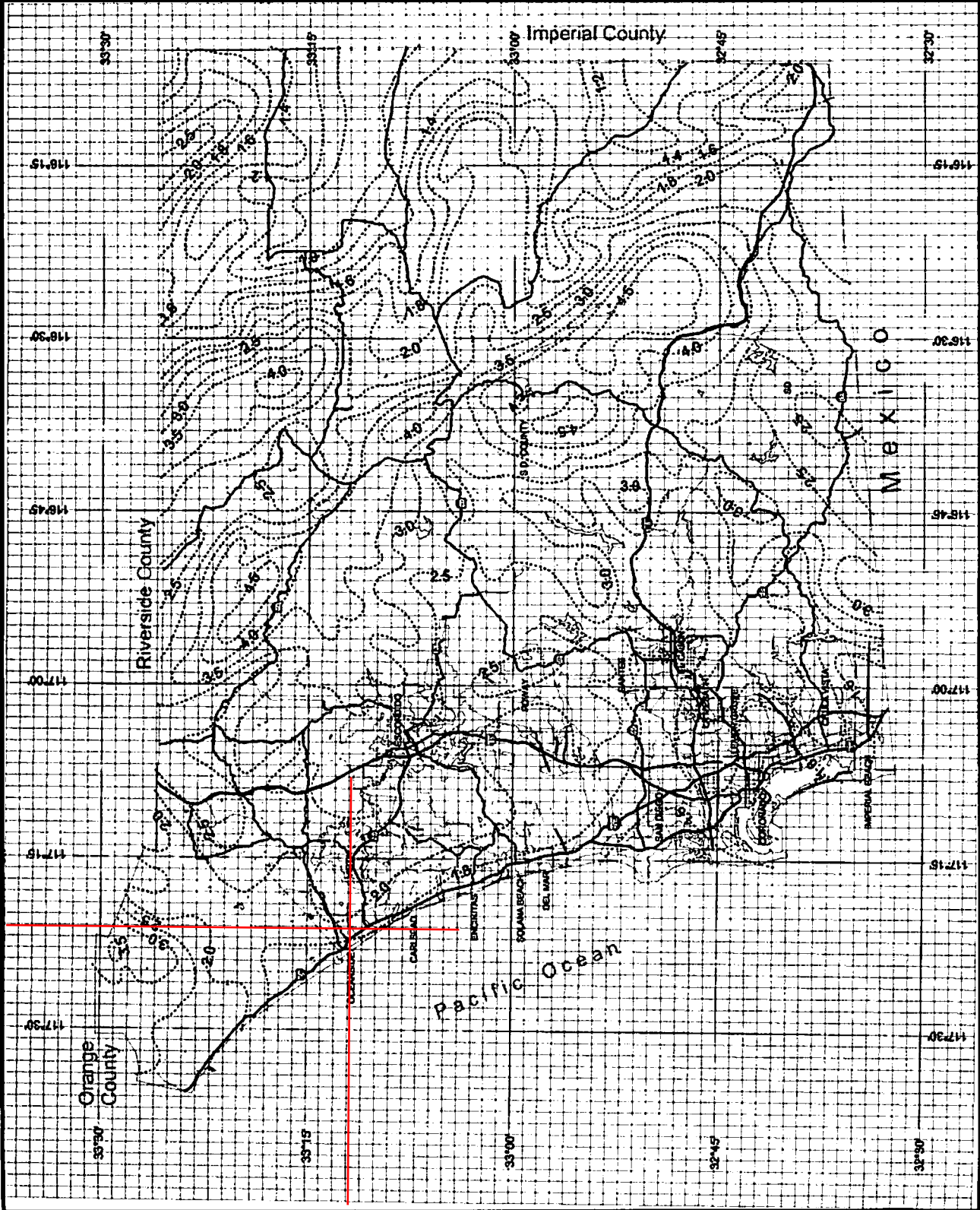
## Rainfall Isoplethals

2 Year Rainfall Event - 24 Hours

Isoplethal (inches)



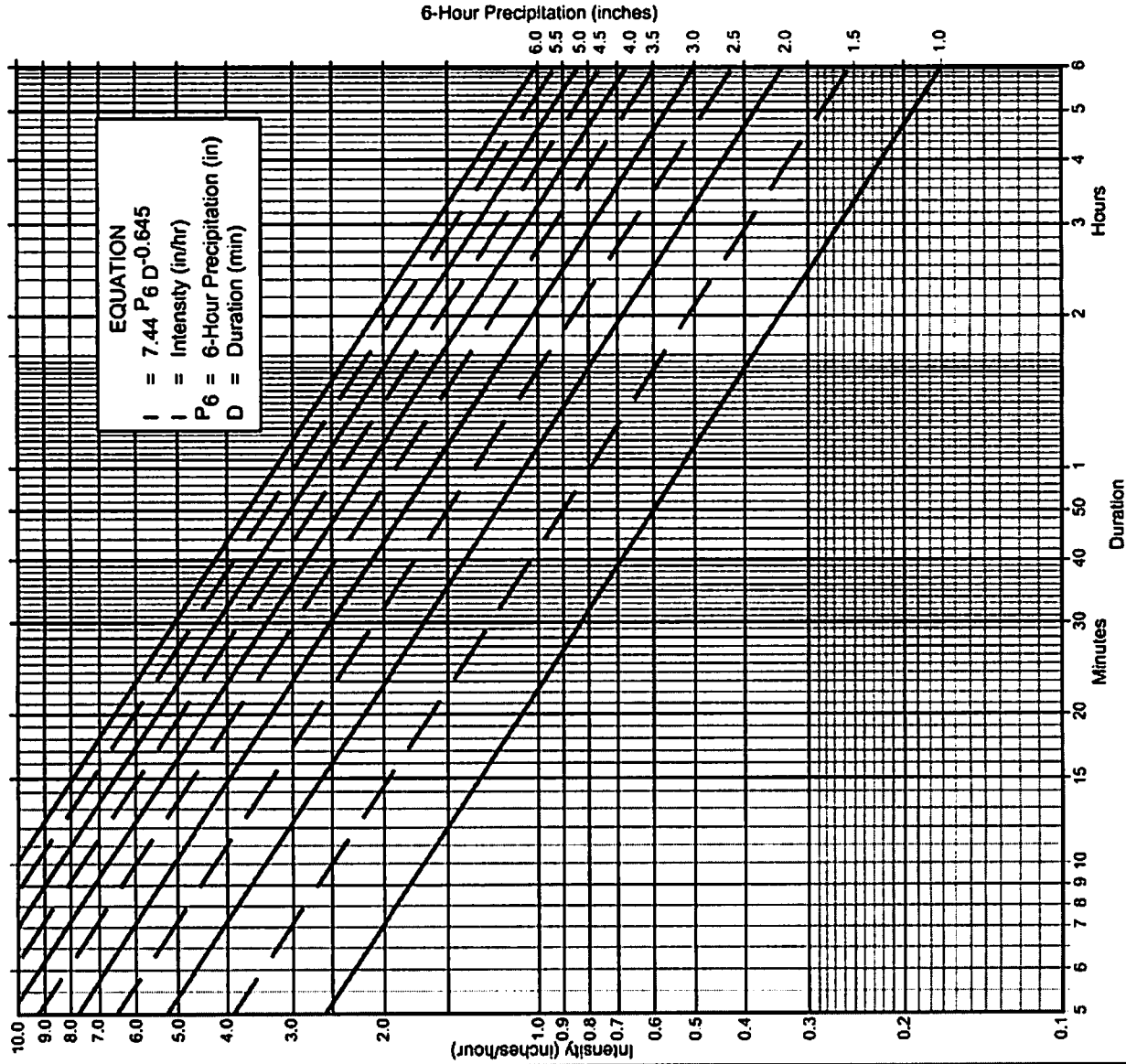
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**A-4**

**INTENSITY - DURATION DESIGN CHARTS  
(10-YEAR)**





### Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
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- (b)  $P_6 =$  \_\_\_\_\_ in.,  $P_{24} =$  \_\_\_\_\_,  $\frac{P_6}{P_{24}} =$  \_\_\_\_\_ %<sup>(2)</sup>
- (c) Adjusted  $P_6^{(2)} =$  \_\_\_\_\_ in.
- (d)  $t_x =$  \_\_\_\_\_ min.
- (e)  $I =$  \_\_\_\_\_ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

P6	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
Duration	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49	15.81
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.60	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.28	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.38	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

Intensity-Duration Design Chart - Template

# County of San Diego Hydrology Manual



## Rainfall Isoplethials

10 Year Rainfall Event - 6 Hours

Isoplethial (Inches)

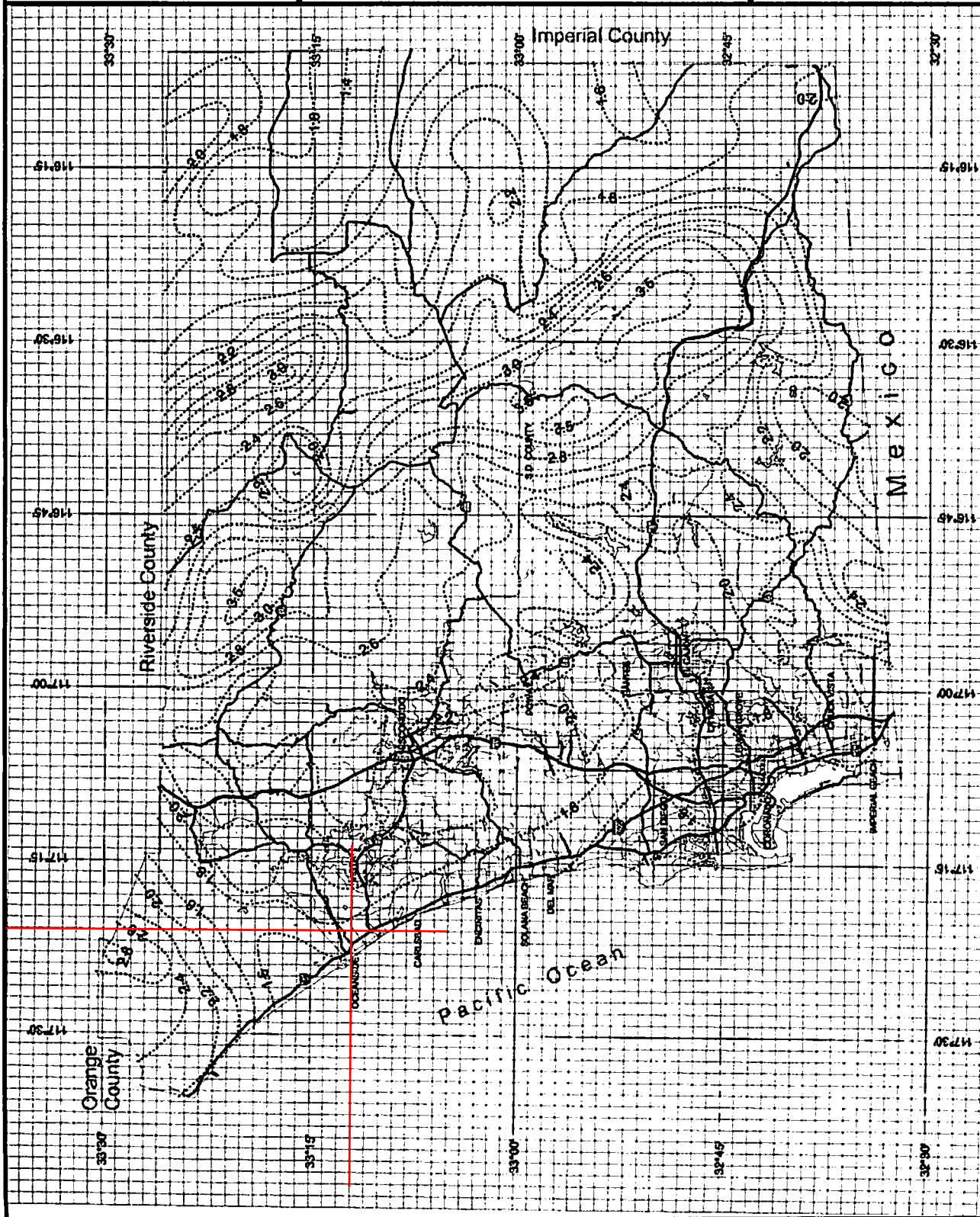
DPW  
GIS  
Department of Public Works  
Division of Public Works

SanGIS  
W. H. H. San Diego County

This map is provided without warranty of any kind. OTHER USERS OF THIS MAP ARE RESPONSIBLE FOR THE ACCURACY OF THE DATA. THE DATA IS PROVIDED AS IS. THE DATA IS NOT TO BE USED FOR ANY PURPOSE OTHER THAN THAT FOR WHICH IT WAS PROVIDED. The County of San Diego is not responsible for any errors or omissions in this map. The County of San Diego is not responsible for any damages or losses resulting from the use of this map. The County of San Diego is not responsible for any claims or liabilities resulting from the use of this map.



3 0 3 Miles



## 10 Year Rainfall Event - 24 Hours

**DPW  
GIS**  
Department of Public Works  
Geographic Information Systems

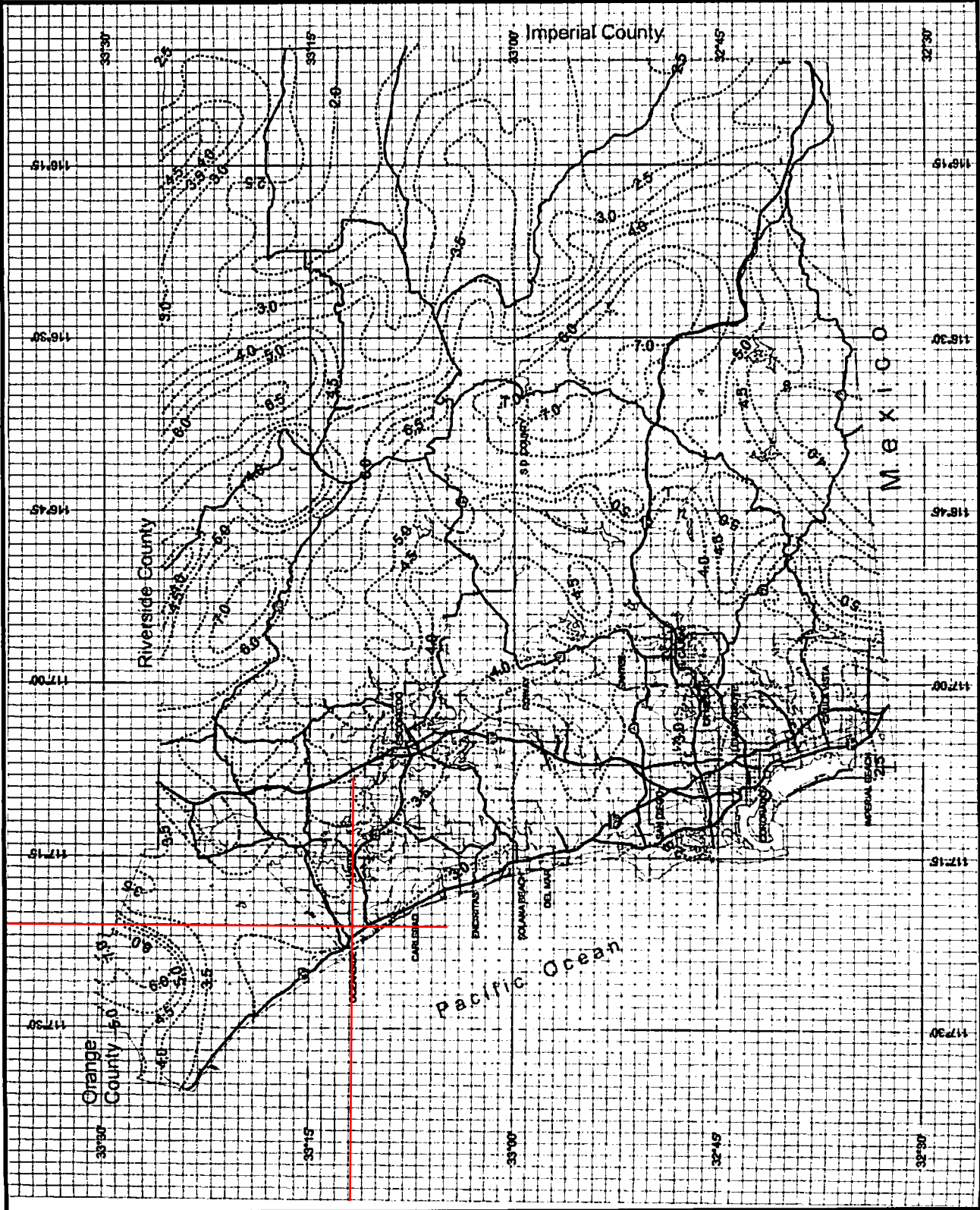


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OTC drugs are supervised without the Federal Food and Drug Administration (FDA) approval required for prescription drugs. OTC drugs are sold without a prescription.



3 0 3 Miles



**A-5**

**INTENSITY - DURATION DESIGN CHARTS  
(100-YEAR)**



Intensity-Duration Design Chart - Template

FIGURE

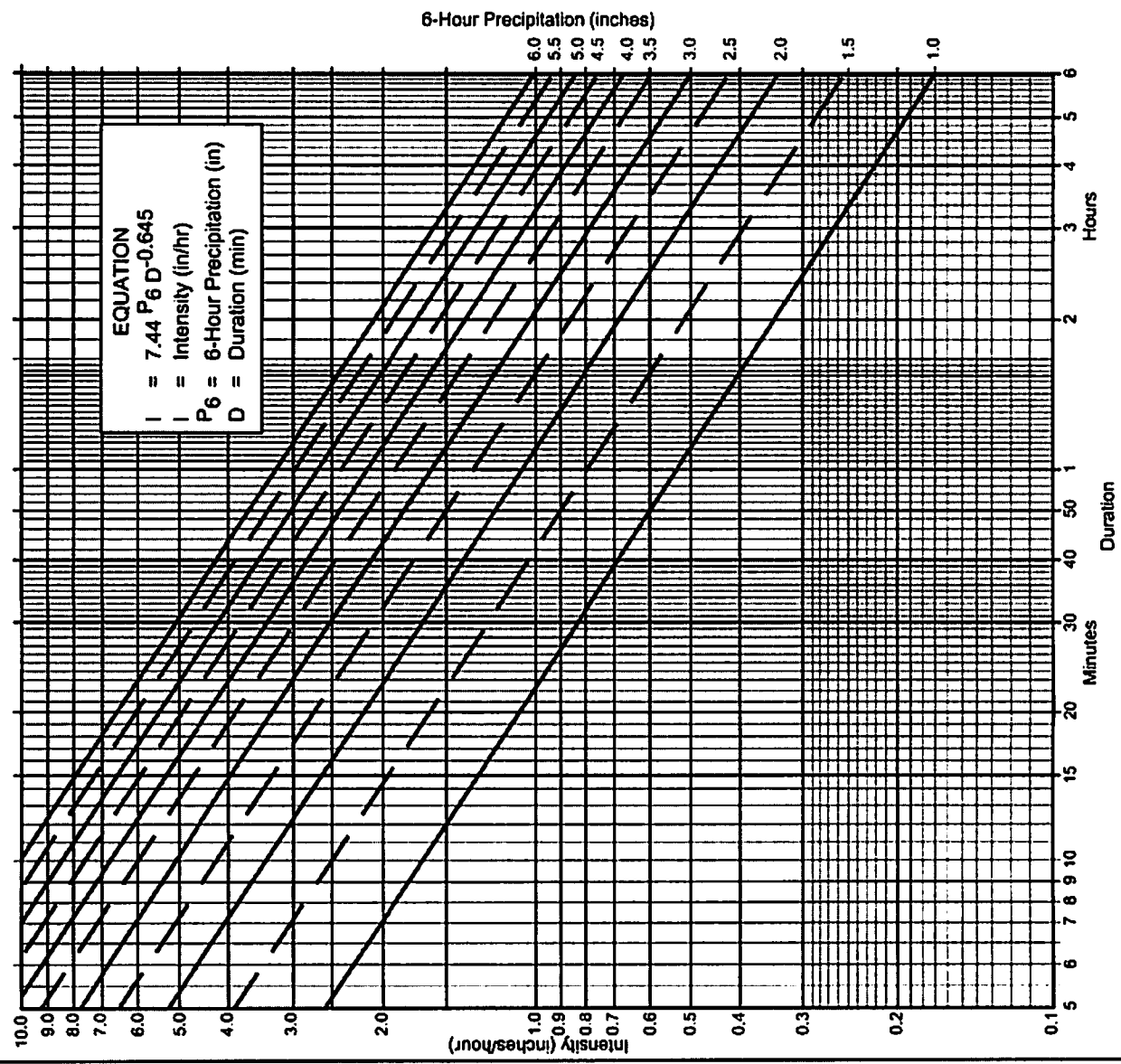
Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency \_\_\_\_\_ year
- (b)  $P_6 =$  \_\_\_\_\_ in.,  $P_{24} =$  \_\_\_\_\_,  $\frac{P_6}{P_{24}} =$  \_\_\_\_\_ % (2)
- (c) Adjusted  $P_6^{(2)} =$  \_\_\_\_\_ in.
- (d)  $t_x =$  \_\_\_\_\_ min.
- (e)  $I =$  \_\_\_\_\_ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.



P6	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
Duration	5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.60	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.29	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.39	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

## Rainfall Isopluvials

## 100 Year Rainfall Event - 6 Hours

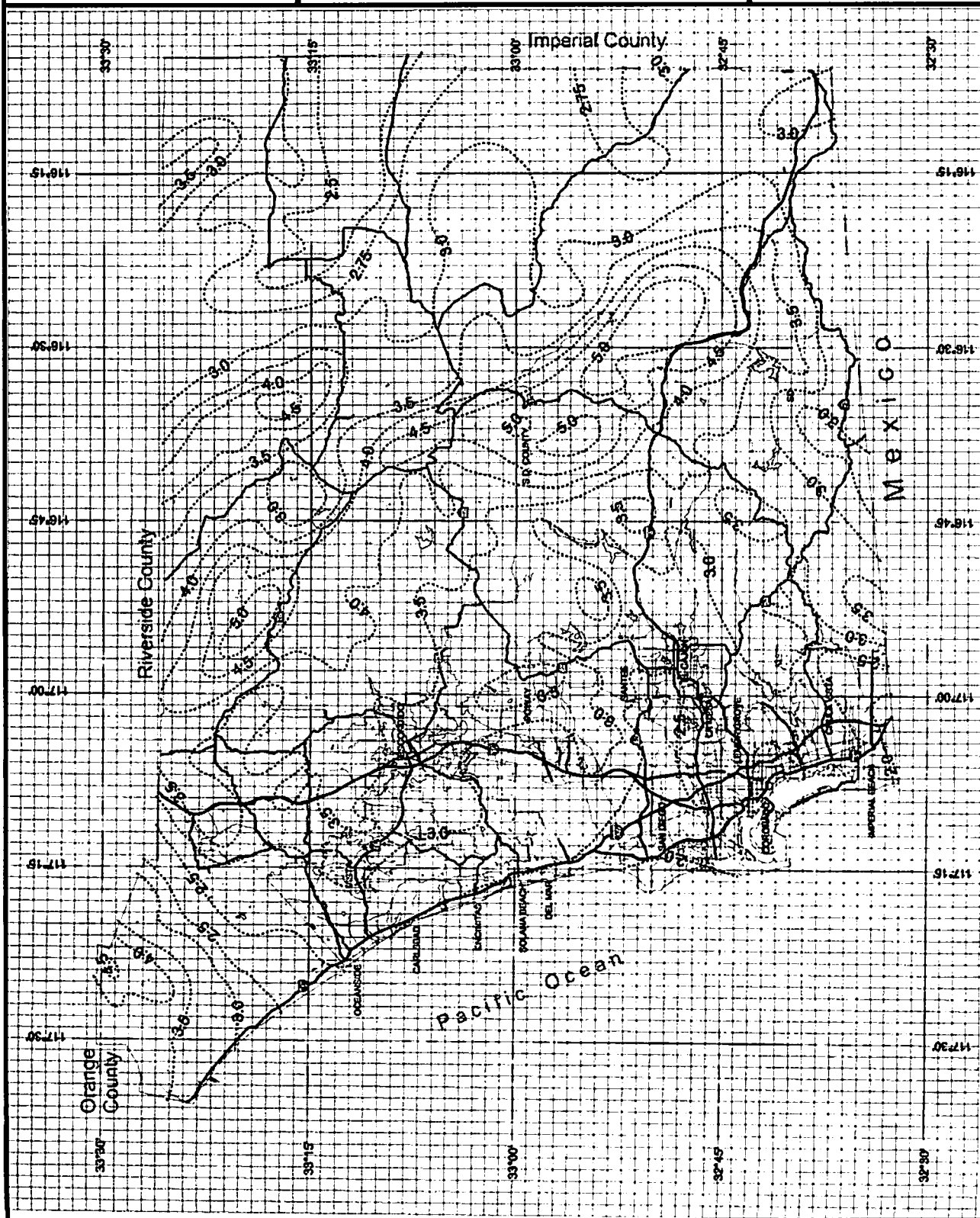
**Survival (inches)**



DOCTOR OF INFORMATION SCIENCE  
The degree program is aimed at those students who want to pursue a career in information science and/or library science. The program is designed to provide students with the knowledge and skills necessary to work in a variety of information science and library science settings. The program is designed to provide students with the knowledge and skills necessary to work in a variety of information science and library science settings. The program is designed to provide students with the knowledge and skills necessary to work in a variety of information science and library science settings.



3 0 3 Miles



# County of San Diego Hydrology Manual



## Rainfall Isophyets

100 Year Rainfall Event - 24 Hours

..... Isophyetal (inches)



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**A – 6**

**RATIONAL METHOD HYDROLOGY  
ONSITE PRE-CONDITION  
Q-2, 10 & 100 YEAR ANALYSIS  
(SEE MAP EXHIBIT A)**

# EX2. RES

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

(c) Copyright 1982-2012 Advanced Engineering Software (aes)  
Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

Buccola Engineering, Inc.  
3142 Vista Way, Suite 301  
Oceanside, CA 92056  
(760) 721-2000

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*

\* Pre-Development Condition Rational Method for 2-Year Storm Event \*

\*\*\*\*\*

FILE NAME: G:\1664\EX2.DAT  
TIME/DATE OF STUDY: 16:56 01/04/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 2.00

6-HOUR DURATION PRECIPITATION (INCHES) = 1.200

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL:	CURB	GUTTER-GEOMETRIES:			MANNING
	WIDTH	CROSSFALL			IN- / OUT-/PARK-	HEIGHT	WIDTH	
	(FT)	(FT)	SIDE / SIDE/ WAY	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 102.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
-----

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 84

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 160.10

DOWNSTREAM ELEVATION(FEET) = 156.50

ELEVATION DIFFERENCE(FEET) = 3.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.517

2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.431

Page 1

EX2. RES

SUBAREA RUNOFF(CFS) = 0.16  
TOTAL AREA(ACRES) = 0.14 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 104.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 156.50 DOWNSTREAM(FEET) = 151.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 340.00 CHANNEL SLOPE = 0.0162  
CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 5.000  
MANNING' S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 0.50  
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 1.810  
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
SOIL CLASSIFICATION IS "D"  
S. C. S. CURVE NUMBER (AMC II) = 84  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.79  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.30  
AVERAGE FLOW DEPTH(FEET) = 0.11 TRAVEL TIME(MIN.) = 4.35  
Tc(MIN.) = 11.87  
SUBAREA AREA(ACRES) = 1.48 SUBAREA RUNOFF(CFS) = 1.24  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.460  
TOTAL AREA(ACRES) = 1.6 PEAK FLOW RATE(CFS) = 1.35

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 1.59  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 440.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 11.87  
RAINFALL INTENSITY(INCH/HR) = 1.81  
TOTAL STREAM AREA(ACRES) = 1.62  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600  
SOIL CLASSIFICATION IS "D"  
S. C. S. CURVE NUMBER (AMC II) = 84  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 128.00  
UPSTREAM ELEVATION(FEET) = 156.50  
DOWNSTREAM ELEVATION(FEET) = 155.50  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.789  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 61.25  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.050  
SUBAREA RUNOFF(CFS) = 0.18  
TOTAL AREA(ACRES) = 0.19 TOTAL RUNOFF(CFS) = 0.18

\*\*\*\*\*

```

                                EX2. RES
FLOW PROCESS FROM NODE      501.00 TO NODE      104.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   155.50  DOWNSTREAM(FEET) =   151.10
CHANNEL LENGTH THRU SUBAREA(FEET) =   220.00  CHANNEL SLOPE =   0.0200
CHANNEL BASE(FEET) =    5.00  "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =    0.50
2 YEAR RAINFALL INTENSITY(INCH/HOUR) =   1.553
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =   84
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          0.25
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    0.70
AVERAGE FLOW DEPTH(FEET) =    0.05  TRAVEL TIME(MIN.) =    5.26
Tc(MIN.) =   15.05
SUBAREA AREA(ACRES) =    0.20  SUBAREA RUNOFF(CFS) =    0.14
AREA-AVERAGE RUNOFF COEFFICIENT =   0.460
TOTAL AREA(ACRES) =    0.4  PEAK FLOW RATE(CFS) =          0.28

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =   0.05  FLOW VELOCITY(FEET/SEC.) =    0.77
LONGEST FLOWPATH FROM NODE      500.00 TO NODE      104.00 =    348.00 FEET.

*****
FLOW PROCESS FROM NODE      104.00 TO NODE      104.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) =   15.05
RAINFALL INTENSITY(INCH/HR) =    1.55
TOTAL STREAM AREA(ACRES) =    0.39
PEAK FLOW RATE(CFS) AT CONFLUENCE =          0.28

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
1           1.35      11.87      1.810      1.62
2           0.28      15.05      1.553      0.39

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
1           1.57      11.87      1.810
2           1.44      15.05      1.553

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =    1.57  Tc(MIN.) =   11.87
TOTAL AREA(ACRES) =    2.0
LONGEST FLOWPATH FROM NODE      100.00 TO NODE      104.00 =    440.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) =    2.0  TC(MIN.) =   11.87
PEAK FLOW RATE(CFS) =    1.57
=====

```

# EX10. RES

\*\*\*\*\*

## RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

Buccola Engineering, Inc.  
3142 Vista Way, Suite 301  
Oceanside, CA 92056  
(760) 721-2000

## \*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*

\* Pre-Development Condition Rational Method for 10-Year Storm Event \*

\*\*\*\*\*

FILE NAME: G:\1664\EX10.DAT

TIME/DATE OF STUDY: 16:55 01/04/2017

## ----- USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: -----

### 2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 10.00

6-HOUR DURATION PRECIPITATION (INCHES) = 1.700

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB GUTTER-GEOMETRIES: HEIGHT (FT)	WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)						
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

### GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN

OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE. \*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 102.00 IS CODE = 21

## ----- >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<< -----

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 84

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 160.10

DOWNSTREAM ELEVATION(FEET) = 156.50

ELEVATION DIFFERENCE(FEET) = 3.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.517

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.443



```

                                EX10. RES
SUBAREA RUNOFF(CFS) =          0.22
TOTAL AREA(ACRES) =          0.14  TOTAL RUNOFF(CFS) =          0.22
*****
FLOW PROCESS FROM NODE      102.00 TO NODE      104.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    156.50  DOWNSTREAM(FEET) =    151.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    340.00  CHANNEL SLOPE =    0.0162
CHANNEL BASE(FEET) =     5.00  "Z" FACTOR =    5.000
MANNING' S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =    0.50
10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.655
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =    84
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          1.14
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.52
AVERAGE FLOW DEPTH(FEET) =    0.13  TRAVEL TIME(MIN.) =    3.73
Tc(MIN.) =    11.25
SUBAREA AREA(ACRES) =    1.48  SUBAREA RUNOFF(CFS) =    1.81
AREA-AVERAGE RUNOFF COEFFICIENT =    0.460
TOTAL AREA(ACRES) =    1.6  PEAK FLOW RATE(CFS) =          1.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =    0.18  FLOW VELOCITY(FEET/SEC.) =    1.86
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    104.00 =    440.00 FEET.
*****
FLOW PROCESS FROM NODE      104.00 TO NODE      104.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    11.25
RAINFALL INTENSITY(INCH/HR) =    2.66
TOTAL STREAM AREA(ACRES) =    1.62
PEAK FLOW RATE(CFS) AT CONFLUENCE =          1.98
*****
FLOW PROCESS FROM NODE      500.00 TO NODE      501.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =    84
INITIAL SUBAREA FLOW-LENGTH(FEET) =    128.00
UPSTREAM ELEVATION(FEET) =    156.50
DOWNSTREAM ELEVATION(FEET) =    155.50
ELEVATION DIFFERENCE(FEET) =    1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    9.789
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH =    61.25
         (Reference: Table 3-1B of Hydrology Manual)
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
10 YEAR RAINFALL INTENSITY(INCH/HOUR) =    2.904
SUBAREA RUNOFF(CFS) =    0.25
TOTAL AREA(ACRES) =    0.19  TOTAL RUNOFF(CFS) =    0.25
*****

```

```

                                EX10. RES
FLOW PROCESS FROM NODE      501.00 TO NODE      104.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   155.50  DOWNSTREAM(FEET) =   151.10
CHANNEL LENGTH THRU SUBAREA(FEET) =   220.00  CHANNEL SLOPE =   0.0200
CHANNEL BASE(FEET) =    5.00  "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =    0.50
  10 YEAR RAINFALL INTENSITY(INCH/HOUR) =   2.277
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =   84
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          0.36
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    0.82
AVERAGE FLOW DEPTH(FEET) =    0.06  TRAVEL TIME(MIN.) =    4.49
Tc(MIN.) =   14.28
SUBAREA AREA(ACRES) =    0.20  SUBAREA RUNOFF(CFS) =    0.21
AREA-AVERAGE RUNOFF COEFFICIENT =   0.460
TOTAL AREA(ACRES) =    0.4  PEAK FLOW RATE(CFS) =          0.41

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =   0.06  FLOW VELOCITY(FEET/SEC.) =    0.89
LONGEST FLOWPATH FROM NODE      500.00 TO NODE      104.00 =    348.00 FEET.

*****
FLOW PROCESS FROM NODE      104.00 TO NODE      104.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) =   14.28
RAINFALL INTENSITY(INCH/HR) =    2.28
TOTAL STREAM AREA(ACRES) =    0.39
PEAK FLOW RATE(CFS) AT CONFLUENCE =    0.41

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
    1         1.98      11.25      2.655        1.62
    2         0.41      14.28      2.277        0.39

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
    1         2.31      11.25      2.655
    2         2.11      14.28      2.277

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =    2.31  Tc(MIN.) =   11.25
TOTAL AREA(ACRES) =    2.0
LONGEST FLOWPATH FROM NODE      100.00 TO NODE      104.00 =    440.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) =    2.0  TC(MIN.) =   11.25
PEAK FLOW RATE(CFS) =    2.31
=====

```

# EX100. RES

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

Buccola Engineering, Inc.  
3142 Vista Way, Suite 301  
Oceanside, CA 92056  
(760) 721-2000

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*  
\* Pre-Development Condition Rational Method for 100-Year Storm Event \*  
\*

\*\*\*\*\*

FILE NAME: G:\1664\EX100.DAT  
TIME/DATE OF STUDY: 16:14 01/04/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 2.700

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB GUTTER-GEOMETRIES: HEIGHT (FT)	MANNING			FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)			WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 102.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 84

INITIAL SUBAREA FLOW-LENGTH(Feet) = 100.00

UPSTREAM ELEVATION(Feet) = 160.10

DOWNSTREAM ELEVATION(Feet) = 156.50

ELEVATION DIFFERENCE(Feet) = 3.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.517

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.469

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                                EX100. RES
SUBAREA RUNOFF(CFS) =          0.36
TOTAL AREA(ACRES) =          0.14  TOTAL RUNOFF(CFS) =          0.36
*****
FLOW PROCESS FROM NODE      102.00 TO NODE      104.00 IS CODE =   51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    156.50  DOWNSTREAM(FEET) =    151.00
CHANNEL LENGTH THRU SUBAREA(FEET) =    340.00  CHANNEL SLOPE =    0.0162
CHANNEL BASE(FEET) =     5.00  "Z" FACTOR =    5.000
MANNING' S FACTOR = 0.030  MAXIMUM DEPTH(FEET) =    0.50
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.354
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =    84
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          1.87
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    1.78
AVERAGE FLOW DEPTH(FEET) =    0.18  TRAVEL TIME(MIN.) =    3.19
Tc(MIN.) =    10.70
SUBAREA AREA(ACRES) =    1.48  SUBAREA RUNOFF(CFS) =    2.97
AREA-AVERAGE RUNOFF COEFFICIENT =    0.460
TOTAL AREA(ACRES) =    1.6  PEAK FLOW RATE(CFS) =    3.26

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =    0.24  FLOW VELOCITY(FEET/SEC.) =    2.18
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    104.00 =    440.00 FEET.
*****
FLOW PROCESS FROM NODE      104.00 TO NODE      104.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    10.70
RAINFALL INTENSITY(INCH/HR) =    4.35
TOTAL STREAM AREA(ACRES) =    1.63
PEAK FLOW RATE(CFS) AT CONFLUENCE =    3.26
*****
FLOW PROCESS FROM NODE      500.00 TO NODE      501.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
RESIDENTIAL (2. DU/AC OR LESS) RUNOFF COEFFICIENT = .4600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =    84
INITIAL SUBAREA FLOW-LENGTH(FEET) =    128.00
UPSTREAM ELEVATION(FEET) =    156.50
DOWNSTREAM ELEVATION(FEET) =    155.50
ELEVATION DIFFERENCE(FEET) =    1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    9.789
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH =    61.25
         (Reference: Table 3-1B of Hydrology Manual)
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.612
SUBAREA RUNOFF(CFS) =    0.40
TOTAL AREA(ACRES) =    0.19  TOTAL RUNOFF(CFS) =    0.40
*****

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EX100. RES  
FLOW PROCESS FROM NODE 501.00 TO NODE 104.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM( FEET ) = 155.50 DOWNSTREAM( FEET ) = 151.10  
CHANNEL LENGTH THRU SUBAREA( FEET ) = 220.00 CHANNEL SLOPE = 0.0200  
CHANNEL BASE( FEET ) = 5.00 "Z" FACTOR = 50.000  
MANNING' S FACTOR = 0.030 MAXIMUM DEPTH( FEET ) = 0.50  
100 YEAR RAINFALL INTENSITY( INCH/ HOUR ) = 3.713  
RESIDENTIAL (2. DU/ AC OR LESS) RUNOFF COEFFICIENT = .4600  
SOIL CLASSIFICATION IS "D"  
S. C. S. CURVE NUMBER ( AMC II ) = 84  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS ) = 0.57  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/ SEC. ) = 0.94  
AVERAGE FLOW DEPTH( FEET ) = 0.07 TRAVEL TIME( MIN. ) = 3.91  
Tc( MIN. ) = 13.70  
SUBAREA AREA( ACRES ) = 0.20 SUBAREA RUNOFF( CFS ) = 0.34  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.460  
TOTAL AREA( ACRES ) = 0.4 PEAK FLOW RATE( CFS ) = 0.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH( FEET ) = 0.07 FLOW VELOCITY( FEET/ SEC. ) = 1.05  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 104.00 = 348.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION( MIN. ) = 13.70  
RAINFALL INTENSITY( INCH/ HR ) = 3.71  
TOTAL STREAM AREA( ACRES ) = 0.39  
PEAK FLOW RATE( CFS ) AT CONFLUENCE = 0.67

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF ( CFS )	Tc ( MIN. )	INTENSITY ( INCH/ HOUR )	AREA ( ACRE )
1	3.26	10.70	4.354	1.63
2	0.67	13.70	3.713	0.39

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF ( CFS )	Tc ( MIN. )	INTENSITY ( INCH/ HOUR )
1	3.78	10.70	4.354
2	3.45	13.70	3.713

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE( CFS ) = 3.78 Tc( MIN. ) = 10.70  
TOTAL AREA( ACRES ) = 2.0  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 440.00 FEET.

END OF STUDY SUMMARY:  
TOTAL AREA( ACRES ) = 2.0 TC( MIN. ) = 10.70  
PEAK FLOW RATE( CFS ) = 3.78

**A – 7**

**RATIONAL METHOD HYDROLOGY  
ONSITE POST CONDITION  
Q- 2, 10 & 100 YEAR  
ANALYSIS  
(SEE MAP EXHIBIT B)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

Buccola Engineering, Inc.  
3142 Vista Way, Suite 301  
Oceanside, CA 92056  
(760) 721-2000

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*

\* Post-Development Condition Rational Method for 2-Year Storm Event \*

\*\*\*\*\*

FILE NAME: G:\1664\P2.DAT

TIME/DATE OF STUDY: 16:13 01/12/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 2.00

6-HOUR DURATION PRECIPITATION (INCHES) = 1.200

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SPECIFIED CONSTANT RUNOFF COEFFICIENT = 0.760

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL:	CURB	GUTTER-GEOMETRIES:			MANNING
	WIDTH	CROSSFALL			IN- / OUT-/PARK-	HEIGHT	WIDTH	
	(FT)	(FT)	SIDE / SIDE/ WAY	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 88

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 153.10

DOWNSTREAM ELEVATION(FEET) = 152.50

ELEVATION DIFFERENCE(FEET) = 0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.741

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2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.14  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.14

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET ) =	151.80	DOWNSTREAM( FEET ) =	151.56
FLOW LENGTH( FEET ) =	35.00	MANNING' S N =	0.013
DEPTH OF FLOW IN	6.0 INCH	PIPE IS	2.3 INCHES
PIPE-FLOW VELOCITY( FEET/SEC. ) =	2.05		
ESTIMATED PIPE DIAMETER( INCH ) =	6.00	NUMBER OF PIPES =	1
PIPE-FLOW( CFS ) =	0.14		
PIPE TRAVEL TIME( MIN. ) =	0.28	Tc( MIN. ) =	5.03
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	102.00 =	95.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.151
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS	"D"
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.08 SUBAREA RUNOFF(CFS) = 0.19
TOTAL AREA(ACRES) =	0.1 TOTAL RUNOFF(CFS) = 0.34
TC(MIN. ) =	5.03

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET ) =	151.56	DOWNSTREAM( FEET ) =	151.38
FLOW LENGTH( FEET ) =	28.00	MANNING' S N =	0.013
DEPTH OF FLOW IN	6.0 INCH	PIPE IS	4.0 INCHES
PIPE-FLOW VELOCITY( FEET/SEC. ) =	2.41		
ESTIMATED PIPE DIAMETER( INCH ) =	6.00	NUMBER OF PIPES =	1
PIPE-FLOW( CFS ) =	0.34		
PIPE TRAVEL TIME( MIN. ) =	0.19	Tc( MIN. ) =	5.22
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	103.00 =	123.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.076
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS	"D"
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.15 SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) =	0.3 TOTAL RUNOFF(CFS) = 0.68



TC(MIN. ) = 5.22

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	151.38	DOWNSTREAM(FEET) =	150.81
FLOW LENGTH(FEET) =	48.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	3.9 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	3.64		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.68		
PIPE TRAVEL TIME(MIN. ) =	0.22	Tc(MIN. ) =	5.44
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	104.00 =	171.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.995
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS "D"	
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.03
SUBAREA RUNOFF(CFS) =	0.07
TOTAL AREA(ACRES) =	0.3
TOTAL RUNOFF(CFS) =	0.73
TC(MIN. ) =	5.44

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	150.81	DOWNSTREAM(FEET) =	149.90
FLOW LENGTH(FEET) =	45.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	6.0 INCH PIPE IS	4.7 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	4.37		
ESTIMATED PIPE DIAMETER(INCH) =	6.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.73		
PIPE TRAVEL TIME(MIN. ) =	0.17	Tc(MIN. ) =	5.61
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	105.00 =	216.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN. ) =	5.61
RAINFALL INTENSITY(INCH/HR) =	2.94
TOTAL STREAM AREA(ACRES) =	0.32
PEAK FLOW RATE(CFS) AT CONFLUENCE =	0.73

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

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=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 153.10
DOWNSTREAM ELEVATION(FEET) = 152.20
ELEVATION DIFFERENCE(FEET) = 0.90
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.934
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
          2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.07
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.07

*****
FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 7
-----
>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 5.08 RAIN INTENSITY(INCH/HOUR) = 3.13
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.10

*****
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 151.20 DOWNSTREAM(FEET) = 150.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 1.84
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.10
PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 5.58
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 145.00 FEET.

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
          2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.947
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8617
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.13
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.23
TC(MIN.) = 5.58

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

```

```

                                P2R. RES
      2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.947
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8304
SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.09
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.32
TC(MIN.) = 5.58

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.80 DOWNSTREAM(FEET) = 150.25
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.84
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.32
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 5.90
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 200.00 FEET.

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
      2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.842
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8058
SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.15
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.46
TC(MIN.) = 5.90

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
      2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.842
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7998
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.06
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.52
TC(MIN.) = 5.90

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 105.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.25 DOWNSTREAM(FEET) = 149.90
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013

```

P2R. RES

DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.08  
 ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.52  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 6.09  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 105.00 = 235.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.09  
 RAINFALL INTENSITY(INCH/HR) = 2.78  
 TOTAL STREAM AREA(ACRES) = 0.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.52

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/ HOUR)	AREA (ACRE)
1	0.73	5.61	2.935	0.32
2	0.52	6.09	2.785	0.23

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/ HOUR)
1	1.21	5.61	2.935
2	1.21	6.09	2.785

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 1.21 Tc(MIN.) = 6.09  
 TOTAL AREA(ACRES) = 0.6  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 105.00 = 235.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 149.90 DOWNSTREAM(FEET) = 149.30  
 FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.29  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.21  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 6.27  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 106.00 = 283.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.27

```

                                P2R. RES
RAINFALL INTENSITY(INCH/HR) = 2.73
TOTAL STREAM AREA(ACRES) = 0.55
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.21

*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00
UPSTREAM ELEVATION(FEET) = 153.00
DOWNSTREAM ELEVATION(FEET) = 152.75
ELEVATION DIFFERENCE(FEET) = 0.25
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.10
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.10

*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 7
-----
>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 5.14 RAIN INTENSITY(INCH/HOUR) = 3.11
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.10

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 106.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26
STREET LENGTH(FEET) = 82.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.25
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 2.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.33
STREET FLOW TRAVEL TIME(MIN.) = 0.81 Tc(MIN.) = 5.96
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.825
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88

```

P2R. RES  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.39

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.21 HALFSTREET FLOOD WIDTH(FEET) = 2.72  
 FLOW VELOCITY(FEET/SEC.) = 1.51 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.32  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 127.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1  
 -----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	5.96
RAINFALL INTENSITY(INCH/HR) =	2.82
TOTAL STREAM AREA(ACRES) =	0.18
PEAK FLOW RATE(CFS) AT CONFLUENCE =	0.39

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.21	6.27	2.731	0.55
2	0.39	5.96	2.825	0.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.57	5.96	2.825
2	1.59	6.27	2.731

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 1.59 Tc(MIN.) = 6.27  
 TOTAL AREA(ACRES) = 0.7  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 106.00 = 283.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31  
 -----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	148.00	DOWNSTREAM(FEET) =	147.50
FLOW LENGTH(FEET) =	16.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS	4.9 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	6.49		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	1.59		
PIPE TRAVEL TIME(MIN.) =	0.04	Tc(MIN.) =	6.32
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 =	299.00 FEET.		

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 10  
 -----

>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

P2R. RES

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21  
 -----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 INITIAL SUBAREA FLOW-LENGTH(Feet) = 57.00  
 UPSTREAM ELEVATION(Feet) = 156.10  
 DOWNSTREAM ELEVATION(Feet) = 153.90  
 ELEVATION DIFFERENCE(Feet) = 2.20  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.946  
 2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.13  
 TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.13

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 91  
 -----

>>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<<

=====

UPSTREAM NODE ELEVATION(Feet) = 153.90  
 DOWNSTREAM NODE ELEVATION(Feet) = 153.00  
 CHANNEL LENGTH THRU SUBAREA(Feet) = 58.00  
 "V" GUTTER WIDTH(Feet) = 3.00 GUTTER HIKE(Feet) = 0.050  
 PAVEMENT LIP(Feet) = 0.030 MANNING'S N = .0150  
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.03500  
 MAXIMUM DEPTH(Feet) = 0.20  
 2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.29  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 1.75  
 AVERAGE FLOW DEPTH(Feet) = 0.08 FLOOD WIDTH(Feet) = 3.05  
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 3.50  
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.32  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.760  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.46

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH(Feet) = 0.10 FLOOD WIDTH(Feet) = 3.91  
 FLOW VELOCITY(Feet/Sec.) = 2.07 DEPTH\*VELOCITY(Ft\*Ft/Sec) = 0.20  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 115.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 31  
 -----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 151.10 DOWNSTREAM(Feet) = 150.70  
 FLOW LENGTH(Feet) = 67.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 3.8 INCHES  
 PIPE-FLOW VELOCITY(Feet/Sec.) = 2.54  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.46  
 PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 3.94  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 503.00 = 182.00 FEET.

P2R. RES

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 503.00 TO NODE 503.00 IS CODE = 81  
 -----

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.06  
 TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.52  
 TC(MIN.) = 3.94

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 503.00 TO NODE 504.00 IS CODE = 31  
 -----

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 150.70 DOWNSTREAM(FEET) = 150.50  
 FLOW LENGTH(FEET) = 36.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.56  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.52  
 PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 4.17  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 504.00 = 218.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81  
 -----

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.68  
 TC(MIN.) = 4.17

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81  
 -----

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.13  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.82  
 TC(MIN.) = 4.17

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 504.00 TO NODE 505.00 IS CODE = 31  
 -----



```

                                P2R. RES
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.50 DOWNSTREAM(FEET) = 150.20
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.84
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.82
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 4.49
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 505.00 = 273.00 FEET.

*****
FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.18
TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.00
TC(MIN.) = 4.49

*****
FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.07
TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.07
TC(MIN.) = 4.49

*****
FLOW PROCESS FROM NODE 505.00 TO NODE 506.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.20 DOWNSTREAM(FEET) = 149.30
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.91
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.07
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 4.86
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 506.00 = 358.00 FEET.

*****
FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2

```

P2R.RES

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 4.86  
 RAINFALL INTENSITY(INCH/HR) = 3.16  
 TOTAL STREAM AREA(ACRES) = 0.45  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00  
 UPSTREAM ELEVATION(FEET) = 153.00  
 DOWNSTREAM ELEVATION(FEET) = 152.75  
 ELEVATION DIFFERENCE(FEET) = 0.25  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994  
 2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.16  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.16

\*\*\*\*\*

FLOW PROCESS FROM NODE 601.00 TO NODE 506.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26  
 STREET LENGTH(FEET) = 81.00 CURB HEIGHT(INCHES) = 8.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.30  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.20  
 HALFSTREET FLOOD WIDTH(FEET) = 2.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.69  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.33  
 STREET FLOW TRAVEL TIME(MIN.) = 0.80 Tc(MIN.) = 5.79  
 2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.875

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.760  
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.29  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.44

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 3.53  
 FLOW VELOCITY(FEET/SEC.) = 1.43 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.32  
 LONGEST FLOWPATH FROM NODE 600.00 TO NODE 506.00 = 126.00 FEET.

# P2R. RES

```
*****
FLOW PROCESS FROM NODE      506.00 TO NODE      506.00 IS CODE =   1
-----
```

```
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
```

```
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =   5.79
RAINFALL INTENSITY(INCH/HR) =   2.88
TOTAL STREAM AREA(ACRES) =   0.20
PEAK FLOW RATE(CFS) AT CONFLUENCE =   0.44
```

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.07	4.86	3.162	0.45
2	0.44	5.79	2.875	0.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	1.44	4.86	3.162
2	1.41	5.79	2.875

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) =   1.44   Tc(MIN.) =   4.86
TOTAL AREA(ACRES) =   0.6
LONGEST FLOWPATH FROM NODE      500.00 TO NODE      506.00 =   358.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE      506.00 TO NODE      507.00 IS CODE =  31
-----
```

```
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) =  148.00 DOWNSTREAM(FEET) =  147.50
FLOW LENGTH(FEET) =   16.00 MANNING'S N =  0.013
DEPTH OF FLOW IN   9.0 INCH PIPE IS   4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   6.33
ESTIMATED PIPE DIAMETER(INCH) =   9.00   NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =   1.44
PIPE TRAVEL TIME(MIN.) =   0.04   Tc(MIN.) =   4.90
LONGEST FLOWPATH FROM NODE      500.00 TO NODE      507.00 =   374.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE      507.00 TO NODE      107.00 IS CODE =  11
-----
```

```
>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
=====
```

## \*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.44	4.90	3.162	0.65

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 107.00 = 374.00 FEET.

## \*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------

1 1.59 6.32 P2R. RES  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 0.73 107.00 = 299.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.67	4.90	3.162
2	2.83	6.32	2.720

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.83 Tc(MIN.) = 6.32  
 TOTAL AREA(ACRES) = 1.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 147.50 DOWNSTREAM(FEET) = 146.40  
 FLOW LENGTH(FEET) = 97.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.07  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.83  
 PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 6.63  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 108.00 = 471.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.63  
 RAINFALL INTENSITY(INCH/HR) = 2.63  
 TOTAL STREAM AREA(ACRES) = 1.38  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600

S. C. S. CURVE NUMBER (AMC II) = 79

INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00

UPSTREAM ELEVATION(FEET) = 152.40

DOWNSTREAM ELEVATION(FEET) = 151.70

ELEVATION DIFFERENCE(FEET) = 0.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.971

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN

THE MAXIMUM OVERLAND FLOW LENGTH = 63.00

(Reference: Table 3-1B of Hydrology Manual)

THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.07

TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.07

\*\*\*\*\*

```

                                P2R.RES
FLOW PROCESS FROM NODE      701.00 TO NODE      701.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    2 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) =  79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) =      0.06  SUBAREA RUNOFF(CFS) =      0.16
TOTAL AREA(ACRES) =      0.1    TOTAL RUNOFF(CFS) =      0.23
TC(MIN.) =      4.97

*****
FLOW PROCESS FROM NODE      701.00 TO NODE      702.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  150.60  DOWNSTREAM(FEET) =  150.18
FLOW LENGTH(FEET) =  90.00  MANNING'S N =  0.013
DEPTH OF FLOW IN  6.0 INCH PIPE IS  3.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  1.93
ESTIMATED PIPE DIAMETER(INCH) =  6.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  0.23
PIPE TRAVEL TIME(MIN.) =  0.78  Tc(MIN.) =  5.75
LONGEST FLOWPATH FROM NODE      700.00 TO NODE      702.00 =  165.00 FEET.

*****
FLOW PROCESS FROM NODE      702.00 TO NODE      702.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    2 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.890
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) =  79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) =      0.05  SUBAREA RUNOFF(CFS) =      0.12
TOTAL AREA(ACRES) =      0.2    TOTAL RUNOFF(CFS) =      0.33
TC(MIN.) =      5.75

*****
FLOW PROCESS FROM NODE      702.00 TO NODE      703.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  150.18  DOWNSTREAM(FEET) =  149.90
FLOW LENGTH(FEET) =  55.00  MANNING'S N =  0.013
DEPTH OF FLOW IN  6.0 INCH PIPE IS  4.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  2.19
ESTIMATED PIPE DIAMETER(INCH) =  6.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  0.33
PIPE TRAVEL TIME(MIN.) =  0.42  Tc(MIN.) =  6.17
LONGEST FLOWPATH FROM NODE      700.00 TO NODE      703.00 =  220.00 FEET.

*****
FLOW PROCESS FROM NODE      703.00 TO NODE      704.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

```

P2R. RES

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 147.13
FLOW LENGTH(FEET) = 14.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.78
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.33
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 6.20
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 704.00 = 234.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 704.00 TO NODE 704.00 IS CODE = 81
-----
```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```
=====
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.752
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.64
TC(MIN.) = 6.20
```

```
*****
FLOW PROCESS FROM NODE 704.00 TO NODE 705.00 IS CODE = 31
-----
```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 147.13 DOWNSTREAM(FEET) = 146.40
FLOW LENGTH(FEET) = 12.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.62
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.64
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 6.23
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 705.00 = 246.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 705.00 TO NODE 705.00 IS CODE = 1
-----
```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.23
RAINFALL INTENSITY(INCH/HR) = 2.74
TOTAL STREAM AREA(ACRES) = 0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.64
```

```
*****
FLOW PROCESS FROM NODE 800.00 TO NODE 801.00 IS CODE = 21
-----
```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 152.40
DOWNSTREAM ELEVATION(FEET) = 151.70
ELEVATION DIFFERENCE(FEET) = 0.70
```

```

                                P2R. RES
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.971
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 63.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
          2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.07
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.07

*****
FLOW PROCESS FROM NODE 801.00 TO NODE 801.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
          2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.162
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.13
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.20
TC(MIN.) = 4.97

*****
FLOW PROCESS FROM NODE 801.00 TO NODE 802.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.60 DOWNSTREAM(FEET) = 150.15
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 1.94
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.20
PIPE TRAVEL TIME(MIN.) = 0.77 Tc(MIN.) = 5.74
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 802.00 = 165.00 FEET.

*****
FLOW PROCESS FROM NODE 802.00 TO NODE 802.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
          2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.891
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.14
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.33
TC(MIN.) = 5.74

*****
FLOW PROCESS FROM NODE 802.00 TO NODE 803.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.15 DOWNSTREAM(FEET) = 149.90
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.6 INCHES

```

```

                                P2R. RES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.05
ESTIMATED PIPE DIAMETER(INCH) = 6.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.33
PIPE TRAVEL TIME(MIN.) = 0.45    Tc(MIN.) = 6.19
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 803.00 = 220.00 FEET.

*****
FLOW PROCESS FROM NODE 803.00 TO NODE 804.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 147.13
FLOW LENGTH(FEET) = 14.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.79
ESTIMATED PIPE DIAMETER(INCH) = 6.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.33
PIPE TRAVEL TIME(MIN.) = 0.03    Tc(MIN.) = 6.22
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 804.00 = 234.00 FEET.

*****
FLOW PROCESS FROM NODE 804.00 TO NODE 804.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
2 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.745
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.32
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.64
TC(MIN.) = 6.22

*****
FLOW PROCESS FROM NODE 804.00 TO NODE 805.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 147.13 DOWNSTREAM(FEET) = 146.40
FLOW LENGTH(FEET) = 12.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.60
ESTIMATED PIPE DIAMETER(INCH) = 6.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.64
PIPE TRAVEL TIME(MIN.) = 0.03    Tc(MIN.) = 6.25
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 805.00 = 246.00 FEET.

*****
FLOW PROCESS FROM NODE 805.00 TO NODE 705.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.25
RAINFALL INTENSITY(INCH/HR) = 2.74
TOTAL STREAM AREA(ACRES) = 0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.64

```



P2R. RES

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN. )	I NTENSI TY (I NCH/HOUR)	AREA (ACRE)
1	2. 83	6. 63	2. 635	1. 38
2	0. 64	6. 23	2. 743	0. 31
3	0. 64	6. 25	2. 736	0. 31

RAINFALL I NTENSI TY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN. )	I NTENSI TY (I NCH/HOUR)
1	3. 93	6. 23	2. 743
2	3. 94	6. 25	2. 736
3	4. 05	6. 63	2. 635

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 4. 05 Tc(MIN. ) = 6. 63

TOTAL AREA(ACRES) = 2. 0

LONGEST FLOWPATH FROM NODE 500. 00 TO NODE 705. 00 = 471. 00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2. 0 TC(MIN. ) = 6. 63

PEAK FLOW RATE(CFS) = 4. 05

=====

=====

END OF RATIONAL METHOD ANALYSIS

♀

\*\*\*\*\*

## RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

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Oceanside, CA 92056  
(760) 721-2000

## \*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*  
\* Post-Development Condition Rational Method for 10-Year Storm Event \*  
\*

\*\*\*\*\*

FILE NAME: G:\1664\P10.DAT

TIME/DATE OF STUDY: 16:14 01/12/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

## 2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 10.00

6-HOUR DURATION PRECIPITATION (INCHES) = 1.700

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SPECIFIED CONSTANT RUNOFF COEFFICIENT = 0.760

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-CROWN TO STREET-CROSSFALL:		CURB GUTTER-GEOMETRIES:	MANNING	
	WIDTH (FT)	CROSSFALL (FT)			IN- / OUT-/PARK- HEIGHT (FT)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167 0.0150

## GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 88

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 153.10

DOWNSTREAM ELEVATION(FEET) = 152.50

ELEVATION DIFFERENCE(FEET) = 0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.741

```

                                P10R. RES
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479
    NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
    SUBAREA RUNOFF(CFS) = 0.20
    TOTAL AREA(ACRES) = 0.06    TOTAL RUNOFF(CFS) = 0.20

*****
FLOW PROCESS FROM NODE    101.00 TO NODE    102.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 151.80 DOWNSTREAM(FEET) = 151.56
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.22
ESTIMATED PIPE DIAMETER(INCH) = 6.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.20
PIPE TRAVEL TIME(MIN.) = 0.26    Tc(MIN.) = 5.00
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    102.00 = 95.00 FEET.

*****
FLOW PROCESS FROM NODE    102.00 TO NODE    102.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.477
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    SOIL CLASSIFICATION IS "D"
    S. C. S. CURVE NUMBER (AMC II) = 88
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) = 0.08    SUBAREA RUNOFF(CFS) = 0.27
    TOTAL AREA(ACRES) = 0.1    TOTAL RUNOFF(CFS) = 0.48
    TC(MIN.) = 5.00

*****
FLOW PROCESS FROM NODE    102.00 TO NODE    103.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 151.56 DOWNSTREAM(FEET) = 151.38
FLOW LENGTH(FEET) = 28.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.65
ESTIMATED PIPE DIAMETER(INCH) = 9.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.48
PIPE TRAVEL TIME(MIN.) = 0.18    Tc(MIN.) = 5.18
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    103.00 = 123.00 FEET.

*****
FLOW PROCESS FROM NODE    103.00 TO NODE    103.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.378
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    SOIL CLASSIFICATION IS "D"
    S. C. S. CURVE NUMBER (AMC II) = 88
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) = 0.15    SUBAREA RUNOFF(CFS) = 0.50
    TOTAL AREA(ACRES) = 0.3    TOTAL RUNOFF(CFS) = 0.96

```

TC(MIN. ) = 5.18

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	151.38	DOWNSTREAM(FEET) =	150.81
FLOW LENGTH(FEET) =	48.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	4.8 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	3.99		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.96		
PIPE TRAVEL TIME(MIN. ) =	0.20	Tc(MIN. ) =	5.38
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	104.00 =	171.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.272
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS "D"	
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.03
SUBAREA RUNOFF(CFS) =	0.10
TOTAL AREA(ACRES) =	0.3
TOTAL RUNOFF(CFS) =	1.04
TC(MIN. ) =	5.38

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	150.81	DOWNSTREAM(FEET) =	149.90
FLOW LENGTH(FEET) =	45.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	4.3 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	4.96		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	1.04		
PIPE TRAVEL TIME(MIN. ) =	0.15	Tc(MIN. ) =	5.53
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	105.00 =	216.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN. ) =	5.53
RAINFALL INTENSITY(INCH/HR) =	4.20
TOTAL STREAM AREA(ACRES) =	0.32
PEAK FLOW RATE(CFS) AT CONFLUENCE =	1.04

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

P10R. RES

```

=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 153.10
DOWNSTREAM ELEVATION(FEET) = 152.20
ELEVATION DIFFERENCE(FEET) = 0.90
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.934
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.10
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.10

*****
FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 7
-----
>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 5.08 RAIN INTENSITY(INCH/HOUR) = 4.43
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.10

*****
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 151.20 DOWNSTREAM(FEET) = 150.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 1.84
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.10
PIPE TRAVEL TIME(MIN.) = 0.50 Tc(MIN.) = 5.58
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 145.00 FEET.

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.175
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7573
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.19
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.28
TC(MIN.) = 5.58

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

```

```

                                P10R. RES
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.175
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7581
SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.13
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.41
TC(MIN.) = 5.58

*****
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.80 DOWNSTREAM(FEET) = 150.25
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.00
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.41
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 5.88
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 200.00 FEET.

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.034
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7588
SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.21
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.61
TC(MIN.) = 5.88

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.034
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7589
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.09
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.70
TC(MIN.) = 5.88

*****
FLOW PROCESS FROM NODE 203.00 TO NODE 105.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.25 DOWNSTREAM(FEET) = 149.90
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013

```

P10R. RES  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.44  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.70  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 6.05  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 105.00 = 235.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.05  
 RAINFALL INTENSITY(INCH/HR) = 3.96  
 TOTAL STREAM AREA(ACRES) = 0.23  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.70

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/ HOUR)	AREA (ACRE)
1	1.04	5.53	4.197	0.32
2	0.70	6.05	3.961	0.23

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/ HOUR)
1	1.68	5.53	4.197
2	1.68	6.05	3.961

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 1.68 Tc(MIN.) = 6.05  
 TOTAL AREA(ACRES) = 0.6  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 105.00 = 235.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 149.90 DOWNSTREAM(FEET) = 149.30  
 FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.53  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.68  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 6.23  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 106.00 = 283.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.23

P10R. RES  
 RAINFALL INTENSITY(INCH/HR) = 3.89  
 TOTAL STREAM AREA(ACRES) = 0.55  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.68

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21  
 -----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

=====

\*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 SOIL CLASSIFICATION IS "D"  
 S. C. S. CURVE NUMBER (AMC II) = 88  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00  
 UPSTREAM ELEVATION(FEET) = 153.00  
 DOWNSTREAM ELEVATION(FEET) = 152.75  
 ELEVATION DIFFERENCE(FEET) = 0.25  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.14  
 TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.14

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 106.00 IS CODE = 62  
 -----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<<

=====

UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26  
 STREET LENGTH(FEET) = 82.00 CURB HEIGHT(INCHES) = 8.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.35  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.20  
 HALFSTREET FLOOD WIDTH(FEET) = 2.00  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.33  
 STREET FLOW TRAVEL TIME(MIN.) = 0.81 Tc(MIN.) = 5.81  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.066

\*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 SOIL CLASSIFICATION IS "D"  
 S. C. S. CURVE NUMBER (AMC II) = 88  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.760  
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.43  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.56

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 4.78  
 FLOW VELOCITY(FEET/SEC.) = 1.40 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.35  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 127.00 FEET.



# P10R. RES

```
*****
FLOW PROCESS FROM NODE      106.00 TO NODE      106.00 IS CODE =   1
-----
```

```
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
```

```
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =   5.81
RAINFALL INTENSITY(INCH/HR) =   4.07
TOTAL STREAM AREA(ACRES) =   0.18
PEAK FLOW RATE(CFS) AT CONFLUENCE =   0.56
```

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.68	6.23	3.888	0.55
2	0.56	5.81	4.066	0.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.17	5.81	4.066
2	2.22	6.23	3.888

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) =   2.22   Tc(MIN.) =   6.23
TOTAL AREA(ACRES) =   0.7
LONGEST FLOWPATH FROM NODE      200.00 TO NODE      106.00 =   283.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE      106.00 TO NODE      107.00 IS CODE =  31
-----
```

```
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) =  148.00 DOWNSTREAM(FEET) =  147.50
FLOW LENGTH(FEET) =   16.00 MANNING'S N =  0.013
DEPTH OF FLOW IN   9.0 INCH PIPE IS   6.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   6.99
ESTIMATED PIPE DIAMETER(INCH) =   9.00   NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =   2.22
PIPE TRAVEL TIME(MIN.) =   0.04   Tc(MIN.) =   6.27
LONGEST FLOWPATH FROM NODE      200.00 TO NODE      107.00 =   299.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE      107.00 TO NODE      107.00 IS CODE =  10
-----
```

```
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====
```

```
*****
FLOW PROCESS FROM NODE      500.00 TO NODE      501.00 IS CODE =  21
-----
```

```
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
```

```
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) = 79
INITIAL SUBAREA FLOW-LENGTH(FEET) =   57.00
```

```

                                P10R. RES
UPSTREAM ELEVATION( FEET) =    156.10
DOWNSTREAM ELEVATION( FEET) =    153.90
ELEVATION DIFFERENCE( FEET) =      2.20
SUBAREA OVERLAND TIME OF FLOW( MIN. ) =    2.946
  10 YEAR RAINFALL INTENSITY( INCH/ HOUR) =    4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF( CFS) =      0.19
TOTAL AREA( ACRES) =      0.05    TOTAL RUNOFF( CFS) =      0.19

*****
FLOW PROCESS FROM NODE    501.00 TO NODE    502.00 IS CODE =   91
-----
>>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<
=====
UPSTREAM NODE ELEVATION( FEET) =    153.90
DOWNSTREAM NODE ELEVATION( FEET) =    153.00
CHANNEL LENGTH THRU SUBAREA( FEET) =    58.00
"V" GUTTER WIDTH( FEET) =    3.00    GUTTER HIKE( FEET) =    0.050
PAVEMENT LIP( FEET) =    0.030    MANNING' S N =    .0150
PAVEMENT CROSSFALL( DECIMAL NOTATION) =    0.03500
MAXIMUM DEPTH( FEET) =    0.20
  10 YEAR RAINFALL INTENSITY( INCH/ HOUR) =    4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED( GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) =    79
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) =      0.42
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/ SEC. ) =    2.03
AVERAGE FLOW DEPTH( FEET) =    0.09    FLOOD WIDTH( FEET) =    3.70
"V" GUTTER FLOW TRAVEL TIME( MIN. ) =    0.48    Tc( MIN. ) =    3.42
SUBAREA AREA( ACRES) =    0.14    SUBAREA RUNOFF( CFS) =    0.46
AREA-AVERAGE RUNOFF COEFFICIENT =    0.760
TOTAL AREA( ACRES) =      0.2    PEAK FLOW RATE( CFS) =      0.65

END OF SUBAREA "V" GUTTER HYDRAULICS:
DEPTH( FEET) =    0.11    FLOOD WIDTH( FEET) =    4.88
FLOW VELOCITY( FEET/ SEC. ) =    2.20    DEPTH*VELOCITY( FT*FT/ SEC) =    0.25
LONGEST FLOWPATH FROM NODE    500.00 TO NODE    502.00 =    115.00 FEET.

*****
FLOW PROCESS FROM NODE    502.00 TO NODE    503.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) =    151.10    DOWNSTREAM( FEET) =    150.70
FLOW LENGTH( FEET) =    67.00    MANNING' S N =    0.013
DEPTH OF FLOW IN    9.0 INCH PIPE IS    4.7 INCHES
PIPE-FLOW VELOCITY( FEET/ SEC. ) =    2.79
ESTIMATED PIPE DIAMETER( INCH) =    9.00    NUMBER OF PIPES =    1
PIPE-FLOW( CFS) =      0.65
PIPE TRAVEL TIME( MIN. ) =    0.40    Tc( MIN. ) =    3.82
LONGEST FLOWPATH FROM NODE    500.00 TO NODE    503.00 =    182.00 FEET.

*****
FLOW PROCESS FROM NODE    503.00 TO NODE    503.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
  10 YEAR RAINFALL INTENSITY( INCH/ HOUR) =    4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED( GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600

```

P10R. RES

S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.09  
 TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.73  
 TC(MIN.) = 3.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 503.00 TO NODE 504.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 150.70 DOWNSTREAM(FEET) = 150.50  
 FLOW LENGTH(FEET) = 36.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.80  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.73  
 PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 4.04  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 504.00 = 218.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.24  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 0.97  
 TC(MIN.) = 4.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.19  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.16  
 TC(MIN.) = 4.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 504.00 TO NODE 505.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 150.50 DOWNSTREAM(FEET) = 150.20  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.00  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.16

```

                                P10R. RES
PIPE TRAVEL TIME(MIN.) = 0.31    Tc(MIN.) = 4.34
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 505.00 = 273.00 FEET.
*****
FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.26
TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.41
TC(MIN.) = 4.34
*****
FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.10
TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 1.51
TC(MIN.) = 4.34
*****
FLOW PROCESS FROM NODE 505.00 TO NODE 506.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 150.20 DOWNSTREAM( FEET) = 149.30
FLOW LENGTH( FEET) = 85.00 MANNING' S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.9 INCHES
PIPE-FLOW VELOCITY( FEET/SEC. ) = 4.15
ESTIMATED PIPE DIAMETER( INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.51
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 4.68
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 506.00 = 358.00 FEET.
*****
FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 4.68
RAINFALL INTENSITY(INCH/HR) = 4.48
TOTAL STREAM AREA(ACRES) = 0.45
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.51
*****
FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21
-----

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                                P10R. RES
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00
UPSTREAM ELEVATION(FEET) = 153.00
DOWNSTREAM ELEVATION(FEET) = 152.75
ELEVATION DIFFERENCE(FEET) = 0.25
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.22
TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.22

*****
FLOW PROCESS FROM NODE 601.00 TO NODE 506.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26
STREET LENGTH(FEET) = 81.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.43
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 3.34
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.45
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.32
STREET FLOW TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 5.92
10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.016
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.760
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.61

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 5.16
FLOW VELOCITY(FEET/SEC.) = 1.42 DEPTH*VELOCITY(FT*FT/SEC.) = 0.36
LONGEST FLOWPATH FROM NODE 600.00 TO NODE 506.00 = 126.00 FEET.

*****
FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.92

```

P10R. RES  
 RAINFALL INTENSITY(INCH/HR) = 4.02  
 TOTAL STREAM AREA(ACRES) = 0.20  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.61

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.51	4.68	4.479	0.45
2	0.61	5.92	4.016	0.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.00	4.68	4.479
2	1.97	5.92	4.016

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.00 Tc(MIN.) = 4.68  
 TOTAL AREA(ACRES) = 0.6  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 506.00 = 358.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 506.00 TO NODE 507.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 148.00 DOWNSTREAM(FEET) = 147.50  
 FLOW LENGTH(FEET) = 16.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.83  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.00  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 4.72  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 507.00 = 374.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 507.00 TO NODE 107.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.00	4.72	4.479	0.65

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 107.00 = 374.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.22	6.27	3.872	0.73

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 299.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.67	4.72	4.479
2	3.94	6.27	3.872

P10R. RES

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 3.94  $T_c$ (MIN.) = 6.27  
 TOTAL AREA(ACRES) = 1.4

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 147.50 DOWNSTREAM(FEET) = 146.40  
 FLOW LENGTH(FEET) = 97.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.57  
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.94  
 PIPE TRAVEL TIME(MIN.) = 0.29  $T_c$ (MIN.) = 6.56  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 108.00 = 471.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.56  
 RAINFALL INTENSITY(INCH/HR) = 3.76  
 TOTAL STREAM AREA(ACRES) = 1.38  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.94

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
 UPSTREAM ELEVATION(FEET) = 152.40  
 DOWNSTREAM ELEVATION(FEET) = 151.70  
 ELEVATION DIFFERENCE(FEET) = 0.70  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.971  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
           THE MAXIMUM OVERLAND FLOW LENGTH = 63.00  
           (Reference: Table 3-1B of Hydrology Manual)  
           THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN  $T_c$  CALCULATION!  
 10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479  
 NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.10  
 TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.10

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 701.00 TO NODE 701.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

10 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.479  
 NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79

P10R. RES

AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.22  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.32  
 TC(MIN.) = 4.97

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM( FEET) = 150.60 DOWNSTREAM( FEET) = 150.18  
 FLOW LENGTH( FEET) = 90.00 MANNING' S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.4 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 2.10  
 ESTIMATED PIPE DIAMETER( INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS) = 0.32  
 PIPE TRAVEL TIME( MIN.) = 0.71 Tc( MIN.) = 5.68  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 165.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 702.00 TO NODE 702.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====  
 10 YEAR RAINFALL INTENSITY( INCH/HOUR) = 4.123  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.17  
 TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.47  
 TC(MIN.) = 5.68

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 702.00 TO NODE 703.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM( FEET) = 150.18 DOWNSTREAM( FEET) = 149.90  
 FLOW LENGTH( FEET) = 55.00 MANNING' S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.1 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 2.42  
 ESTIMATED PIPE DIAMETER( INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS) = 0.47  
 PIPE TRAVEL TIME( MIN.) = 0.38 Tc( MIN.) = 6.06  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 703.00 = 220.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 703.00 TO NODE 704.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM( FEET) = 148.60 DOWNSTREAM( FEET) = 147.13  
 FLOW LENGTH( FEET) = 14.00 MANNING' S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.1 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 7.45  
 ESTIMATED PIPE DIAMETER( INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS) = 0.47  
 PIPE TRAVEL TIME( MIN.) = 0.03 Tc( MIN.) = 6.10  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 704.00 = 234.00 FEET.



# P10R. RES

```
*****
FLOW PROCESS FROM NODE      704.00 TO NODE      704.00 IS CODE =   81
-----
```

```
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
```

```
10 YEAR RAINFALL INTENSITY(INCH/HOUR) =   3.942
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) =   79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) =      0.16  SUBAREA RUNOFF(CFS) =      0.46
TOTAL AREA(ACRES) =      0.3    TOTAL RUNOFF(CFS) =      0.91
TC(MIN. ) =      6.10
```

```
*****
FLOW PROCESS FROM NODE      704.00 TO NODE      705.00 IS CODE =   31
-----
```

```
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) =  147.13  DOWNSTREAM(FEET) =  146.40
FLOW LENGTH(FEET) =   12.00  MANNING'S N =  0.013
DEPTH OF FLOW IN   6.0 INCH PIPE IS   3.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC. ) =   7.20
ESTIMATED PIPE DIAMETER(INCH) =   6.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      0.91
PIPE TRAVEL TIME(MIN. ) =   0.03  Tc(MIN. ) =   6.12
LONGEST FLOWPATH FROM NODE      700.00 TO NODE      705.00 =      246.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE      705.00 TO NODE      705.00 IS CODE =    1
-----
```

```
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
```

```
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN. ) =   6.12
RAINFALL INTENSITY(INCH/HR) =   3.93
TOTAL STREAM AREA(ACRES) =   0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE =      0.91
```

```
*****
FLOW PROCESS FROM NODE      800.00 TO NODE      801.00 IS CODE =   21
-----
```

```
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
```

```
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) =   79
INITIAL SUBAREA FLOW-LENGTH(FEET) =   75.00
UPSTREAM ELEVATION(FEET) =   152.40
DOWNSTREAM ELEVATION(FEET) =   151.70
ELEVATION DIFFERENCE(FEET) =    0.70
SUBAREA OVERLAND TIME OF FLOW(MIN. ) =   4.971
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH =   63.00
         (Reference: Table 3-1B of Hydrology Manual )
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
10 YEAR RAINFALL INTENSITY(INCH/HOUR) =   4.479
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =      0.10
TOTAL AREA(ACRES) =      0.03  TOTAL RUNOFF(CFS) =      0.10
```

P10R. RES

```

*****
FLOW PROCESS FROM NODE      801.00 TO NODE      801.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.479
    NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    S. C. S. CURVE NUMBER (AMC II) = 79
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) =      0.05  SUBAREA RUNOFF(CFS) =      0.19
    TOTAL AREA(ACRES) =      0.1  TOTAL RUNOFF(CFS) =      0.29
    TC(MIN. ) =      4.97

*****
FLOW PROCESS FROM NODE      801.00 TO NODE      802.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
    ELEVATION DATA: UPSTREAM(FEET) = 150.60  DOWNSTREAM(FEET) = 150.15
    FLOW LENGTH(FEET) = 90.00  MANNING'S N = 0.013
    DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.9 INCHES
    PIPE-FLOW VELOCITY(FEET/SEC.) = 2.14
    ESTIMATED PIPE DIAMETER(INCH) = 6.00  NUMBER OF PIPES = 1
    PIPE-FLOW(CFS) = 0.29
    PIPE TRAVEL TIME(MIN. ) = 0.70  Tc(MIN. ) = 5.67
    LONGEST FLOWPATH FROM NODE 800.00 TO NODE 802.00 = 165.00 FEET.

*****
FLOW PROCESS FROM NODE      802.00 TO NODE      802.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
    10 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.130
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    S. C. S. CURVE NUMBER (AMC II) = 79
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) =      0.06  SUBAREA RUNOFF(CFS) =      0.20
    TOTAL AREA(ACRES) =      0.2  TOTAL RUNOFF(CFS) =      0.47
    TC(MIN. ) =      5.67

*****
FLOW PROCESS FROM NODE      802.00 TO NODE      803.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
    ELEVATION DATA: UPSTREAM(FEET) = 150.15  DOWNSTREAM(FEET) = 149.90
    FLOW LENGTH(FEET) = 55.00  MANNING'S N = 0.013
    DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.2 INCHES
    PIPE-FLOW VELOCITY(FEET/SEC.) = 2.33
    ESTIMATED PIPE DIAMETER(INCH) = 9.00  NUMBER OF PIPES = 1
    PIPE-FLOW(CFS) = 0.47
    PIPE TRAVEL TIME(MIN. ) = 0.39  Tc(MIN. ) = 6.06
    LONGEST FLOWPATH FROM NODE 800.00 TO NODE 803.00 = 220.00 FEET.

*****
FLOW PROCESS FROM NODE      803.00 TO NODE      804.00 IS CODE =  31
-----

```

# P10R. RES

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM( FEET ) = 148.60 DOWNSTREAM( FEET ) = 147.13  
FLOW LENGTH( FEET ) = 14.00 MANNING' S N = 0.013  
DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.1 INCHES  
PIPE-FLOW VELOCITY( FEET/SEC. ) = 7.46  
ESTIMATED PIPE DIAMETER( INCH ) = 6.00 NUMBER OF PIPES = 1  
PIPE-FLOW( CFS ) = 0.47  
PIPE TRAVEL TIME( MIN. ) = 0.03 Tc( MIN. ) = 6.10  
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 804.00 = 234.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 804.00 TO NODE 804.00 IS CODE = 81

>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

10 YEAR RAINFALL INTENSITY( INCH/HOUR ) = 3.942  
\*USER SPECIFIED( GLOBAL ):  
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
S. C. S. CURVE NUMBER ( AMC II ) = 79  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
SUBAREA AREA( ACRES ) = 0.16 SUBAREA RUNOFF( CFS ) = 0.46  
TOTAL AREA( ACRES ) = 0.3 TOTAL RUNOFF( CFS ) = 0.91  
Tc( MIN. ) = 6.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 804.00 TO NODE 805.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM( FEET ) = 147.13 DOWNSTREAM( FEET ) = 146.40  
FLOW LENGTH( FEET ) = 12.00 MANNING' S N = 0.013  
DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.7 INCHES  
PIPE-FLOW VELOCITY( FEET/SEC. ) = 7.20  
ESTIMATED PIPE DIAMETER( INCH ) = 6.00 NUMBER OF PIPES = 1  
PIPE-FLOW( CFS ) = 0.91  
PIPE TRAVEL TIME( MIN. ) = 0.03 Tc( MIN. ) = 6.12  
LONGEST FLOWPATH FROM NODE 800.00 TO NODE 805.00 = 246.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 805.00 TO NODE 705.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION( MIN. ) = 6.12  
RAINFALL INTENSITY( INCH/HR ) = 3.93  
TOTAL STREAM AREA( ACRES ) = 0.31  
PEAK FLOW RATE( CFS ) AT CONFLUENCE = 0.91

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF ( CFS )	Tc ( MIN. )	INTENSITY ( INCH/HOUR )	AREA ( ACRE )
1	3.94	6.56	3.761	1.38
2	0.91	6.12	3.930	0.31
3	0.91	6.12	3.930	0.31

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

P10R. RES

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.51	6.12	3.930
2	5.51	6.12	3.930
3	5.69	6.56	3.761

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.69 Tc(MIN.) = 6.56

TOTAL AREA(ACRES) = 2.0

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 705.00 = 471.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 2.0 TC(MIN.) = 6.56

PEAK FLOW RATE(CFS) = 5.69

=====

END OF RATIONAL METHOD ANALYSIS

♀

\*\*\*\*\*

## RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003, 1985, 1981 HYDROLOGY MANUAL

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Ver. 17.5 Release Date: 07/05/2012 License ID 1463

Analysis prepared by:

Buccola Engineering, Inc.  
3142 Vista Way, Suite 301  
Oceanside, CA 92056  
(760) 721-2000

## \*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Sandpiper Villa - Preliminary Hydrology Report \*  
\* Post-Development Condition Rational Method for 100-Year Storm Event \*  
\*

\*\*\*\*\*

FILE NAME: G:\1664\P100.DAT

TIME/DATE OF STUDY: 16:08 01/12/2017

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

## 2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 2.700

SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SPECIFIED CONSTANT RUNOFF COEFFICIENT = 0.760

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-CROWN TO STREET-CROSSFALL:		IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING HIKE FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)			WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

## GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600

SOIL CLASSIFICATION IS "D"

S. C. S. CURVE NUMBER (AMC II) = 88

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 153.10

DOWNSTREAM ELEVATION(FEET) = 152.50

ELEVATION DIFFERENCE(FEET) = 0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.741

P100R. RES

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.32  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.32

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 151.80 DOWNSTREAM(FEET) = 151.56  
 FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 3.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.48  
 ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.32  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 4.98  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 95.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 SOIL CLASSIFICATION IS "D"  
 S. C. S. CURVE NUMBER (AMC II) = 88  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.43  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.76  
 TC(MIN.) = 4.98

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 151.56 DOWNSTREAM(FEET) = 151.38  
 FLOW LENGTH(FEET) = 28.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.98  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.76  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.13  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 123.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.995  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 SOIL CLASSIFICATION IS "D"  
 S. C. S. CURVE NUMBER (AMC II) = 88  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.80

```

                                P100R. RES
TOTAL AREA(ACRES) =          0.3  TOTAL RUNOFF(CFS) =          1.54
TC(MIN. ) =          5.13

*****
FLOW PROCESS FROM NODE      103.00 TO NODE      104.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   151.38  DOWNSTREAM(FEET) =   150.81
FLOW LENGTH(FEET) =    48.00  MANNING'S N =   0.013
DEPTH OF FLOW IN    9.0 INCH PIPE IS    6.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    4.38
ESTIMATED PIPE DIAMETER(INCH) =    9.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =          1.54
PIPE TRAVEL TIME(MIN. ) =    0.18  Tc(MIN. ) =    5.32
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    104.00 =    171.00 FEET.

*****
FLOW PROCESS FROM NODE      104.00 TO NODE      104.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HR) =   6.839
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) =   88
AREA-AVERAGE RUNOFF COEFFICIENT =   0.7600
SUBAREA AREA(ACRES) =    0.03  SUBAREA RUNOFF(CFS) =    0.16
TOTAL AREA(ACRES) =    0.3  TOTAL RUNOFF(CFS) =    1.66
TC(MIN. ) =    5.32

*****
FLOW PROCESS FROM NODE      104.00 TO NODE      105.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   150.81  DOWNSTREAM(FEET) =   149.90
FLOW LENGTH(FEET) =    45.00  MANNING'S N =   0.013
DEPTH OF FLOW IN    9.0 INCH PIPE IS    5.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    5.53
ESTIMATED PIPE DIAMETER(INCH) =    9.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =          1.66
PIPE TRAVEL TIME(MIN. ) =    0.14  Tc(MIN. ) =    5.45
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    105.00 =    216.00 FEET.

*****
FLOW PROCESS FROM NODE      105.00 TO NODE      105.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN. ) =    5.45
RAINFALL INTENSITY(INCH/HR) =    6.73
TOTAL STREAM AREA(ACRES) =    0.32
PEAK FLOW RATE(CFS) AT CONFLUENCE =    1.66

*****
FLOW PROCESS FROM NODE      200.00 TO NODE      201.00 IS CODE =   21
-----

```

P100R.RES

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S.C.S. CURVE NUMBER (AMC II) = 88
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 153.10
DOWNSTREAM ELEVATION(FEET) = 152.20
ELEVATION DIFFERENCE(FEET) = 0.90
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.934
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16
```

```
*****
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
-----
```

```
ELEVATION DATA: UPSTREAM(FEET) = 151.20 DOWNSTREAM(FEET) = 150.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.11
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.16
PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 5.37
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 145.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
```

```
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
```

```
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.795
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S.C.S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.31
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.46
TC(MIN.) = 5.37
```

```
*****
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81
-----
```

```
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
```

```
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.795
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S.C.S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.04 SUBAREA RUNOFF(CFS) = 0.21
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.67
```



TC(MIN. ) = 5.37

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	150.80	DOWNSTREAM(FEET) =	150.25
FLOW LENGTH(FEET) =	55.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	4.1 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	3.41		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.67		
PIPE TRAVEL TIME(MIN. ) =	0.27	Tc(MIN. ) =	5.64
LONGEST FLOWPATH FROM NODE	200.00 TO NODE	203.00 =	200.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.584
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS "D"	
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.07 SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) =	0.2 TOTAL RUNOFF(CFS) = 1.00
TC(MIN. ) =	5.64

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.584
*USER SPECIFIED(GLOBAL):	
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT =	.7600
SOIL CLASSIFICATION IS "D"	
S. C. S. CURVE NUMBER (AMC II) =	88
AREA-AVERAGE RUNOFF COEFFICIENT =	0.7600
SUBAREA AREA(ACRES) =	0.03 SUBAREA RUNOFF(CFS) = 0.15
TOTAL AREA(ACRES) =	0.2 TOTAL RUNOFF(CFS) = 1.15
TC(MIN. ) =	5.64

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 105.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	150.25	DOWNSTREAM(FEET) =	149.90
FLOW LENGTH(FEET) =	35.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	9.0 INCH PIPE IS	5.7 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	3.87		
ESTIMATED PIPE DIAMETER(INCH) =	9.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	1.15		
PIPE TRAVEL TIME(MIN. ) =	0.15	Tc(MIN. ) =	5.79
LONGEST FLOWPATH FROM NODE	200.00 TO NODE	105.00 =	235.00 FEET.

\*\*\*\*\*  
 Page 5

P100R. RES  
FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.79  
RAINFALL INTENSITY(INCH/HR) = 6.47  
TOTAL STREAM AREA(ACRES) = 0.23  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.15

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.66	5.45	6.728	0.32
2	1.15	5.79	6.473	0.23

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN.)	INTENSITY (INCH/HOUR)
1	2.75	5.45	6.728
2	2.75	5.79	6.473

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.75 T<sub>c</sub>(MIN.) = 5.79  
TOTAL AREA(ACRES) = 0.6  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 105.00 = 235.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 149.90 DOWNSTREAM(FEET) = 149.30  
FLOW LENGTH(FEET) = 48.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.25  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.75  
PIPE TRAVEL TIME(MIN.) = 0.15 T<sub>c</sub>(MIN.) = 5.94  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 106.00 = 283.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.94  
RAINFALL INTENSITY(INCH/HR) = 6.37  
TOTAL STREAM AREA(ACRES) = 0.55  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<

P100R. RES

```
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00
UPSTREAM ELEVATION(FEET) = 153.00
DOWNSTREAM ELEVATION(FEET) = 152.75
ELEVATION DIFFERENCE(FEET) = 0.25
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.22
TOTAL AREA(ACRES) = 0.04 TOTAL RUNOFF(CFS) = 0.22
=====
```

```
*****
FLOW PROCESS FROM NODE 301.00 TO NODE 106.00 IS CODE = 62
=====
```

```
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
```

```
UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26
STREET LENGTH(FEET) = 82.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00
```

```
DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018
```

```
SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200
```

```
*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.25
HALFSTREET FLOOD WIDTH(FEET) = 4.72
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.41
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.35
STREET FLOW TRAVEL TIME(MIN.) = 0.97 Tc(MIN.) = 5.96
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.350
```

```
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
SOIL CLASSIFICATION IS "D"
S. C. S. CURVE NUMBER (AMC II) = 88
AREA-AVERAGE RUNOFF COEFFICIENT = 0.760
SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.68
TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.87
```

```
END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 6.66
FLOW VELOCITY(FEET/SEC.) = 1.47 DEPTH*VELOCITY(FT*FT/SEC.) = 0.41
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 127.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1
=====
```

```
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
```

```
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
```

P100R. RES  
 TIME OF CONCENTRATION(MIN. ) = 5.96  
 RAINFALL INTENSITY(INCH/HR) = 6.35  
 TOTAL STREAM AREA(ACRES) = 0.18  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.87

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN. )	INTENSITY (INCH/HR)	AREA (ACRE)
1	2.75	5.94	6.366	0.55
2	0.87	5.96	6.350	0.18

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	T <sub>c</sub> (MIN. )	INTENSITY (INCH/HR)
1	3.62	5.94	6.366
2	3.61	5.96	6.350

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.62 T<sub>c</sub>(MIN. ) = 5.94  
 TOTAL AREA(ACRES) = 0.7  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 106.00 = 283.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 148.00 DOWNSTREAM(FEET) = 147.50  
 FLOW LENGTH(FEET) = 16.00 MANNING' S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC. ) = 7.97  
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.62  
 PIPE TRAVEL TIME(MIN. ) = 0.03 T<sub>c</sub>(MIN. ) = 5.97  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 299.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 57.00  
 UPSTREAM ELEVATION(FEET) = 156.10  
 DOWNSTREAM ELEVATION(FEET) = 153.90  
 ELEVATION DIFFERENCE(FEET) = 2.20  
 SUBAREA OVERLAND TIME OF FLOW(MIN. ) = 2.946  
 100 YEAR RAINFALL INTENSITY(INCH/HR) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON T<sub>c</sub> = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.05 TOTAL RUNOFF(CFS) = 0.30

P100R.RES

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION( FEET ) = 153.90  
 DOWNSTREAM NODE ELEVATION( FEET ) = 153.00  
 CHANNEL LENGTH THRU SUBAREA( FEET ) = 58.00  
 "V" GUTTER WIDTH( FEET ) = 3.00 GUTTER HIKE( FEET ) = 0.050  
 PAVEMENT LIP( FEET ) = 0.030 MANNING' S N = .0150  
 PAVEMENT CROSSFALL( DECIMAL NOTATION ) = 0.03500  
 MAXIMUM DEPTH( FEET ) = 0.20  
 100 YEAR RAINFALL INTENSITY( INCH/ HOUR ) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED( GLOBAL ):  
 RESIDENTIAL ( 10.9 DU/ AC OR LESS ) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER ( AMC II ) = 79  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS ) = 0.66  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/ SEC. ) = 2.25  
 AVERAGE FLOW DEPTH( FEET ) = 0.11 FLOOD WIDTH( FEET ) = 4.88  
 "V" GUTTER FLOW TRAVEL TIME( MIN. ) = 0.43 Tc( MIN. ) = 3.38  
 SUBAREA AREA( ACRES ) = 0.14 SUBAREA RUNOFF( CFS ) = 0.73  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.760  
 TOTAL AREA( ACRES ) = 0.2 PEAK FLOW RATE( CFS ) = 1.03

END OF SUBAREA "V" GUTTER HYDRAULICS:  
 DEPTH( FEET ) = 0.14 FLOOD WIDTH( FEET ) = 6.16  
 FLOW VELOCITY( FEET/ SEC. ) = 2.46 DEPTH\*VELOCITY( FT\*FT/ SEC ) = 0.33  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 115.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE ( NON-PRESSURE FLOW )<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET ) = 151.10 DOWNSTREAM( FEET ) = 150.70  
 FLOW LENGTH( FEET ) = 67.00 MANNING' S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 6.4 INCHES  
 PIPE-FLOW VELOCITY( FEET/ SEC. ) = 3.07  
 ESTIMATED PIPE DIAMETER( INCH ) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS ) = 1.03  
 PIPE TRAVEL TIME( MIN. ) = 0.36 Tc( MIN. ) = 3.74  
 LONGEST FLOWPATH FROM NODE 500.00 TO NODE 503.00 = 182.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 503.00 TO NODE 503.00 IS CODE = 81

>>>>ADDIT ION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY( INCH/ HOUR ) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED( GLOBAL ):  
 RESIDENTIAL ( 10.9 DU/ AC OR LESS ) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER ( AMC II ) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA( ACRES ) = 0.03 SUBAREA RUNOFF( CFS ) = 0.14  
 TOTAL AREA( ACRES ) = 0.2 TOTAL RUNOFF( CFS ) = 1.16  
 TC( MIN. ) = 3.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 503.00 TO NODE 504.00 IS CODE = 31

P100R. RES

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-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.70 DOWNSTREAM(FEET) = 150.50
FLOW LENGTH(FEET) = 36.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.02
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.16
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 3.94
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 504.00 = 218.00 FEET.

*****
FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.07 SUBAREA RUNOFF(CFS) = 0.38
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.54
TC(MIN.) = 3.94

*****
FLOW PROCESS FROM NODE 504.00 TO NODE 504.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.30
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.84
TC(MIN.) = 3.94

*****
FLOW PROCESS FROM NODE 504.00 TO NODE 505.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.50 DOWNSTREAM(FEET) = 150.20
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.48
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.84
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 4.20
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 505.00 = 273.00 FEET.

*****
FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

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                                P100R. RES
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
    NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    S. C. S. CURVE NUMBER (AMC II) = 79
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) = 0.08 SUBAREA RUNOFF(CFS) = 0.41
    TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 2.24
    TC(MIN.) = 4.20

*****
    FLOW PROCESS FROM NODE 505.00 TO NODE 505.00 IS CODE = 81
    -----
    >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
    -----
    100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
    NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    S. C. S. CURVE NUMBER (AMC II) = 79
    AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
    SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.16
    TOTAL AREA(ACRES) = 0.4 TOTAL RUNOFF(CFS) = 2.41
    TC(MIN.) = 4.20

*****
    FLOW PROCESS FROM NODE 505.00 TO NODE 506.00 IS CODE = 31
    -----
    >>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
    >>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
    -----
    ELEVATION DATA: UPSTREAM(FEET) = 150.20 DOWNSTREAM(FEET) = 149.30
    FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013
    DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.3 INCHES
    PIPE-FLOW VELOCITY(FEET/SEC.) = 4.78
    ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
    PIPE-FLOW(CFS) = 2.41
    PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 4.50
    LONGEST FLOWPATH FROM NODE 500.00 TO NODE 506.00 = 358.00 FEET.

*****
    FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 1
    -----
    >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
    -----
    TOTAL NUMBER OF STREAMS = 2
    CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
    TIME OF CONCENTRATION(MIN.) = 4.50
    RAINFALL INTENSITY(INCH/HR) = 7.11
    TOTAL STREAM AREA(ACRES) = 0.45
    PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.41

*****
    FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21
    -----
    >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
    -----
    *USER SPECIFIED(GLOBAL):
    RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
    S. C. S. CURVE NUMBER (AMC II) = 79
    INITIAL SUBAREA FLOW-LENGTH(FEET) = 45.00
    UPSTREAM ELEVATION(FEET) = 153.00
    DOWNSTREAM ELEVATION(FEET) = 152.75

```

P100R. RES  
 ELEVATION DIFFERENCE(FEET) = 0.25  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.994  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.35  
 TOTAL AREA(ACRES) = 0.06 TOTAL RUNOFF(CFS) = 0.35

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 601.00 TO NODE 506.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 152.75 DOWNSTREAM ELEVATION(FEET) = 152.26  
 STREET LENGTH(FEET) = 81.00 CURB HEIGHT(INCHES) = 8.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.68  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.26  
 HALFSTREET FLOOD WIDTH(FEET) = 5.59  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.43  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.38  
 STREET FLOW TRAVEL TIME(MIN.) = 0.94 Tc(MIN.) = 5.94  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.369  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.760  
 SUBAREA AREA(ACRES) = 0.14 SUBAREA RUNOFF(CFS) = 0.65  
 TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.97

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 7.09  
 FLOW VELOCITY(FEET/SEC.) = 1.51 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.44  
 LONGEST FLOWPATH FROM NODE 600.00 TO NODE 506.00 = 126.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.94  
 RAINFALL INTENSITY(INCH/HR) = 6.37  
 TOTAL STREAM AREA(ACRES) = 0.20  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.97

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.41	4.50	7.114	0.45



			P100R. RES	
2	0.97	5.94	6.369	0.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	3.14	4.50	7.114
2	3.12	5.94	6.369

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.14 Tc(MIN.) = 4.50  
TOTAL AREA(ACRES) = 0.6  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 506.00 = 358.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 506.00 TO NODE 507.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 148.00 DOWNSTREAM(FEET) = 147.50  
FLOW LENGTH(FEET) = 16.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.70  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 3.14  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 4.53  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 507.00 = 374.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 507.00 TO NODE 107.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.14	4.53	7.114	0.65

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 107.00 = 374.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.62	5.97	6.343	0.73

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 299.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	5.88	4.53	7.114
2	6.42	5.97	6.343

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.42 Tc(MIN.) = 5.97  
TOTAL AREA(ACRES) = 1.4

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

```

                                P100R.RES
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 147.50 DOWNSTREAM(FEET) = 146.40
FLOW LENGTH(FEET) = 97.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 12.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.06
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.42
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 6.24
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 108.00 = 471.00 FEET.

*****
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.24
RAINFALL INTENSITY(INCH/HR) = 6.17
TOTAL STREAM AREA(ACRES) = 1.38
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.42

*****
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 152.40
DOWNSTREAM ELEVATION(FEET) = 151.70
ELEVATION DIFFERENCE(FEET) = 0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.971
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 63.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16

*****
FLOW PROCESS FROM NODE 701.00 TO NODE 701.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S. C. S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.35
TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.51
TC(MIN.) = 4.97

*****
FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 31
-----

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                                P100R.RES
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.60 DOWNSTREAM(FEET) = 150.18
FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.39
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.51
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 5.60
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 165.00 FEET.

*****
FLOW PROCESS FROM NODE 702.00 TO NODE 702.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.615
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.28
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.75
Tc(MIN.) = 5.60

*****
FLOW PROCESS FROM NODE 702.00 TO NODE 703.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 150.18 DOWNSTREAM(FEET) = 149.90
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.73
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.75
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 5.93
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 703.00 = 220.00 FEET.

*****
FLOW PROCESS FROM NODE 703.00 TO NODE 704.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 147.13
FLOW LENGTH(FEET) = 14.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.50
ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.75
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.96
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 704.00 = 234.00 FEET.

*****
FLOW PROCESS FROM NODE 704.00 TO NODE 704.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.352
*USER SPECIFIED(GLOBAL):

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                                P100R.RES
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) = 79
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.75
TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.47
TC(MIN.) = 5.96
*****
FLOW PROCESS FROM NODE 704.00 TO NODE 705.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 147.13 DOWNSTREAM(FEET) = 146.40
FLOW LENGTH(FEET) = 12.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.18
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.47
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.98
LONGEST FLOWPATH FROM NODE 700.00 TO NODE 705.00 = 246.00 FEET.
*****
FLOW PROCESS FROM NODE 705.00 TO NODE 705.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.98
RAINFALL INTENSITY(INCH/HR) = 6.34
TOTAL STREAM AREA(ACRES) = 0.31
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.47
*****
FLOW PROCESS FROM NODE 800.00 TO NODE 801.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(GLOBAL):
RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600
S.C.S. CURVE NUMBER (AMC II) = 79
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00
UPSTREAM ELEVATION(FEET) = 152.40
DOWNSTREAM ELEVATION(FEET) = 151.70
ELEVATION DIFFERENCE(FEET) = 0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.971
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 63.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.03 TOTAL RUNOFF(CFS) = 0.16
*****
FLOW PROCESS FROM NODE 801.00 TO NODE 801.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.114
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

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P100R. RES

\*USER SPECIFIED(GLOBAL):

RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S.C.S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.05 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.1 TOTAL RUNOFF(CFS) = 0.46  
 TC(MIN.) = 4.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 801.00 TO NODE 802.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 150.60 DOWNSTREAM(FEET) = 150.15  
 FLOW LENGTH(FEET) = 90.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.39  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.46  
 PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 5.60  
 LONGEST FLOWPATH FROM NODE 800.00 TO NODE 802.00 = 165.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 802.00 TO NODE 802.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.614  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S.C.S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.33  
 TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.75  
 TC(MIN.) = 5.60

\*\*\*\*\*

FLOW PROCESS FROM NODE 802.00 TO NODE 803.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 150.15 DOWNSTREAM(FEET) = 149.90  
 FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 5.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.60  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.75  
 PIPE TRAVEL TIME(MIN.) = 0.35 Tc(MIN.) = 5.95  
 LONGEST FLOWPATH FROM NODE 800.00 TO NODE 803.00 = 220.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 803.00 TO NODE 804.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 147.13  
 FLOW LENGTH(FEET) = 14.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.50  
 ESTIMATED PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1

# P100R. RES

PIPE-FLOW(CFS) = 0.75  
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.98  
 LONGEST FLOWPATH FROM NODE 800.00 TO NODE 804.00 = 234.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 804.00 TO NODE 804.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.340  
 \*USER SPECIFIED(GLOBAL):  
 RESIDENTIAL (10.9 DU/AC OR LESS) RUNOFF COEFFICIENT = .7600  
 S. C. S. CURVE NUMBER (AMC II) = 79  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7600  
 SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.75  
 TOTAL AREA(ACRES) = 0.3 TOTAL RUNOFF(CFS) = 1.47  
 TC(MIN.) = 5.98

\*\*\*\*\*

FLOW PROCESS FROM NODE 804.00 TO NODE 805.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 147.13 DOWNSTREAM(FEET) = 146.40  
 FLOW LENGTH(FEET) = 12.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 3.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.17  
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.47  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 6.00  
 LONGEST FLOWPATH FROM NODE 800.00 TO NODE 805.00 = 246.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 805.00 TO NODE 705.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.00  
 RAINFALL INTENSITY(INCH/HR) = 6.32  
 TOTAL STREAM AREA(ACRES) = 0.31  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.47

## \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.42	6.24	6.167	1.38
2	1.47	5.98	6.335	0.31
3	1.47	6.00	6.323	0.31

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

## \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	9.09	5.98	6.335
2	9.11	6.00	6.323
3	9.28	6.24	6.167

P100R.RES

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =	9.28	Tc(MIN. ) =	6.24
TOTAL AREA(ACRES) =	2.0		
LONGEST FLOWPATH FROM NODE	500.00	TO NODE	705.00 = 471.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	2.0	Tc(MIN. ) =	6.24
PEAK FLOW RATE(CFS)	=	9.28		

=====

=====

END OF RATIONAL METHOD ANALYSIS

=====

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## A - 8

**“Technical Memorandum: Determination for Pre- and Post- Developed 100-year Peak Flow” for: Sandpiper Villa, prepared by: “Tory R. Walker Engineering”, Revision dated: September 13, 2019**



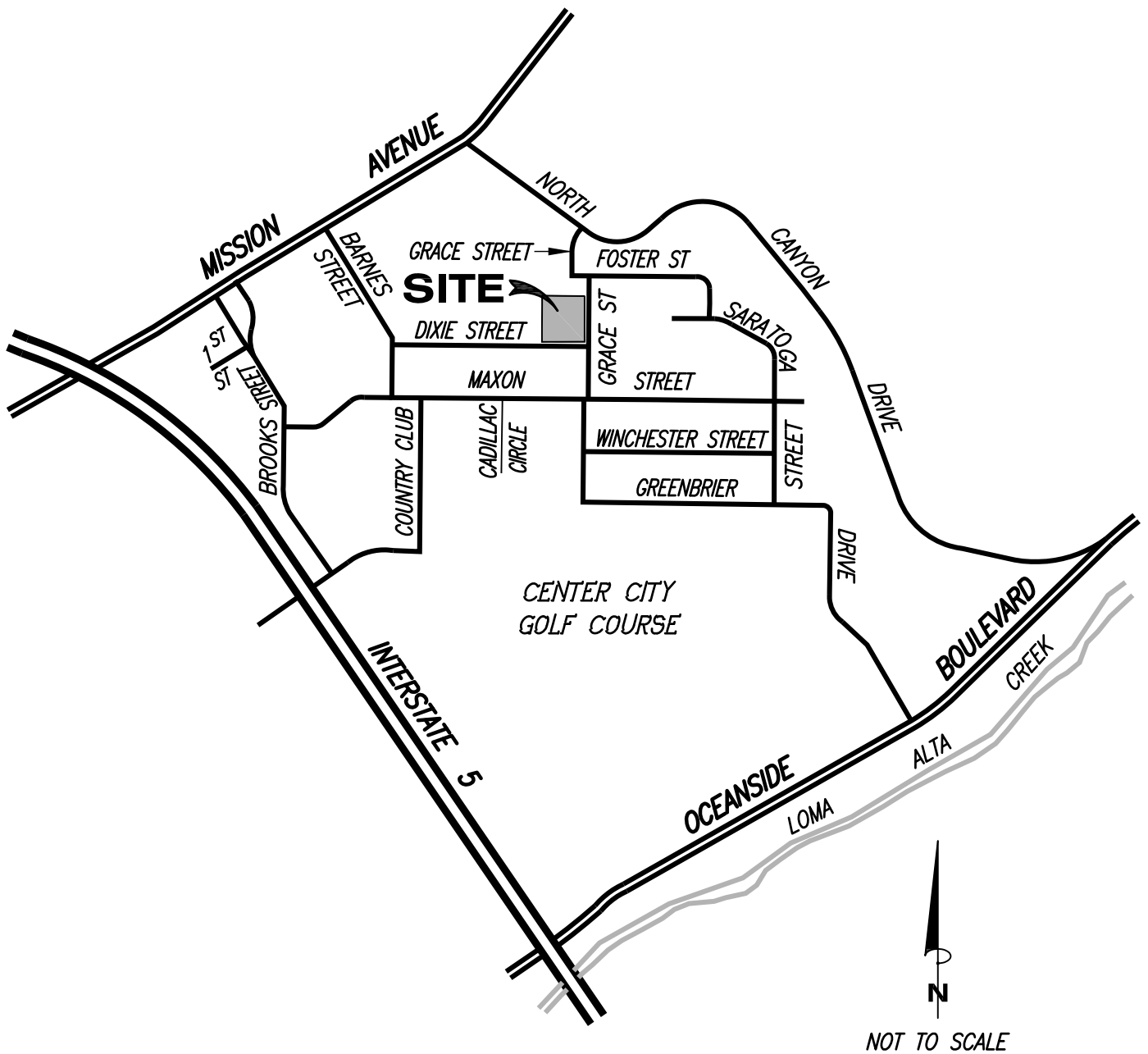
**SECTION 5.0**  
**FIGURES AND EXHIBITS**

Figure

1. Vicinity Map

Exhibits

- Exhibit A – Existing-Condition Hydrology Map
- Exhibit B – Proposed-Condition Hydrology Map



**PRELIMINARY HYDROLOGY REPORT**

**FOR**

**SANDPIPER VILLA  
(ZA15-00007, D15-00014, CUP16-00005)**

PREPARED IN THE OFFICE OF:

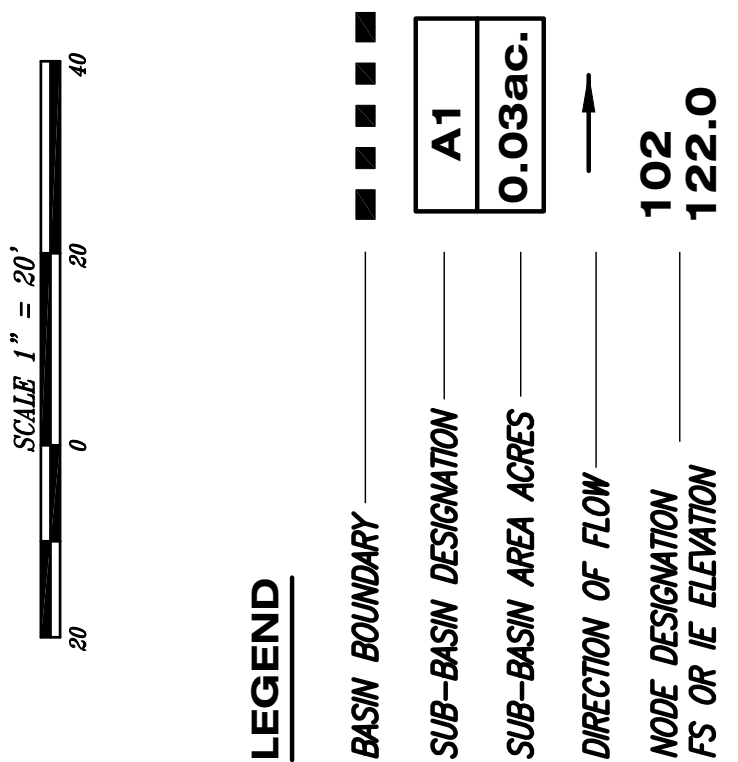
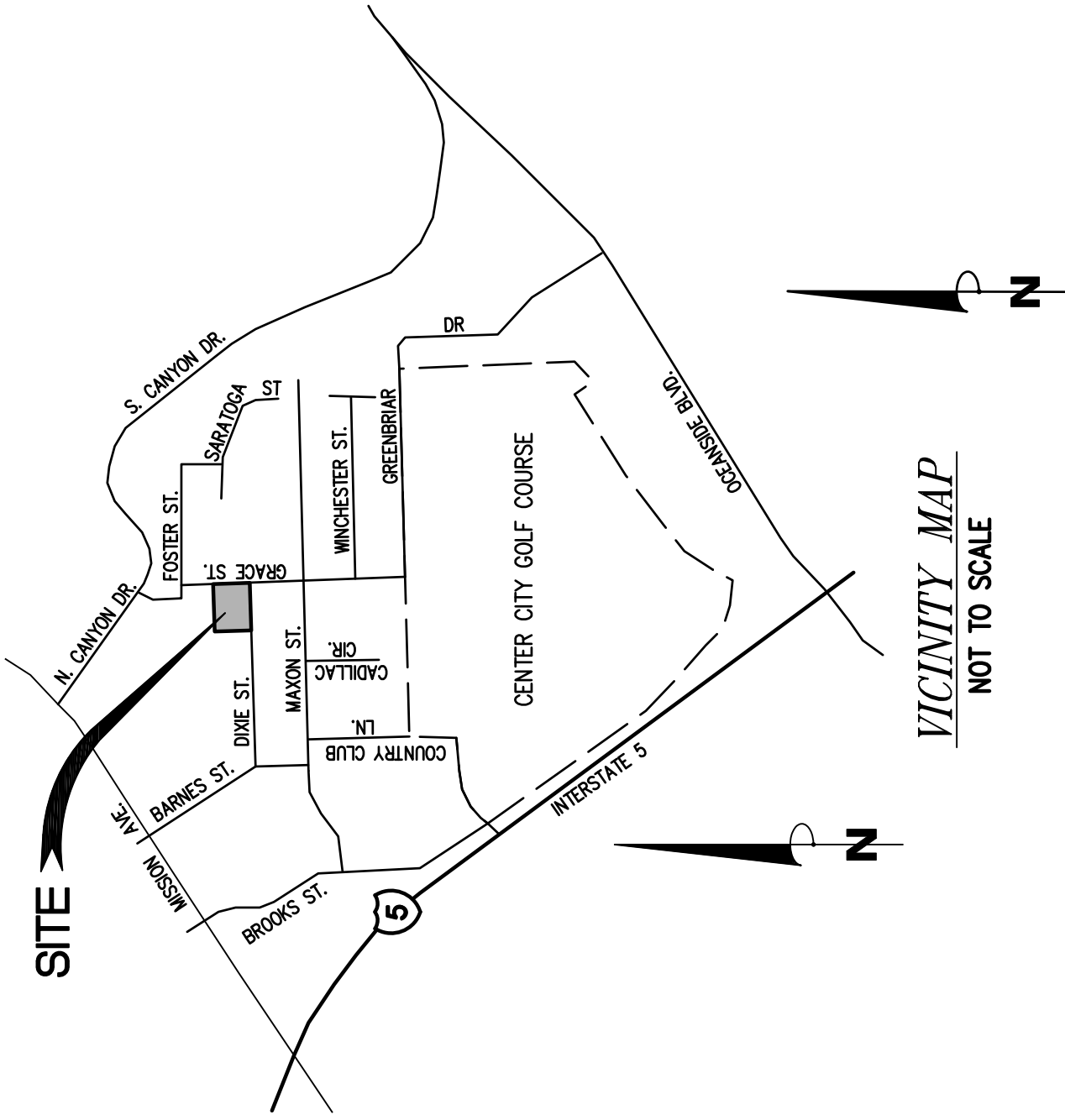
**BUCCOLA**  
**ENGINEERING, inc**

3142 Vista Way, Suite 301, Oceanside, CA 92056

760/721-2000

**FIGURE 1**

**VICINITY MAP**



**EXHIBIT A**

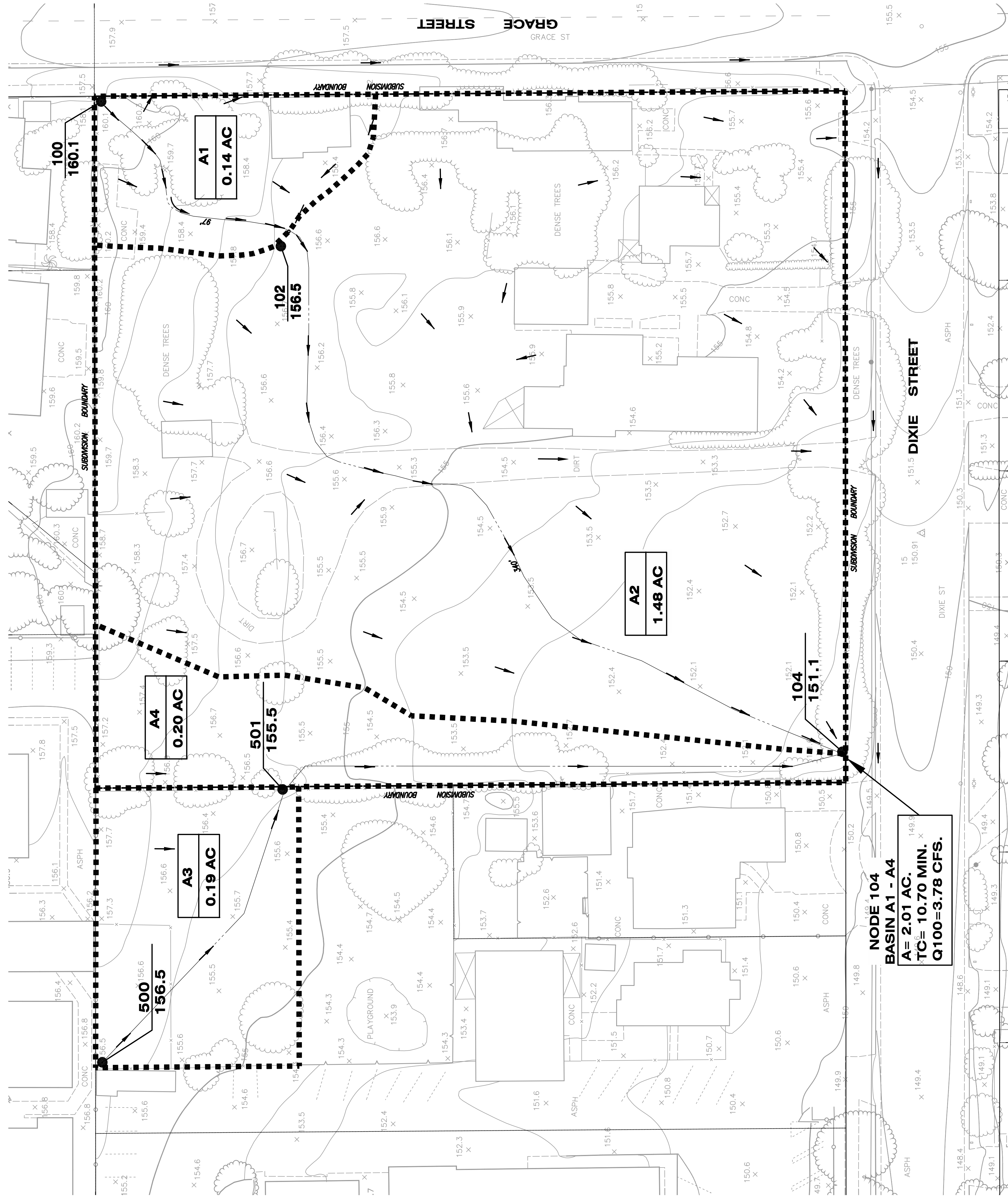
**EXISTING CONDITION  
HYDROLOGY MAP**

**FOR**

**SANDPIPER VILLA**

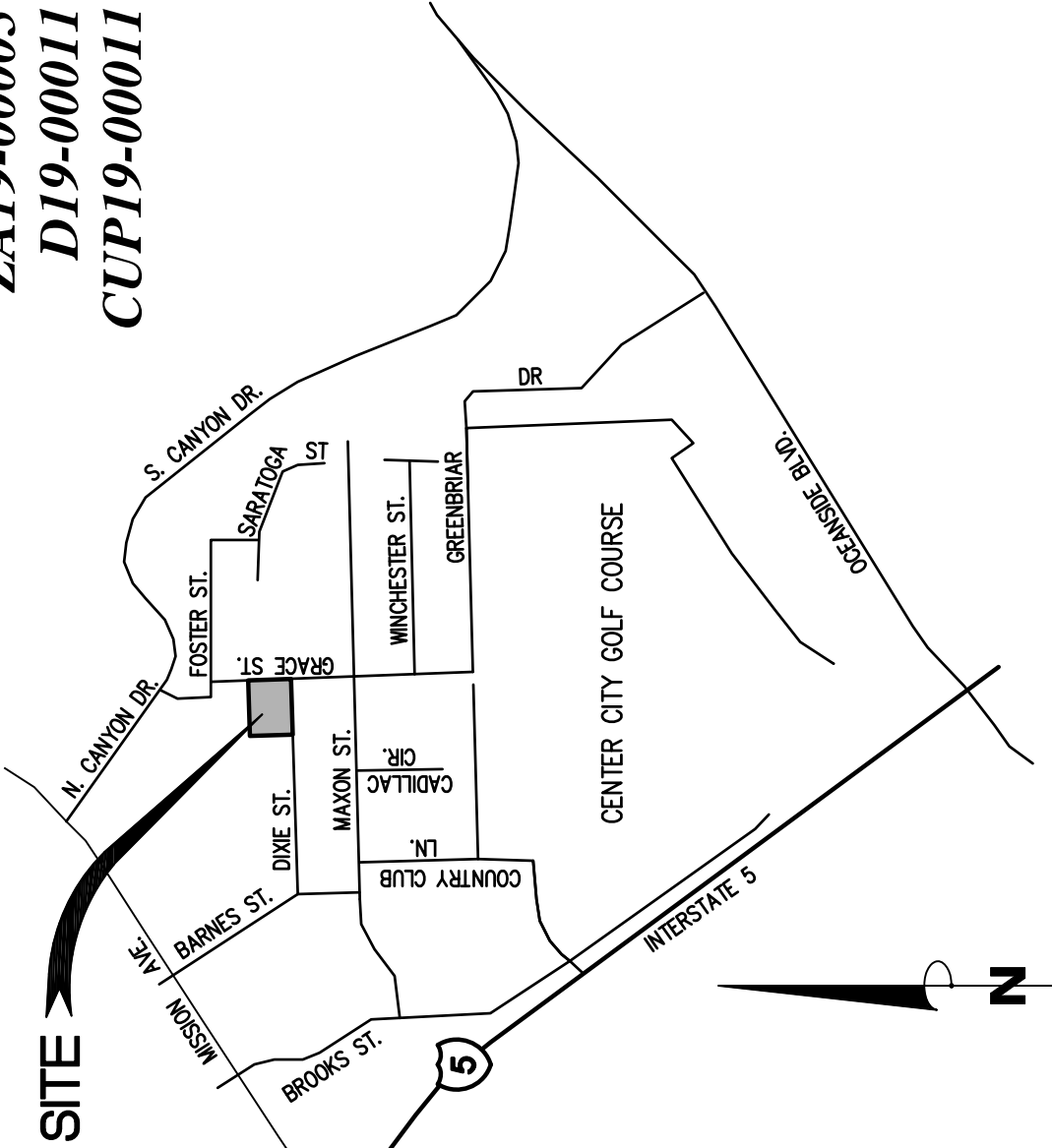
**ASSISTED LIVING FACILITY**

**OCEANSIDE, CA**

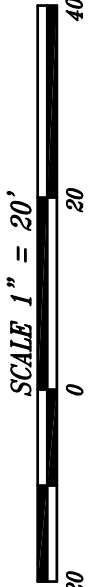




ZA19-00005  
D19-00011  
CUP19-00011



- LEGEND**
- SUB-BASIN BOUNDARY
  - SUB-BASIN DESIGNATION
  - SUB-BASIN AREA ACRES
  - DIRECTION OF FLOW
  - NODE DESIGNATION
  - FS OR IE ELEVATION
  - IMPERVIOUS-POC CONCRETE
  - SOLID UNIT PAVERS
- E1**  
0.08ac
- 102**  
122.0



**EXHIBIT B**

**PROPOSED CONDITION  
HYDROLOGY MAP**

**FOR**

**SANDPIPER VILLA**

**ASSISTED LIVING FACILITY**

**OCEANSIDE, CA**

PREPARED IN THE OFFICE OF:

**BUCCOLA**  
**ENGINEERING, inc**

760/721-2000  
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